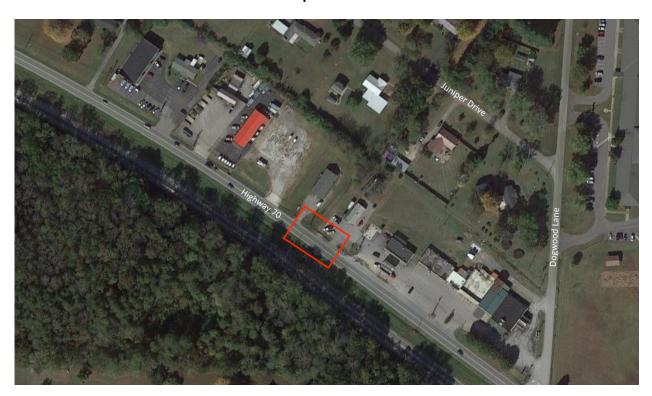


Pegram Highway 70 Flood Remediation

Final Design Academic Report April 2017



Highway 70 Shopping Area 500 Block Hwy 70 Pegram, TN 37143

Enclosures:

- A) Request for Proposal
- B) Proposal
- C) Concept Plan & Historical Review
- D) Existing Conditions Package
- E) Design Development Package
- F) Man-Hour Log & Timesheets
- G) Meeting Minutes
- H) Presentation Slides
- I) Reference Material

Contributors:

Nathan Curtis David Lowery Cody Glenn Abigail Queen Christian Reid



Section 1: Background Information

The city of Pegram, TN sent a request to the Civil Engineering Department at Lipscomb University for the provision of engineering services to assist with flooding issues at the 500 block of Highway 70, Pegram TN. Flooding at this location occurs multiple times a year, typically incurring property damage. Because the flood area is commercial, business is disrupted and often drives business owners away. It is also reported that the flooding will overtop Highway 70 in a large storm, creating safety issues.

Section 2: Design Team

The members of the design team and their respective roles are as follows:

Student Design Team

• David Lowery- Project Manager

- Has gained project management experience through working as a Project Management Intern on two multi-million-dollar construction projects for Brasfield & Gorrie General Contractors.
- Has gained site design & storm-water management experience, as well as survey experience through an internship in the Land Planning Division with Gresham Smith & Partners.

• Abby Queen -Assistant Project Manager

- Has gained project management experience through working as a Project Engineer for Meccon Industries Inc.
- Has exceptional writing & communication skills.

• Nathan Curtis - Lead CAD Drafter / Lead Survey Manager

- Has gained CAD drafting experience through working as an AutoCAD Drafter for Malo Studios, as well as through working as an intern for Engineering Missions International.
- Has gained survey experience through completing the Surveying course within Lipscomb University's Engineering Program.

• Cody Glenn - Lead Estimator

 $\circ~$ Has gained significant experience in estimating through his internship with Jones Brothers Contractors.

• Christian Reid - Hydraulic Analysis & Design Lead

- Has gained experience in hydraulic analysis & design through his Fluid Mechanics & Hydrology courses at Lipscomb.
- Has gained experience in hydraulic analysis through his position as an *Environmental Engineering Intern* with General Mills Inc.



Technical Advisors

- Chris Gwaltney P.E.
- Matt Lackey, P.E.
- Justin Bryan, P.E.
- Peter Chimera, E.I.T.

Section 3: Scope of Services

The scope of this project was to provide analysis, and design for the purpose of proving that the existing conditions cause the culverts under HWY 70 to fail per TDOT standards, and to provide design development drawings to aid in future design and construction of a flood control plan.

Deliverables:

- Concept Plan & Historical Review:
 - This included a historical review, decision matrix, and a recommended flood control plan.
- Complete set of design development construction drawings submitted at:
 - o 30%, 60%, 90%, and Completed Design Development.
 - Each submittal included a design report with a preliminary construction cost estimate.
- A Final Report, including:
 - o Oral Presentation to client
 - o Oral Presentation to Lipscomb Engineering Dept.
 - o Oral Presentation at Symposium
 - o Poster Presentation at Symposium

Section 4: Project Summary

To meet the requested scope of services, the team proposed the following phasing plan to complete the work.

- Phase 1 Site Investigation
- Phase 2 Survey
- Phase 3 Preliminary Analysis & Design
- Phase 4 Final Design



Phase 1 - Site Investigation

The purpose of this task was to gather site data and information for future design work. Subtasks during Phase 1 included:

- Site Visits
 - The team Performed an initial site visit to meet with the mayor and take pictures of the site. The mayor showed us each problem area and pictures were taken for reference during the design phase. Pictures can be found in *Enclosure I*.
- Researching TDOT Culvert Requirements
 - Research was conducted to obtain the TDOT standards for culverts in order to make a comparison between the performance of existing culverts, and the performance standards set out by TDOT. The standards can be found summarized in *Enclosure D*, as well as in the TDOT drainage manual found in *Enclosure I*. After analysis, it was found that all the culverts along the flow path of interest are failing per TDOT standards. The detailed results can be found in *Enclosure D*.
- Research Historical Flood Data
 - A well-developed storm history was developed using NOAA public information. This data was used to create a Historical Review of Flooding for the town of Pegram. This review can be found in Enclosure C.

Phase 2- Survey

The purpose of this task was to gather data that would be used to create a topographic map. This topo map would become the basis for preliminary and final design solutions.

The subtasks during the survey phase included:

- Delineating the Survey Boundary
 - Using Google maps, a general survey boundary was created to ensure sufficient survey data is collected.
- Present Project to Survey Team
 - A presentation was made to inform the survey team of the survey boundary, scope of the survey, and other logistical information.
- Preliminary Survey
 - The design team performed a preliminary survey at the site to find benchmarks and set control points for the survey team. Because no existing benchmarks could be found, a benchmark was assumed at the corner of Hwy 70 and Dogwood Ln and was given a known elevation

of 0ft. The location of this benchmark is shown in the design development drawings in *Enclosure E*.

- Provide Oversight to Survey Team
 - The survey was conducted by the sophomore survey class under the oversight of the design team. The survey was conducted using 3 Topcon total stations, and the following data was included:
 - Topographic data
 - Culvert locations and inverts
 - Edge of Pavement
 - Ditch locations and elevations
 - Building locations
- Produce Topographic Map / Site Plan
 - The survey data was transferred into AutoCAD Civil 3d and was delineated into a topographic site survey. The survey can be found in Enclosure D.

Phase 3- Preliminary Analysis & Design

The purpose of this task was to determine possible design solutions so that the team could make a recommendation to the City of Pegram for a proposed solution and receive feedback from the city.

. Subtasks during Phase 3 included:

- Delineating Drainage Basin
 - Using USGS Topo Maps, a drainage basin was delineated by using contour lines and known knowledge of the site from site visits. It was found that the drainage basin for the culverts at Hwy 70 was approximately 150 acres. The watershed map can be found in Enclosure D.
- Hydraulic Analysis
 - The survey and drainage basin data was used to perform a hydraulic analysis of the watershed, specifically along the flowpath of interest. It was determined that there are 3 different drainage basins contributing to the flows at the Culverts at the 500 block of Tennessee Highway 70, our primary area of interest. The largest drainage basin is approximately 100 acres northwest of the site, next is approximately 20 acres northeast of the primary site, and finally the 30 acre residential around the houses just north of the primary site. Once the drainage basins were delineated, the TR-55 method was

used to determine time of concentration and then that data was used as an input for Hydroflow, an Autodesk extension commonly used in practice, to determine our flows at the primary site. This information was then used to analyze our culverts throughout the project area.

Culvert Analysis

O Hydraulic capacity of the current culverts was evaluated using Hydroflow Express within the AutoCad Civil 3d Suite. The culverts were analyzed using the flows found from the hydraulic analysis. Hydroflow Express used the manning's equations to solve for the flows in the culverts, and took into account pipe roughness, size, length, slope, and other factors. It was found that when modeled for the 50yr storm, each culvert along the flow path of interest was failing with flows overtopping the road. The details of the culvert analysis can be seen in *Enclosure D – Existing Conditions Package*

• Preliminary Design

The preliminary design consisted of exploring possible solutions to the problems found while performing the hydraulic analysis. A concept plan was created outlining the possible solutions that would be further explored in the Final Design phase. This concept plan can be found in *Enclosure C.*

• Create Decision Matrix

O The decision matrix was used to determine the best solution for the City of Pegram. The criteria for the decision matrix were weighted usings a paired comparison analysis. The 5 criteria (Cost, Aesthetics, Performance, Maintenance and Land Use, and Durability) were matched against each other and given weight proportional to their importance. IE: When Aesthetics [B] is compared to cost [a], cost is given the more importance by a factor of 3, thus the cell is given the name A3. The final weight was determined by taking the total number each criterion is given over the total number added after all comparisons have been made. These weights were then used as a multiplier in the decision matrix, which compared the 3 preliminary designs (detention basin, water reroute and culvert modification) with each design's criteria rank.



Phase 4 - Final Design

The purpose of this phase was to fully design the method, or combinations of methods chosen by the Design Team in conjuncture with the City, and to produce complete design development drawings and specifications to present to the City of Pegram.

Detention Pond Design:

Detention ponds were developed to control release rate of the large amount of water flowing to the culverts at Tennessee Highway 70. This flow was largely due to a contributing watershed of approximately 100acres located north of the site. It was found in the hydrologic analysis that this flow would need to be slowed to meet the requirement established by TDOT for culverts (that they must pass the 50yr storm). The pond was developed using Hydroflow, which is an extension of Autodesk's Civil3D program. The program allowed the team to determine the approximate size requirements of detention and the appropriate release rate. Using the size and release rate information found in Hydroflow, the pond size was then iterated using a 3:1 side slope until the desired capacity was reached. The Hydroflow extension also allowed us to specify a proper outlet structure that would give the desired release rate. The details of the pond design can be found in *Enclosure E – Design Development Package*.

Diversion Design:

A diversion ditch was designed to help decrease the flow of water to Highway 70. In preliminary analysis, it was noted that there seemed to be a ditch that travelled away from the primary flow path, along the back of the businesses toward Dogwood Lane. The observed ditch did not intersect with the primary flowpath, and therefore the ditch was not being effectively utilized. The Pegram Design team developed a concrete channel that extends the ditch and intersects with the primary flow path. This allows for the flow to be directed away from highway 70. In addition to a channel, a detention structure has been added to control the amount of water that is diverted. This structure allows for a small amount of water to pass through to highway 70, and once the flow reaches the maximum flowrate that Hwy 70 can handle, any additional flow is diverted along the diversion channel, away from Hwy 70. Details for the diversion design can be seen in *Enclosure E – Design Development Package*.



Construction Cost Estimates:

The purpose of this task was to estimate the cost of construction for the proposed solutions. There were 2 major parts of the estimate: detention and diversion.

- Detention: For the detention pond, the scope included in the estimate is grading, reseeding, replacing topsoil, fill material for the dam, and a construction entrance. The fill material is to have a clay content equal to 15-30% by weight and less than 10% coarse aggregates. For the pond, all cut material is used onsite for fill, therefore saving money by not having to haul the cut away.
- Diversion: The diversion ditch estimate for the concrete channel and diversion structure includes the following scope: cut, haul off, formwork, resteel, concrete placement, and backfill.

The construction cost estimates were derived from unit prices provided by the lead estimator at Jones Bros Contractors LLC. The cost estimate breakdown can be seen in *Enclosure E – Design Development Package*.

Section 5: Quality Assurance / Project Management

The quality of the design work provided was monitored by the project manager and by all members of the design team in the following ways:

- Action Items
 - An action items spreadsheet was maintained by the project manager through the duration of the project so that all team members knew what tasks they are responsible for.
- Weekly Timesheets
 - All hours worked by each team member were logged on a weekly timesheet and sent to the Assistant Project Manager each Friday.
- Weekly Progress Meetings
 - The team held a weekly meeting to monitor the quality and progress of the work which each respective team member was responsible for.
- Technical Advisor Meetings
 - The team held meetings with technical advisors at milestone checkpoints throughout the duration of the project.



Enclosure (A): Request for Proposal



REQUEST FOR PROPOSAL (RFP)

PEGRAM, TN FLOOD REMEDIATION

AUGUST 30, 2016

RAYMOND B JONES COLLEGE OF ENGINEERING LIPSCOMB UNIVERSITY 1 UNIVERSITY PARK DRIVE NASHVILLE, TN 37214



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1. SUMMARY AND BACKGROUND

Lipscomb University's Raymond B Jones College of Engineering in partnership with the town of Pegram, TN is currently accepting proposals for the design of flood control structures in Pegram, TN. Currently the town of Pegram experiences frequent flooding of US Highway 70 and commercial properties along US 70. The flooding hampers economic development for the town, causes delays for emergency vehicles, and is a safety concern for travelers on US 70.

The purpose of this Request for Proposal (RFP) is to solicit proposals from various student teams, conduct a fair and extensive evaluation based on criteria listed herein, and select the candidate who best represents the direction Raymond B Jones College of Engineering wishes to go.

Raymond B Jones College of Engineering is an academic unit under the auspices of Lipscomb University for the education and training of engineers in three ABET/EAC accredited engineering programs: Civil Engineering, Electrical and Computer Engineering, and Mechanical Engineering. The college of engineering at Lipscomb focuses primarily on undergraduate engineering education within a faith-based community. Our client base consists of small and medium-sized businesses as well as international non-governmental humanitarian organizations which lack engineering experience and expertise.

Raymond B Jones College of Engineering is located in Nashville, Tennessee on the campus of Lipscomb University.

Our services include:

- Engineering Design
- Engineering Studies

Customer contacts

Executive Manager: Charles Moorehead, Pegram Mayor and Sean Monahan, US EPA

Project Executive: Chris A. Gwaltney



2. Proposal Guidelines

This Request for Proposal represents the requirements for the proposal process as part of the graduation requirements for engineering students in the Raymond B Jones College of Engineering. Proposals will be accepted until 8:00 am CST November 1, 2016. Any proposals received after this date and time will be returned to the sender. All proposals must be signed by the proposed project manager and all team members.

If the team submitting a proposal must outsource or contract any work to meet the requirements contained herein, this must be clearly stated in the proposal. Additionally, all costs included in proposals must be all-inclusive to include any outsourced or contracted work. Any proposals which call for outsourcing or contracting work must include a name and description of the organizations being contracted.

All costs must be itemized to include an explanation of all fees and costs.

Contract terms and conditions will be negotiated upon selection of the highest qualified firm for this RFP. All contractual terms and conditions will be subject to review by Raymond B Jones College of Engineering and will include scope, budget, schedule, and other necessary items pertaining to the project.

3. PROJECT PURPOSE AND DESCRIPTION

The purpose of this project is as follows:

To provide design documents, including plan drawings and specifications to facilitate the construction of flood control structures to alleviate flooding in Pegram, TN.

Project Description:

Pegram, TN is located approximately 23 miles west of Nashville along US Highway 70 (see figure 1). Flooding in Pegram is a result of storm water runoff from highlands to the north of town. The runoff drains to the south towards the Harpeth River, but must first pass under US 70 and a CSX rail line (see figure 2). The culverts under US 70 are inadequate to pass the runoff of relatively frequent rainfall events and thus water backs up into the commercial area along the highway, and eventually overtops the highway. The flood water is then retained by the CSX railroad embankment until it can drain through a culvert and bridge under the railroad. The rainfall return frequency for the flood events is unknown to the RFP writer. This project is part of the The College/Underserved Community Partnership Program (CUPP) through the US EPA.

 $\underline{https://www.epa.gov/communityhealth/collegeunderserved-community-partnership-program-cupp}$



Figure 1. Site Location

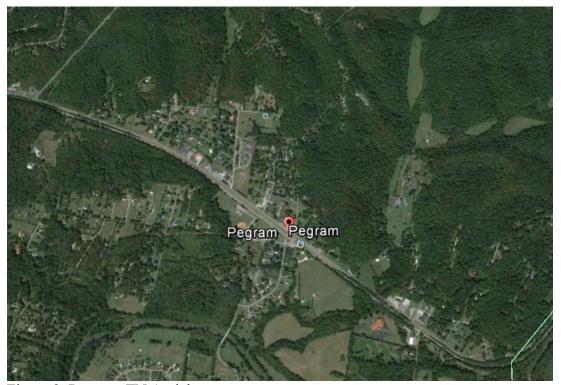


Figure 2. Pegram, TN Aerial



Figure 3. Commercial Area

4. PROJECT SCOPE

The scope of this project is to provide all analyses, laboratory testing, design, and construction documentation required for the design and construction of a comprehensive flood control project for Pegram, TN.

The following criteria must be met to achieve a successful project:

- Historical review of flood events in Pegram.
- Historical review of any flood studies performed for Pegram.
- A topographic survey of the primary areas flooded in Pegram.
- Determine possible flood control practices, structures, and combinations of such that will relieve flooding in Pegram; including their advantages, disadvantages, costs, and constraints.
- Development and implementation of a decision matrix for selection of a flood control plan to carry out for the final design.
- Work with the town officials in Pegram, the Tennessee Department of Transportation (TDOT), CSX Railroad, and The College/Underserved Community Partnership Program (CUPP) through the US EPA.
- A hydrologic/hydraulic study required for the design.
- Final design for all components of the selected flood control plan.



Deliverables

- Feasibility Report (with historic review, presentation of completed decision matrix, and a recommended flood control plan). This report will be presented at a review meeting with the client and other interested parties.
- Complete set of construction drawings submitted at:
 - o 30%, 60%, 90%, IFC.
 - Each submittal shall include a design report with a preliminary construction cost estimate.
 - Specifications shall be provided with each submittal, except the 30% submittal.
 - o An invoice for work completed will be provided at each submittal
- A Final Report, including:
 - o Sections on all parts of the design
 - o Oral Presentation to client
 - o Oral Presentation at Symposium
 - Poster Presentation at Symposium

5. REQUEST FOR PROPOSAL AND PROJECT TIMELINE

Request for Proposal Timeline:

All proposals in response to this RFP are due no later than 8:00 am CST November 1, 2016.

Presentation of the Proposal to the client shall be on November 8, 2016. Evaluation and negotiations of the proposal will be conducted immediately following the presentation. The Final Proposal will be signed and the Notice to Proceed (NTP) issued no later than end of business on November 9, 2016.

Project Timeline:

Project work begins immediately upon receipt of the NTP.

Date due	Deliverable
December 6, 2016	Site Survey
December 6, 2016	Historic Review, Conceptual Flood Control Plans, & Decision Matrix
	with criteria and weighting
January 24, 2017	Completed Decision Matrix with selected plan & 30% Submittal
February 14, 2017	60% Submittal
March 7, 2017	90% Submittal
March 28, 2017	Final Design Report and PowerPoint slides for Oral Presentation
April 4, 2017	Oral Presentation
April 11, 2017	IFC Drawings and Specifications

6. BUDGET AND SCHEDULE

All proposals must include a detailed schedule linked to a valid Work Breakdown Structure (WBS) identifying each task necessary for successful completion of the project. Person-hours associated with each task must be clearly tabulated along with each task's duration.

In addition to the detailed breakdown, a summary accounting of man-hours and direct costs to complete the tasks described in the project scope must be listed for each of the following items in accordance with the format below:

Task	Person Hours
Historic Review, Conceptual Plan, &	XXX
Decision Matrix with preferred plan	
Hydrologic/Hydraulic Study	XXX
Design of Flood Control Structure(s)	XXX
Meetings with client and other parties	XXX
Final Design Report and Oral Presentation	XXX
CAD	XXX
Specifications	XXX

Direct costs will be provided for all items required to complete the work.

A fee schedule will be provided for all labor anticipated to complete the work.

7. TEAM QUALIFICATIONS

Teams must provide the following items as part of their proposal for consideration:

- Description of experience.
- Resumes of all team members
- Management plan detailing areas of responsibility for each team member.
- Timeframe for completion of the project

8. QUALITY ASSURANCE

Each team will provide a detailed plan to assure that a high quality product is delivered.

9. PROPOSAL EVALUATION CRITERIA

Raymond B Jones College of Engineering will evaluate all proposals based on the following criteria. To ensure consideration for this Request for Proposal, your proposal should be complete and include all of the following criteria:



- Overall quality of the response to this Request for Proposal.
- Overall proposal suitability: proposed solution(s) must meet the scope and needs included herein and be presented in a clear and organized manner
- Value and Quality: Teams will be evaluated on the value and quality their solution(s) based on the work to be performed in accordance with the scope of this project
- Technical expertise and experience: Teams must provide descriptions and documentation of staff technical expertise and experience

Each team must submit 2 copies of their proposal to the address below by November 11, 2016 at 8am CST:

Raymond B Jones College of Engineering Lipscomb University 1 University Park Dr Nashville, TN 37214



Enclosure (B): Project Proposal

Charles Moorehead Mayor, City of Pegram Pegram City Hall 308 Highway 70 Pegram, TN 37143

Dear Mr. Moorehead,

Subject: Proposal for Engineering Services – Flood Remediation

Highway 70 Shopping Area

Pegram, TN 37143

Enclosures:

(A) Proposal for Engineering Services

- (B) Preliminary Work Breakdown Structure
- (C) Estimated Project Schedule

Lipscomb University Senior Design Team presents for the town of Pegram our proposal for engineering services to remediate the flooding issue at the 500 block on Tennessee Highway 70. We have prepared this proposal based on the following information.

- Request for proposal submitted to the group by Lipscomb University as a basis for the senior design project
- Site Visit & Meeting with Mayor of Pegram
- Aerial photography of the site
- Publically available historical data

The Lipscomb University Senior Design Team appreciates the consideration of the City of Pegram for our participation on the project.

Sincerely,

David Lower

- David A. Lowery



Enclosure (A): Proposal for Engineering Services



Section 1: Background Information

The city of Pegram, TN sent a request to the Civil Engineering Department at Lipscomb University provide engineering services to assist with flooding issues at the 500 block of Highway 70, Pegram TN. Flooding at this location occurs multiple times a year, typically incurring property damage. Because the flood area is commercial, business is disrupted and often drives business owners away. It is also reported that the flooding will overtop Highway 70 in a large storm, therefore creating safety issues. This proposal, based upon the request for proposal, historical data, site visits, and conversations with longtime Pegram residents, is a proposal for engineering services to analyze the flooding problem, and design a solution.

Section 2: Design Team

The members of the design team and their respective roles are as follows:

Student Design Team

• David Lowery- Project Manager

- Has gained project management experience through working as a Project Management Intern on two multi-million-dollar construction projects for Brasfield & Gorrie General Contractors.
- Has gained site design & storm-water management experience, as well as survey experience through an internship in the Land Planning Division with Gresham Smith & Partners.

• Abby Queen -Assistant Project Manager

- Has gained project management experience through working as a Project Engineer for Meccon Industries Inc.
- Has exceptional writing & communication skills.

• Nathan Curtis - Lead CAD Drafter / Lead Survey Manager

- Has gained CAD drafting experience through working as an AutoCAD Drafter for Malo Studios, as well as through working as an intern for Engineering Missions International.
- Has gained survey experience through completing the Surveying course within Lipscomb University's Engineering Program.

• Cody Glenn - Lead Estimator

• Has gained significant experience in estimating through his internship with Jones Brothers Contractors.



• Christian Reid - Hydraulic Analysis & Design Lead

- Has gained experience in hydraulic analysis & design through his Fluid Mechanics & Hydrology courses at Lipscomb.
- Has gained experience in hydraulic analysis through his position as an *Environmental Engineering Intern* with General Mills Inc.

Technical Advisors

- Chris Gwaltney P.E.
- Matt Lackey, P.E.
- Justin Bryan, P.E.
- Peter Chimera, E.I.T.

Section 3: Scope of Services

The scope of this project is to provide analysis, design, and construction documentation required for the design and construction of a flood control plan for Pegram, TN.

- Historical review of flood events in Pegram.
- Historical review of any flood studies performed for Pegram.
- A topographic survey of the primary areas flooded in Pegram (subcontracted to Lipscomb surveying course, but administered by team).
- Determine possible flood control practices, structures, and combinations of such that will relieve flooding in Pegram; including their advantages, disadvantages, costs, and constraints.
- Development and implementation of a decision matrix for selection of a flood control plan to carry out for the final design.
- Work with the town officials in Pegram, the Tennessee Department of Transportation (TDOT), CSX Railroad, and The College/Underserved Community Partnership Program (CUPP) through the US EPA.
- A hydrologic/hydraulic study required for the design.
- Final design for all components of the selected flood control plan.

Deliverables:

- Feasibility Report
 - This will include a historical review, presentation of completed decision matrix, and a recommended flood control plan. This report will be presented at a review meeting with the client and other interested parties.
- Complete set of construction drawings submitted at:
 - o 30%, 60%, 90%, Issued for Construction.



- o A client meeting will be held with each submittal
- Each submittal will include a design report with a preliminary construction cost estimate.
- Specifications will be provided with the 90% submittal and Issued for Construction Drawings.
- o An invoice for work completed will be provided at each submittal
- A Final Report, including:
 - Oral Presentation to client
 - o Oral Presentation at Symposium
 - o Poster Presentation at Symposium

Section 4: Project Plan

To meet the requested scope of services, the team is proposing the following phasing plan to complete the work.

- Phase 1 Site Investigation
- Phase 2 Survey
- Phase 3 Preliminary Design
- Phase 4 Final Design

Phase 1 - Site Investigation

The purpose of this task is to gather site data and information for future engineering design work. Subtasks during Phase 1 shall include but are not limited to:

- Research TDOT Culvert Requirements
 - Research will be conducted to obtain the TDOT standards for culverts in order to make a comparison between the performance of existing culverts, and the performance standards set out by TDOT.
- Research ROW / Utility Constraints
 - ROW boundaries will be determined from plats and will be used during the design phase.
 - Utility Easements will be determined using plats as well as field located using TN 411. These will be used during the design phase.
- Research Historical Flood Data
 - A well-developed storm history will be developed using NOAA public information.
- Site Visits
 - The team will perform site visits to obtain any needed information such as pictures, measurements, or additional survey data.



Phase 2- Survey

The purpose of this task is to gather data that will be used to build a topographic map. This topo map will be the basis for preliminary design solutions. The mapping will provide contours at one foot intervals. The Pegram Flood Team will prepare the topographic map using CAD software. Subtasks during Phase 2 shall include but are not limited to:

- Delineate Survey Boundary
 - Using Google maps, a general survey boundary will be created to ensure sufficient survey data is collected.
- Present Project to Survey Team
 - A presentation will be made to inform the survey team of the needs for the survey.
- Preliminary Survey
 - The design team will perform a preliminary survey at the site to find benchmarks and set control points for the survey team.
- Provide Oversight to Survey Team
 - the design team will accompany the survey team to provide assistance and oversight to the team as they perform the survey.
- Produce Topographic Map / Site Plan
 - The survey data will be transferred into AutoCAD to produce a Topo Survey. This will be used as a basis for design.

Phase 3- Preliminary Design

The purpose of this task will be to determine possible design solutions so that the team can make a recommendation to the City of Pegram for a proposed solution and the City can provide input on which design they believe will suit their needs. Subtasks during Phase 3 shall include but are not limited to:

- Delineate Drainage Basin
 - Using USGS Topo Maps, a drainage basin may be obtained by using the contour lines.
- NCRS TR 55 Method of Analysis
 - The survey and drainage basin data will be used in the NCRS TR-55 methodology. The Time of concentration will be acquired through this process.



- Culvert Analysis
 - Hydraulic capacity of the current culverts will be evaluated from the known dimensions of the culverts.
 - This data will be compared with the TDOT standards for culverts to determine if the current culvert meets the requirements.
- Preliminary Detention Design
 - For our purposes, the use of detention basins will be investigated in multiple locations. The simplified steps for design will be as follows:
 - Estimate the preliminary storage volume
 - Use site topography to prepare a preliminary layout of a detention basin that has the desired volume and outlet configuration.
 - Determine stage-storage-outflow characteristics of the trial pond size.
 - Perform routing of input hydrographs through the pond.
- Preliminary Ditch Improvement Design
 - Ditch modifications will be analyzed to determine the feasibility of improving the efficiency of channel flow to alleviate flooding
 - The use of In-Channel Bio Retention will also be investigated.
- Preliminary Culvert Improvement Design
 - Using the data from the culvert analyses performed during the *Site Investigation* phase, the team will design to either resize the current culverts or add supplementary culverts underneath highway 70, Juniper Drive, and Hannah Ford Road
- Create Decision Matrix
 - The criteria for decision matrix are as follows:
 - Cost
 - Maintenance
 - Feasibility
 - Performance
 - Longevity
 - Degree of Disruption

Phase 4 - Final Design

The purpose of this task is to fully design the method, or combinations of methods chosen by the Design Team in conjuncture with the City, and to produce complete construction documents and specifications to present to the City of



Pegram. All work during this phase will be done to produce the deliverables listed in *Section 3: Scope of Services.*

Section 5: Quality Assurance / Project Management

The quality of the design work provided will be monitored by the project manager and by all members of the design team. The quality of the work will be monitored in the following ways:

- Action Items
 - An action items spreadsheet will be maintained by the project manager and will be sent out at the beginning of each week so that all team members know what tasks they are responsible for.
- Weekly Timesheets
 - All hours worked by each team member will logged on a weekly timesheet and sent to the Assistant Project Manager each Friday.
- Weekly Progress Meetings
 - The team will hold a weekly meeting to monitor the quality and progress of the work which each respective team member is responsible for.
- Technical Advisor Meetings
 - The team will hold meetings with technical advisors at milestone checkpoints throughout the duration of the project.
 - The professional advisors for this project are listed in *Section 2: Design Team*
 - These meetings will serve to allow the advisors to make comments and suggestions to help increase the quality of the design work.

Section 6: Time Estimations

The client will only be billed for hours worked. The team will not exceed the estimated number of hours without consulting the client. The current task and time estimates can be seen in *Enclosure (B) Preliminary Work Breakdown Structure*.

Section 7: Schedule

A working copy of the project schedule was developed in Microsoft Project and is included as an attachment. The schedule will be maintained by the Project Manager and will be available upon request. The Estimated Project Schedule is attached in *Enclosure (C) Preliminary Project Schedule*.

The dates for each submittal are listed below. Please plan on meeting within a week of each submittal for review.

Date Due	Deliverable
January 24, 2017	Completed Decision Matrix with selected plan & 30% Submittal
February 14, 2017	60% Submittal
March 7, 2017	90% Submittal
March 28, 2017	Final Design Report
April 11, 2017	IFC Drawings and Specifications

Section 8: Closing

Lipscomb University Senior Design Team appreciates the opportunity to work on this project. The team Is available to meet with you to discuss the proposed work, or to discuss any modifications that may need to be made to the proposal to fit your needs. We look forward to working with you.

Sincerely,

-David A. Lowery

- Charles Morehead



Enclosure (B):

Preliminary Work Breakdown Structure



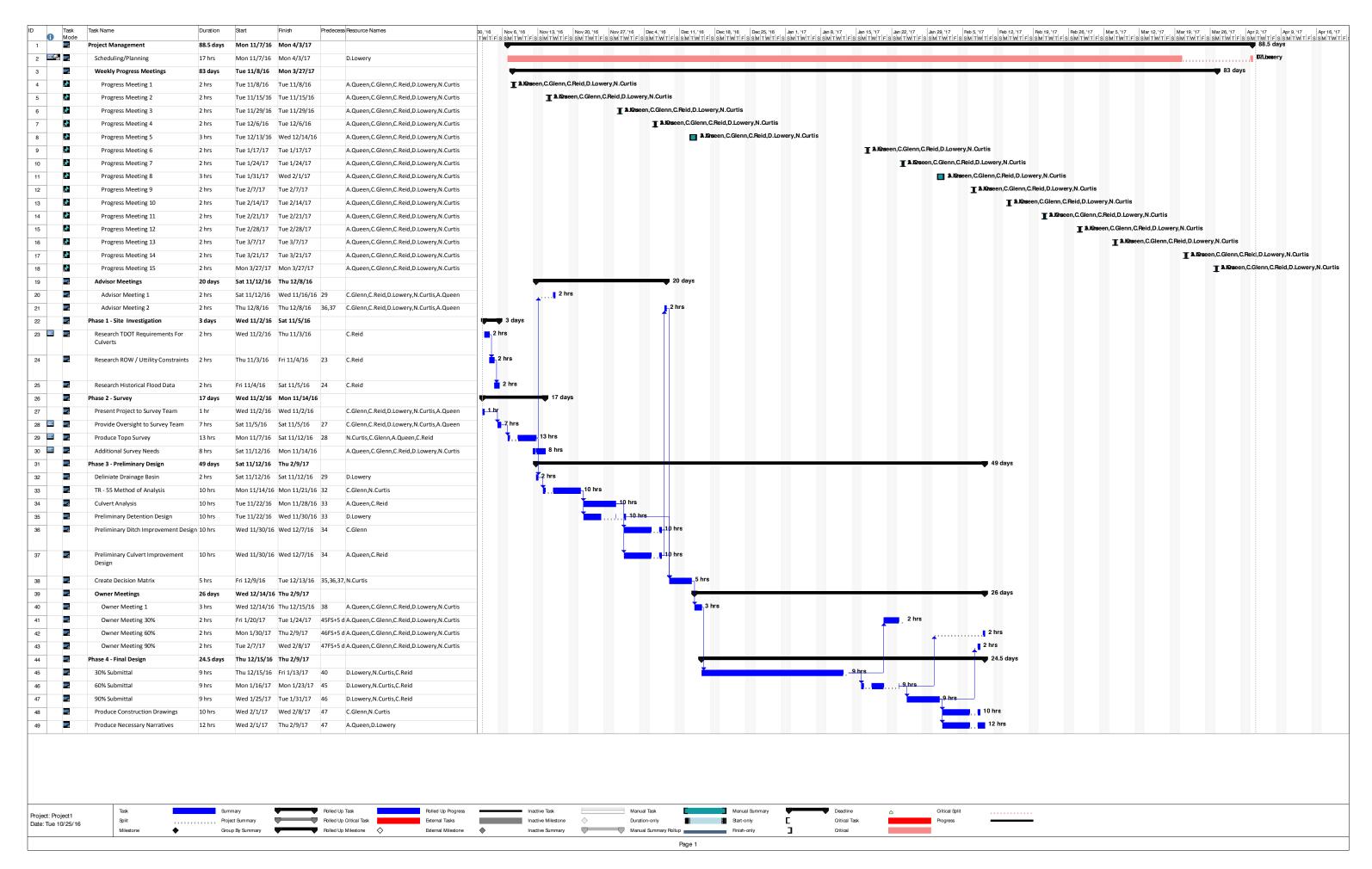
Enclosure (C):

Preliminary Project
Schedule

ENCLOSURE (B) - PRELIMINARY WORK BREAKDOWN STRUCTURE

CATEGORY:	TASKS:	TEAM MEMBER	# OF TEAM	MAN HOURS	TOTAL HOURS
PROJECT MANAGEMENT					
	Scheduling/Planning	D.Lowery	1	17	17
Management	Advisor Meetings	A.Queen,C.Glenn,C.Reid,D.Lowery,N.Curtis	5	5	25
Ü	Weekly Progress Meetings	A.Queen,C.Glenn,C.Reid,D.Lowery,N.Curtis	5	30	150
	PHASI	1 - SITE INVESTIGATION	<u>'</u>		
	Research TDOT Requirements For Culverts	C.Reid	1	2	2
Investigation	Research ROW / Uttility Constraints	C.Reid	1	2	2
0	Research Historical Flood Data	C.Reid	1	4	4
		PHASE 2 - SURVEY:			
	Present Project to Survey Team	A.Queen,C.Glenn,C.Reid,D.Lowery,N.Curtis	5	1	5
	Preliminary Survey Trip	A.Queen,C.Glenn,C.Reid,D.Lowery,N.Curtis	5	3	15
	Provide Oversight to Survey Team	A.Queen,C.Glenn,C.Reid,D.Lowery,N.Curtis	5	8	40
	Produce Topo Survey	N.Curtis, C.Glenn, A.Queen, C.Reid	1	13	13
	Additional Survey Needs	C.Glenn,C.Reid,D.Lowery,N.Curtis	4	5	20
	·	3 - PRELIMINARY DESIGN	<u> </u>	•	
	Deliniate Drainage Basin	D.Lowery	1	2	2
Hydraulic Analysis	TR - 55 Method of Analysis	C.Glenn,N.Curtis	3	10	30
	Culvert Analysis	A.Queen,C.Reid	3	10	30
	Preliminary Detention Design	D.Lowery	2	10	20
Determine Preliminary	Preliminary Ditch Improvement Design	C.Glenn	2	10	20
Solutions	Preliminary Culvert Improvement Design	A.Queen,C.Reid	2	10	20
	Create Decision Matrix	N.Curtis,A.Queen	2	6	12
PHASE 4 - FINAL DESIGN					
	30% Submittal	A.Queen,C.Glenn,C.Reid,D.Lowery,N.Curtis	5	10	50
	30% Submittal Owner Meeting	A.Queen, C.Glenn, C.Reid, D.Lowery, N.Curtis	5	1	5
	60% Submittal	A.Queen, C.Glenn, C.Reid, D.Lowery, N.Curtis	5	10	50
	60% Submittal Owner Meeting	A.Queen, C.Glenn, C.Reid, D.Lowery, N.Curtis	5	1	5
	90% Submittal	A.Queen, C.Glenn, C.Reid, D.Lowery, N.Curtis	5	10	50
Final Design	90% Submittal Owner Meeting	A.Queen, C.Glenn, C.Reid, D.Lowery, N.Curtis	5	1	5
	Issued for Construction Drawings	C.Glenn,N.Curtis,C.Reid	3	10	30
	Construction Specifications	A.Queen,D.Lowery	2	5	10
	Oral Presentation To Client	A.Queen, C.Glenn, C.Reid, D.Lowery, N.Curtis	5	3	15
	Oral Presentation At Symposium	A.Queen, C.Glenn, C.Reid, D.Lowery, N.Curtis	5	3	15
	Poster Presentation At Symposium	A.Queen, C.Glenn, C.Reid, D.Lowery, N.Curtis	5	1	5

TOTAL: 667





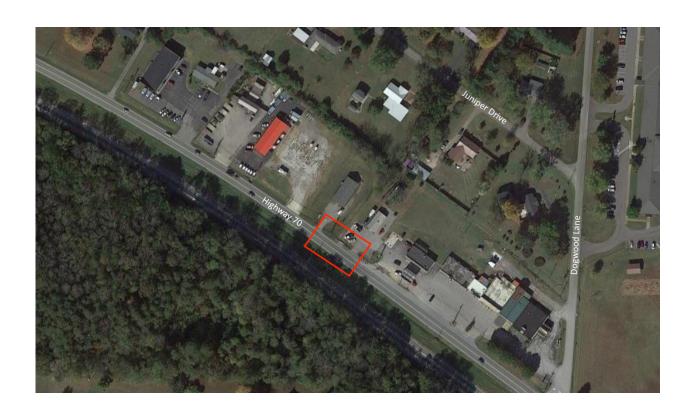
Enclosure (C): Concept Plan & Historical Review



Enclosure (D): Existing Conditions Package



Existing Conditions of the Pegram Highway 70 Culverts *Technical Report*



Highway 70 Shopping Area 500 Block Hwy 70 Pegram, TN 37143

Enclosures:

- A. Survey Existing Conditions
- B. Watershed Delineation Map
- C. Soil Report
- D. Land Use Map
- E. Hydrology Report
- F. Culvert Analysis Report

Contributors:

Nathan Curtis David Lowery Cody Glenn Abigail Queen Christian Reid

Introduction:

The Lipscomb University senior design team was asked by the city of Pegram to address a flooding issue that takes place at three culverts running under Highway 70. It was apparent that these culverts were not meeting TDOT standards, however there was no qualitative data to back up the claim. The following is our analysis of the existing conditions of the culverts at the 500 block of Hwy 70 as well as the culverts along the flow path to the 500 block of Hwy 70.

Research & Analysis:

We set out in the fall of 2017 to gather survey data around the place of flooding, in hopes that it would help inform our hydraulic analysis. Our survey covered the area bounded by Highway 70, Dogwood Lane, and Hannah Ford Road. The completed survey can be seen in enclosure (A). This data, along with GIS data, was used to analyze the watershed and current culvert conditions. We found that each of the culverts along the flow path of interest (flowing south from Hannah Ford Rd along the ditch to HWY 70), are failing per TDOT standards as seen in Figure 1.

TDOT Standards:

	Interstate System and Arterial With Full Access Control	Arterial Without Full Access Control	Collector	Local Road
Inlet Design Frequency	50-yr	10-yr ¹	10-yr ¹	10-yr
Sewer Design Frequency	50-yr	10-yr ¹	10-yr ¹	10-yr
Culvert Design Frequency	50-yr Check for 100-yr	50-yr Check for 100-yr	50-yr Check for 100-yr	50-yr Check for 100-yr
Roadway Freeboard ²	50-yr	50-yr	50-yr	50-yr
Ditch Design Frequency	50-yr	10-yr ¹	10-yr ¹	10-yr

Figure 1 TDOT Current Culvert Standards

Per the TDOT standards shown above, all culverts are to be designed for a 50 year storm, and if feasible, for the 100 year storm. Each of the culverts along the flow path are failing under the 50-year storm conditions.



For ease of reference, Figure 2 (Left) shows the naming convention used for each of the culverts along the flow path. This can be seen in more detail in Enclosure (A).

The results of our analysis for a 50 year storm event can be seen summarized in Table 1 below, and in more detail in *enclosures* (E)& (F).

CULVERT DATA ALONG FLOWPATH FOR 50 YEAR STORM — EXISTING											
CULVERT NAME	# OF CULVERTS	SIZE OF CULVERTS	CULVERT CAPACITY (CFS)	TOTAL INCOMING FLOW (CFS)	FLOW OVERTOPPING (CFS)	DEPTH OF FLOW OVERTOPPING ROAD					
1	1	36X60" ELLIPTICAL	106	148	41	3 IN.					
2	1	36" ROUND	68	103	34	1.8 IN.					
3	3	36" ROUND	143	172	28	2.4 IN.					
4	3	18X30" ELLIPTICAL	64	220	125	5 IN.					

Table 1 Culvert Analysis under 50-yr Storm Conditions

Conclusion:

According to our analysis, all culverts along the flow path of interest are failing at the 50-year storm. From this data, we can conclude that the problem is not only the culverts that run under highway 70 (culvert 4 in Fig 2), but all the other culverts as well. We request that TDOT review our work and consider addressing the issues we have found.

Sincerely,

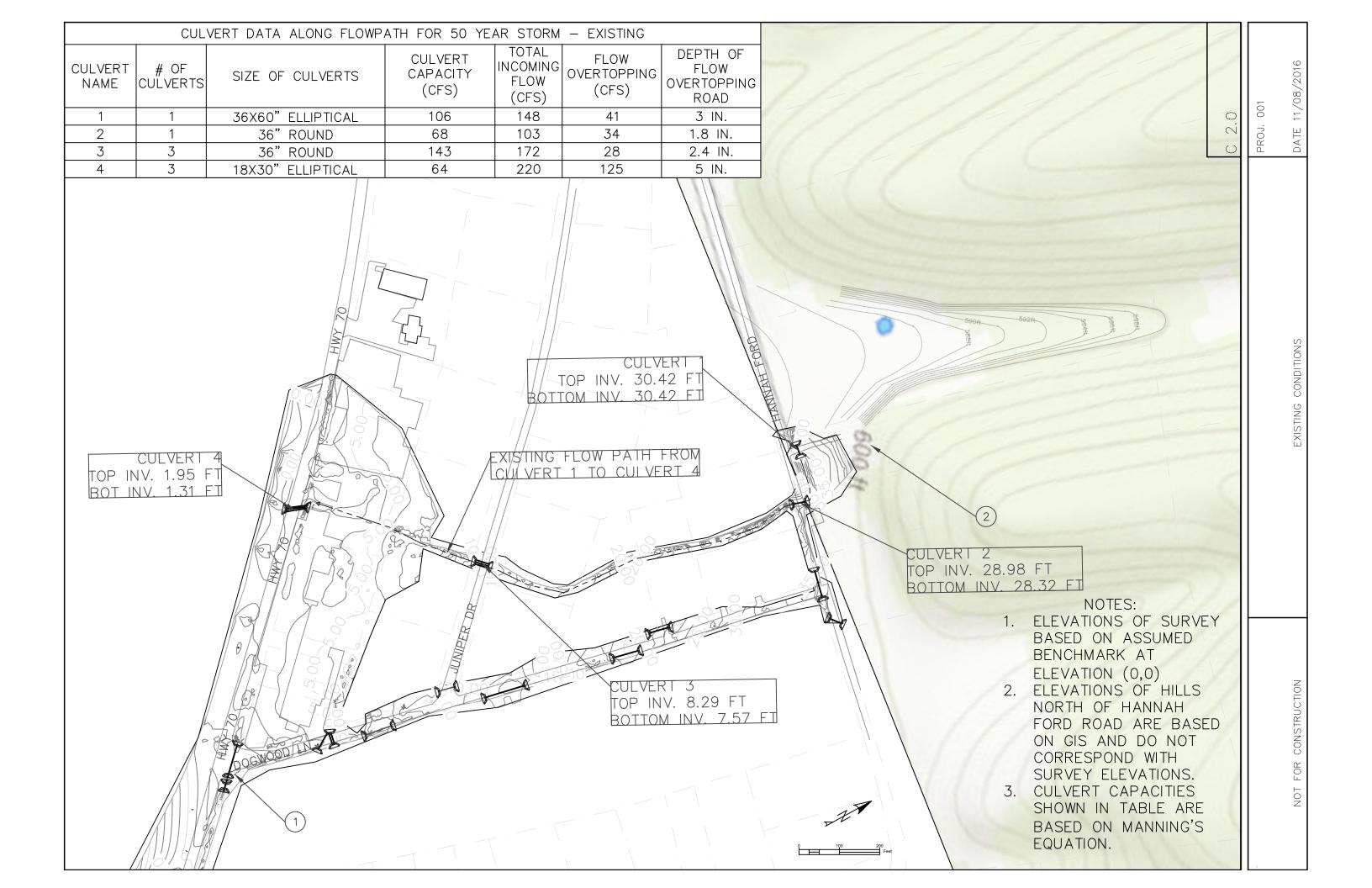
David Lowery (615) 881-3973

loweryda@mail.lipscomb.edu



ENCLOSURE (A)

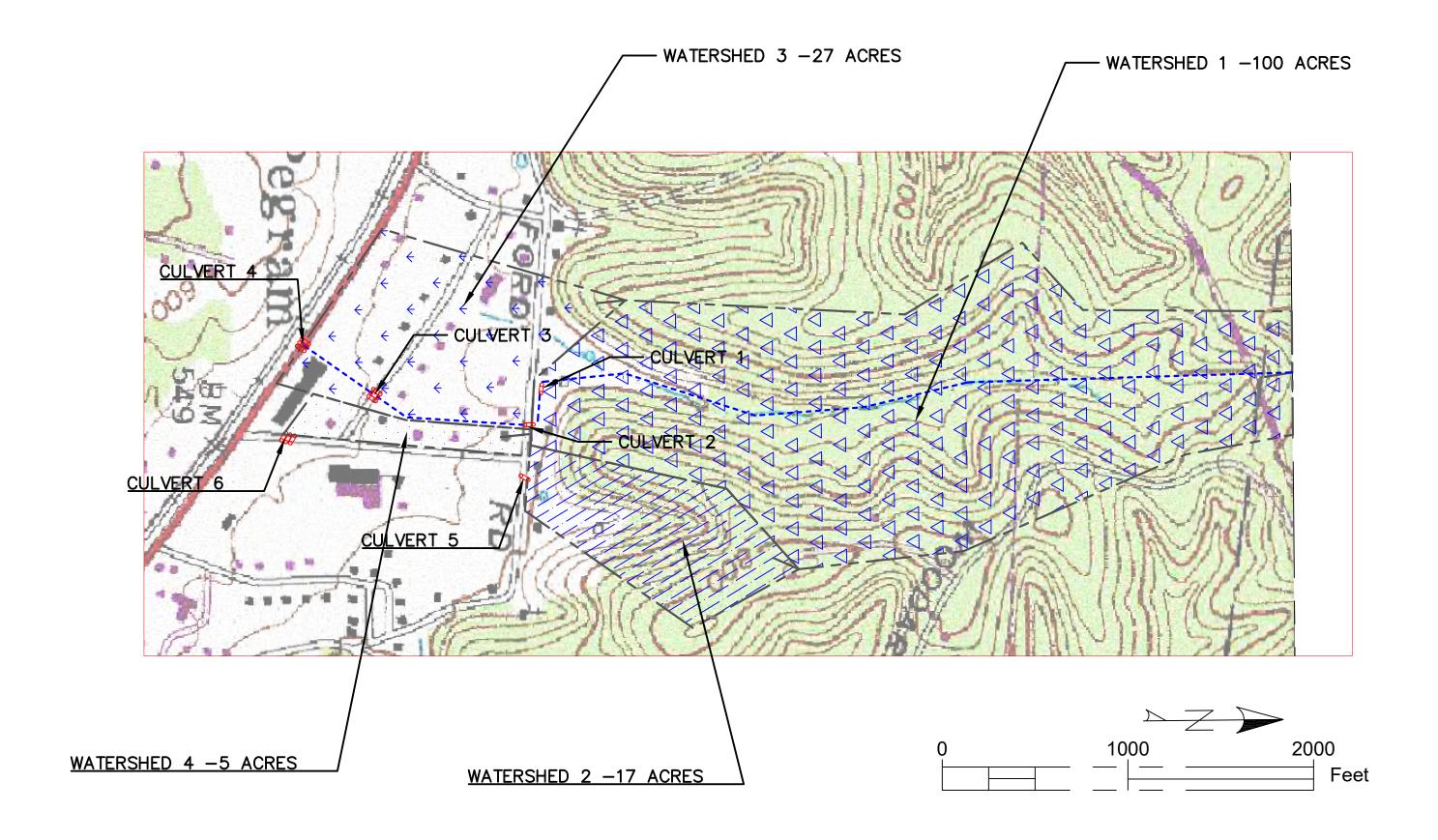
SURVEY – EXISTING CONDITIONS





ENCLOSURE (B)

WATERSHED DELINIATION MAP





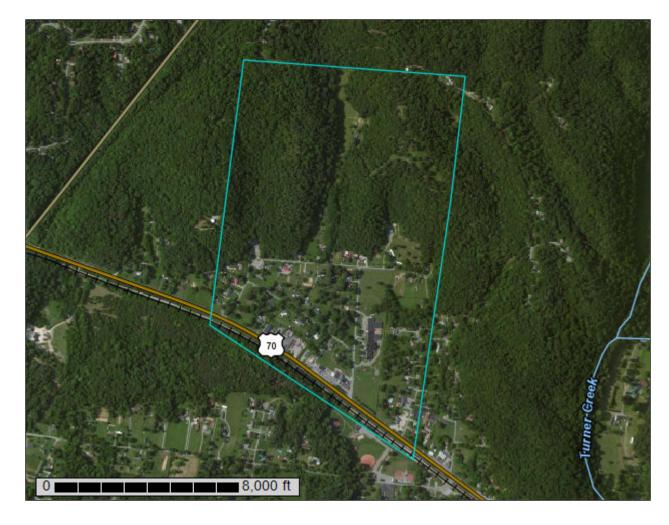
ENCLOSURE (C)

SOIL REPORT



Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Cheatham County, Tennessee





MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Unit Polygons

-

Soil Map Unit Lines

Soil Map Unit Points

Special Point Features

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Blowout

 \boxtimes

Borrow Pit

Ж

Clay Spot

 \Diamond

Closed Depression

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Gravel Pit

...

Gravelly Spot

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Landfill

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Lava Flow

Marsh or swamp

2

Mine or Quarry

X.

Miscellaneous Water

0

Perennial Water
Rock Outcrop

Saline Spot

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Sandy Spot

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Severely Eroded Spot

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Sinkhole

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Sodic Spot

Slide or Slip

Spoil Area

Stony Spot



Very Stony Spot

3

Wet Spot Other



Special Line Features

Water Features

_

Streams and Canals

Transportation

ransp

Rails

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Interstate Highways

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US Routes

 \sim

Major Roads

~

Local Roads

Background

100

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Cheatham County, Tennessee Survey Area Data: Version 10, Sep 11, 2015

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Mar 17, 2011—May 30, 2011

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Cheatham County, Tennessee (TN021)								
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI					
AmB2	Armour silt loam, 2 to 5 percent slopes	23.8	10.5%					
AmC2	Armour silt loam, 5 to 12 percent slopes	0.0	0.0%					
ВуВ2	Byler silt loam, 2 to 5 percent slopes, eroded	53.3	23.4%					
En	Ennis gravelly silt loam, occasionally flooded	12.8	5.6%					
HaC	Hawthorne gravelly silt loam, 5 to 12 percent slopes	17.7	7.8%					
HaD	Hawthorne gravelly silt loam, 12 to 20 percent slopes	16.7	7.3%					
HsF	Hawthorne-Sulphura association, steep	68.1	29.9%					
HuB	Humphreys gravelly silt loam, 2 to 5 percent slopes	12.6	5.5%					
MnD2	Minvale gravelly silt loam, 12 to 20 percent slopes, eroded	22.7	10.0%					
Totals for Area of Interest		227.6	100.0%					

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They

generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Cheatham County, Tennessee

AmB2—Armour silt loam, 2 to 5 percent slopes

Map Unit Setting

National map unit symbol: 2td31 Elevation: 500 to 850 feet

Mean annual precipitation: 48 to 58 inches

Mean annual air temperature: 57 to 61 degrees F Frost-free period: 190 to 230 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Armour and similar soils: 90 percent Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Armour

Setting

Landform: Stream terraces

Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave, convex Across-slope shape: Linear, convex

Parent material: Silty alluvium over clayey residuum weathered from phosphatic

limestone

Typical profile

A - 0 to 19 inches: silt loam

Bt - 19 to 58 inches: silty clay loam

BC - 58 to 79 inches: clay

Properties and qualities

Slope: 2 to 5 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20

to 0.60 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Available water storage in profile: High (about 11.6 inches)

Interpretive groups

Land capability classification (irrigated): 2e Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: B Hydric soil rating: No

Minor Components

Byler

Percent of map unit: 4 percent Landform: Stream terraces

Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave, convex Across-slope shape: Linear, convex

Hydric soil rating: No

Arrington

Percent of map unit: 4 percent

Landform: Flood plains

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope

Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

Mimosa

Percent of map unit: 2 percent

Landform: Escarpments

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave, convex Across-slope shape: Linear, convex

Hydric soil rating: No

AmC2—Armour silt loam, 5 to 12 percent slopes

Map Unit Setting

National map unit symbol: 2td32

Elevation: 500 to 850 feet

Mean annual precipitation: 48 to 58 inches Mean annual air temperature: 57 to 61 degrees F

Frost-free period: 190 to 230 days

Farmland classification: Not prime farmland

Map Unit Composition

Armour and similar soils: 90 percent Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Armour

Setting

Landform: Stream terraces

Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave, convex Across-slope shape: Linear, convex

Parent material: Silty alluvium over clayey residuum weathered from phosphatic

limestone

Typical profile

A - 0 to 19 inches: silt loam

Bt - 19 to 58 inches: silty clay loam

BC - 58 to 79 inches: clay

Properties and qualities

Slope: 5 to 12 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20

to 0.60 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Available water storage in profile: High (about 11.6 inches)

Interpretive groups

Land capability classification (irrigated): 3e Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: B Hydric soil rating: No

Minor Components

Byler

Percent of map unit: 4 percent Landform: Stream terraces

Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave, convex Across-slope shape: Linear, convex

Hydric soil rating: No

Dellrose

Percent of map unit: 4 percent

Landform: Hillsides

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

Mimosa

Percent of map unit: 2 percent Landform: Escarpments

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave, convex Across-slope shape: Linear, convex

Hydric soil rating: No

ByB2—Byler silt loam, 2 to 5 percent slopes, eroded

Map Unit Setting

National map unit symbol: kpd6 Elevation: 400 to 700 feet

Mean annual precipitation: 48 to 55 inches Mean annual air temperature: 57 to 61 degrees F

Frost-free period: 190 to 205 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Byler and similar soils: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Byler

Setting

Landform: Stream terraces

Landform position (three-dimensional): Tread

Parent material: Loamy alluvium over clayey residuum weathered from limestone

Typical profile

H1 - 0 to 9 inches: silt loam
H2 - 9 to 24 inches: silt loam
H3 - 24 to 44 inches: silty clay loam
H4 - 44 to 60 inches: silty clay loam

Properties and qualities

Slope: 2 to 5 percent

Depth to restrictive feature: About 24 inches to fragipan

Natural drainage class: Moderately well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.06 to 0.20 in/hr)

Depth to water table: About 24 to 36 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Low (about 4.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C Hydric soil rating: No

En—Ennis gravelly silt loam, occasionally flooded

Map Unit Setting

National map unit symbol: kpd9 Elevation: 900 to 1,300 feet

Mean annual precipitation: 45 to 54 inches
Mean annual air temperature: 57 to 61 degrees F

Frost-free period: 180 to 205 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Ennis and similar soils: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Ennis

Setting

Landform: Flood plains

Landform position (three-dimensional): Tread

Parent material: Loamy alluvium derived from limestone, sandstone, and shale

Typical profile

H1 - 0 to 7 inches: gravelly silt loam H2 - 7 to 60 inches: gravelly silt loam

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: Occasional Frequency of ponding: None

Available water storage in profile: Moderate (about 7.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2w

Hydrologic Soil Group: A Hydric soil rating: No

HaC—Hawthorne gravelly silt loam, 5 to 12 percent slopes

Map Unit Setting

National map unit symbol: kpdf Elevation: 900 to 1,300 feet

Mean annual precipitation: 48 to 55 inches Mean annual air temperature: 57 to 61 degrees F

Frost-free period: 185 to 205 days

Farmland classification: Not prime farmland

Map Unit Composition

Hawthorne and similar soils: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hawthorne

Setting

Landform: Hillslopes

Landform position (three-dimensional): Crest

Parent material: Gravelly residuum weathered from limestone and siltstone

Typical profile

H1 - 0 to 6 inches: gravelly silt loam

H2 - 6 to 33 inches: very channery silt loam

Cr - 33 to 43 inches: bedrock

Properties and qualities

Slope: 5 to 12 percent

Depth to restrictive feature: 20 to 39 inches to paralithic bedrock

Natural drainage class: Somewhat excessively drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

high (0.00 to 0.20 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Low (about 3.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4s

Hydrologic Soil Group: B Hydric soil rating: No

HaD—Hawthorne gravelly silt loam, 12 to 20 percent slopes

Map Unit Setting

National map unit symbol: 2v59f Elevation: 350 to 1,070 feet

Mean annual precipitation: 48 to 58 inches
Mean annual air temperature: 57 to 69 degrees F

Frost-free period: 190 to 230 days

Farmland classification: Not prime farmland

Map Unit Composition

Hawthorne and similar soils: 88 percent

Minor components: 12 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hawthorne

Setting

Landform: Hillslopes

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Gravelly residuum weathered from limestone and siltstone

Typical profile

Oi - 0 to 1 inches: slightly decomposed plant material

A - 1 to 5 inches: gravelly silt loam
AE - 5 to 12 inches: gravelly silt loam
Bw - 12 to 18 inches: very gravelly silt loam
C - 18 to 26 inches: very gravelly silt loam

Cr - 26 to 36 inches: bedrock

Properties and qualities

Slope: 12 to 20 percent

Depth to restrictive feature: 20 to 30 inches to paralithic bedrock

Natural drainage class: Somewhat excessively drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.10 to 0.20 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Available water storage in profile: Very low (about 2.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B Hydric soil rating: No

Minor Components

Sugargrove

Percent of map unit: 6 percent

Landform: Hillsides

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

Dellrose

Percent of map unit: 4 percent

Landform: Hillsides

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Concave Across-slope shape: Linear

Hydric soil rating: No

Sengtown

Percent of map unit: 2 percent

Landform: Hills

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Hydric soil rating: No

HsF—Hawthorne-Sulphura association, steep

Map Unit Setting

National map unit symbol: kpdh Elevation: 600 to 1,300 feet

Mean annual precipitation: 48 to 55 inches Mean annual air temperature: 57 to 61 degrees F

Frost-free period: 185 to 205 days

Farmland classification: Not prime farmland

Map Unit Composition

Hawthorne and similar soils: 60 percent Sulphura and similar soils: 20 percent Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hawthorne

Setting

Landform: Hillslopes

Landform position (three-dimensional): Side slope

Parent material: Gravelly residuum weathered from limestone and siltstone

Typical profile

H1 - 0 to 6 inches: gravelly silt loam

H2 - 6 to 33 inches: very channery silt loam

Cr - 33 to 43 inches: bedrock

Properties and qualities

Slope: 20 to 60 percent

Depth to restrictive feature: 20 to 39 inches to paralithic bedrock

Natural drainage class: Somewhat excessively drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

high (0.00 to 0.20 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Low (about 3.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: B Hydric soil rating: No

Description of Sulphura

Setting

Landform: Hillslopes

Landform position (three-dimensional): Side slope

Parent material: Channery residuum weathered from limestone and shale

Typical profile

H1 - 0 to 10 inches: gravelly silt loam

H2 - 10 to 22 inches: very channery silt loam

R - 22 to 32 inches: bedrock

Properties and qualities

Slope: 20 to 60 percent

Depth to restrictive feature: 20 to 40 inches to lithic bedrock Natural drainage class: Somewhat excessively drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Very low (about 2.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: C Hydric soil rating: No

Minor Components

Minor components

Percent of map unit: 20 percent

Hydric soil rating: No

HuB—Humphreys gravelly silt loam, 2 to 5 percent slopes

Map Unit Setting

National map unit symbol: kpdj Elevation: 600 to 1,200 feet

Mean annual precipitation: 46 to 60 inches
Mean annual air temperature: 57 to 61 degrees F

Frost-free period: 180 to 205 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Humphreys and similar soils: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Humphreys

Setting

Landform: Stream terraces

Landform position (three-dimensional): Tread

Parent material: Loamy alluvium and/or colluvium derived from limestone

Typical profile

H1 - 0 to 8 inches: gravelly silt loam
H2 - 8 to 51 inches: gravelly silty clay loam
H3 - 51 to 60 inches: gravelly silty clay loam

Properties and qualities

Slope: 2 to 5 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00

in/hr)

Depth to water table: About 60 to 72 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Moderate (about 7.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: A Hydric soil rating: No

MnD2—Minvale gravelly silt loam, 12 to 20 percent slopes, eroded

Map Unit Setting

National map unit symbol: kpdp Elevation: 500 to 1,200 feet

Mean annual precipitation: 45 to 55 inches Mean annual air temperature: 57 to 61 degrees F

Frost-free period: 180 to 205 days

Farmland classification: Not prime farmland

Map Unit Composition

Minvale and similar soils: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Minvale

Setting

Landform: Hillslopes

Landform position (three-dimensional): Base slope

Parent material: Loamy colluvium derived from cherty limestone

Typical profile

H1 - 0 to 8 inches: gravelly silt loam H2 - 8 to 18 inches: gravelly silt loam

H3 - 18 to 60 inches: gravelly silty clay loam

Properties and qualities

Slope: 12 to 20 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to

high (0.60 to 2.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Moderate (about 8.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

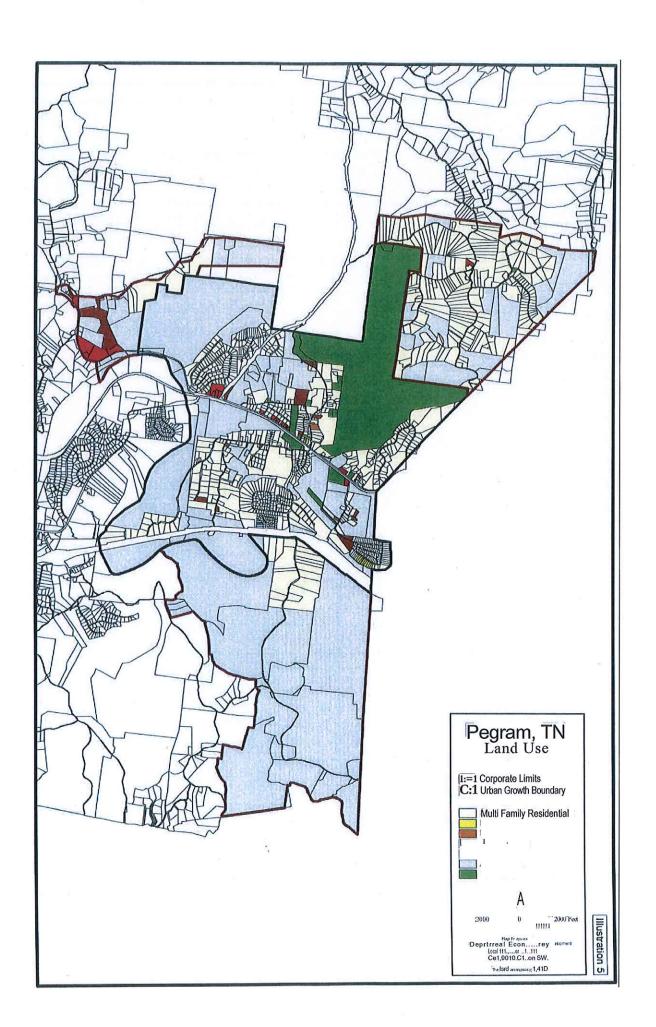
Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: B Hydric soil rating: No



ENCLOSURE (D)

LAND USE MAP





ENCLOSURE (E)

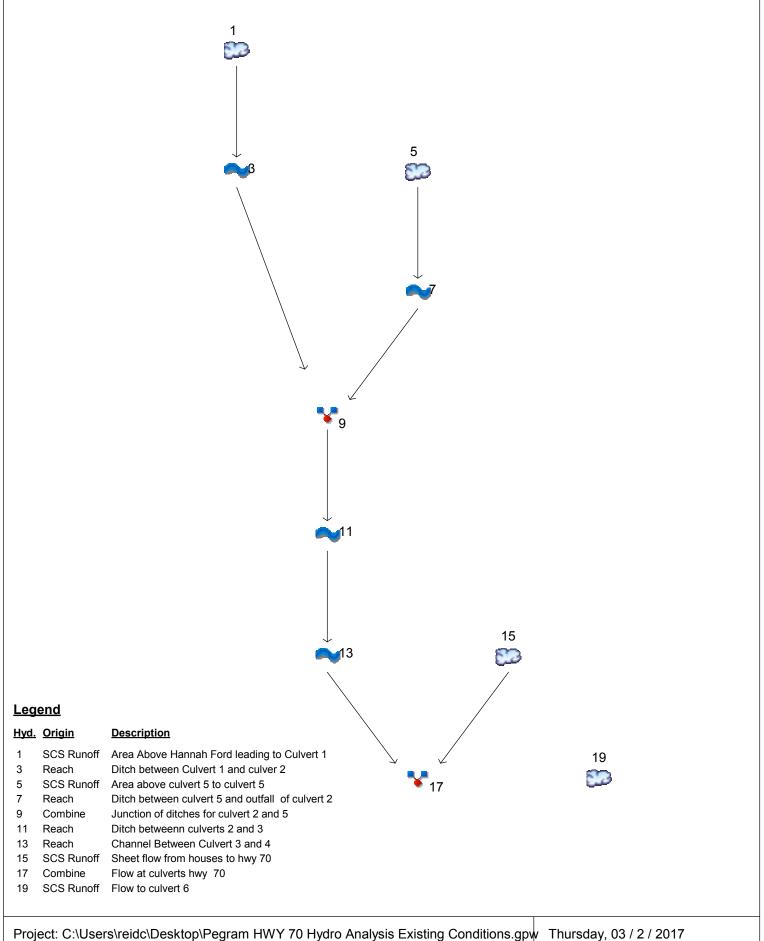
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Watershed Model Schematic



Hydrograph Return Period Recap Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

-	Hydrograph	Inflow				Peak Ou	tflow (cfs)				Hydrograph
0.	type (origin)	hyd(s)	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	Description
1	SCS Runoff			19.31		44.33	69.68	112.65	150.27	192.30	Area Above Hannah Ford leading to
3	Reach	1		19.31		44.38	69.68	112.65	150.52	192.53	Ditch between Culvert 1 and culver 2
5	SCS Runoff			11.25		21.71	31.32	46.54	59.46	73.57	Area above culvert 5 to culvert 5
7	Reach	5		11.24		21.72	31.35	46.56	59.47	73.68	Ditch between culvert 5 and outfall or
9	Combine	3, 7,		25.21		55.60	85.98	137.16	182.11	231.88	Junction of ditches for culvert 2 and 5
11	Reach	9		24.73		54.96	85.22	136.38	181.23	230.94	Ditch betweenn culverts 2 and 3
13	Reach	11		24.49		54.60	84.84	135.91	180.75	230.39	Channel Between Culvert 3 and 4
15	SCS Runoff			12.98		20.93	27.87	38.53	47.37	56.85	Sheet flow from houses to hwy 70
17	Combine	13, 15,		37.38		75.52	112.71	174.39	228.03	287.05	Flow at culverts hwy 70
19	SCS Runoff			5.886		9.331	12.30	16.91	20.75	24.86	Flow to culvert 6

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Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	19.31	1	739	153,782				Area Above Hannah Ford leading to
3	Reach	19.31	1	740	153,781	1			Ditch between Culvert 1 and culver 2
5	SCS Runoff	11.25	1	725	42,927				Area above culvert 5 to culvert 5
7	Reach	11.24	1	726	42,926	5			Ditch between culvert 5 and outfall of
9	Combine	25.21	1	736	196,707	3, 7,			Junction of ditches for culvert 2 and 5
11	Reach	24.73	1	739	196,705	9			Ditch betweenn culverts 2 and 3
13	Reach	24.49	1	741	196,704	11			Channel Between Culvert 3 and 4
15	SCS Runoff	12.98	1	739	71,713				Sheet flow from houses to hwy 70
17	Combine	37.38	1	741	268,417	13, 15,			Flow at culverts hwy 70
19	SCS Runoff	5.886	2	726	20,177				Flow to culvert 6

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Hydrograph Report

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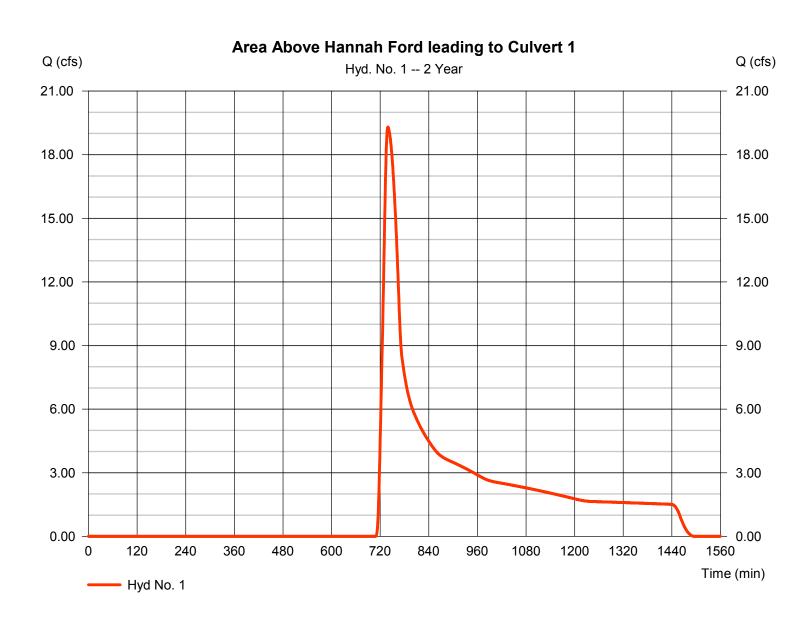
Thursday, 03 / 2 / 2017

Hyd. No. 1

Area Above Hannah Ford leading to Culvert 1

Hydrograph type = SCS Runoff Peak discharge = 19.31 cfsStorm frequency Time to peak = 739 min = 2 yrsTime interval = 1 min Hyd. volume = 153.782 cuft Curve number = 56* Drainage area = 100.000 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 34.70 min = TR55 Total precip. Distribution = Type II = 3.62 inStorm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = [(17.000 x 36) + (83.000 x 60)] / 100.000



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5 $\,$

Hyd. No. 1Area Above Hannah Ford leading to Culvert 1

<u>Description</u>	A		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.400 = 150.0 = 3.62 = 5.00		0.400 0.0 3.62 0.00		0.050 0.0 3.62 0.00		
Travel Time (min)	= 19.36	+	0.00	+	0.00	=	19.36
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 1610.00 = 4.00 = Unpaved =3.23		0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 8.32	+	0.00	+	0.00	=	8.32
, ,			0.00		0.00		
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 12.00 = 8.00 = 2.00 = 0.050 =5.53		0.00 0.00 0.00 0.015 0.00		0.00 0.00 0.00 0.015		
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value	= 12.00 = 8.00 = 2.00 = 0.050		0.00 0.00 0.00 0.015		0.00 0.00 0.00 0.015		
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 12.00 = 8.00 = 2.00 = 0.050 =5.53	+	0.00 0.00 0.00 0.015 0.00	+	0.00 0.00 0.00 0.015	=	7.07

Hydrograph Report

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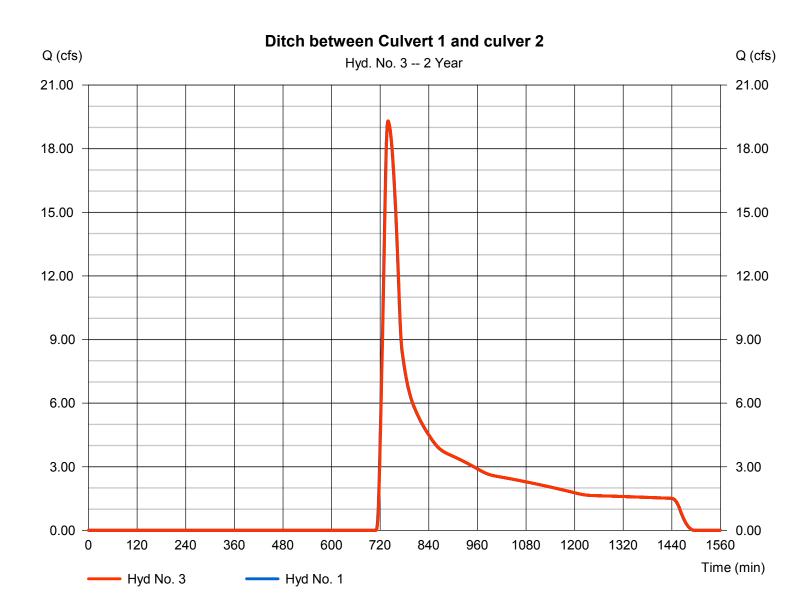
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Hyd. No. 3

Ditch between Culvert 1 and culver 2

= Reach Peak discharge = 19.31 cfsHydrograph type Storm frequency = 2 yrs Time to peak = 740 min Time interval = 1 min Hyd. volume = 153.781 cuft = 1 - Area Above Hannah Ford leachtigrtdy@elvert 1 Inflow hyd. No. = Trapezoidal Channel slope Reach length = 1.8 % = 118.0 ftBottom width = 3.0 ftManning's n = 0.030Side slope Max. depth = 5.0 ft= 3.0:1Rating curve x Rating curve m = 3.202= 1.279Ave. velocity = 4.74 ft/sRouting coeff. = 1.2129

Modified Att-Kin routing method used.



Hydrograph Report

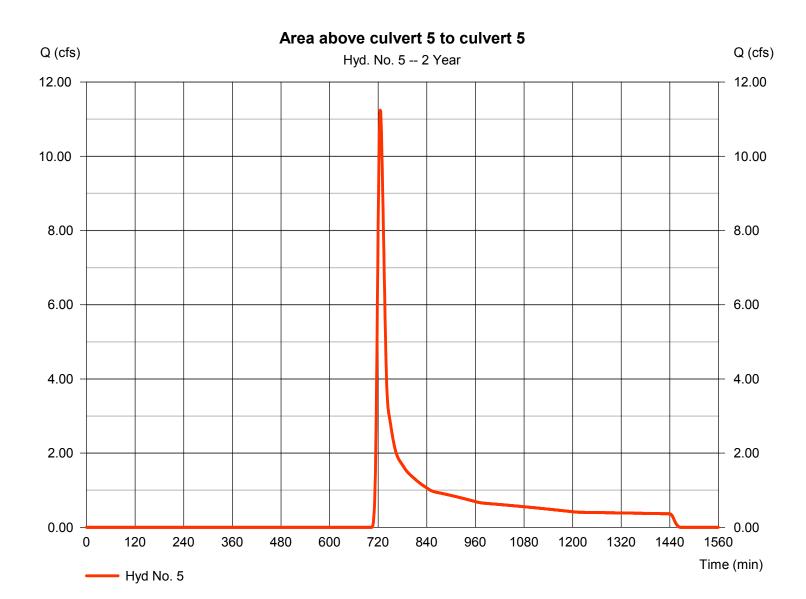
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Hyd. No. 5

Area above culvert 5 to culvert 5

= 11.25 cfsHydrograph type = SCS Runoff Peak discharge Storm frequency = 2 yrsTime to peak = 725 min Time interval = 1 min Hyd. volume = 42,927 cuft Drainage area Curve number = 20.000 ac= 60 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 16.77 min = TR55 Total precip. = 3.62 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Hyd. No. 5Area above culvert 5 to culvert 5

<u>Description</u>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>	
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%) Travel Time (min)	= 0.400 = 150.0 = 3.62 = 14.00 = 12.82	+	0.011 0.0 0.00 0.00	+	0.011 0.0 0.00 0.00	=	12.82	
Shallow Concentrated Flow								
Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 1350.00 = 12.50 = Unpaved =5.70	d	0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00			
Travel Time (min)	= 3.94	+	0.00	+	0.00	=	3.94	
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 0.00 = 0.00 = 0.00 = 0.015 =0.00		0.00 0.00 0.00 0.015 0.00		0.00 0.00 0.00 0.015			
Flow length (ft)	({0})0.0		0.0		0.0			
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00	
Total Travel Time, Tc								

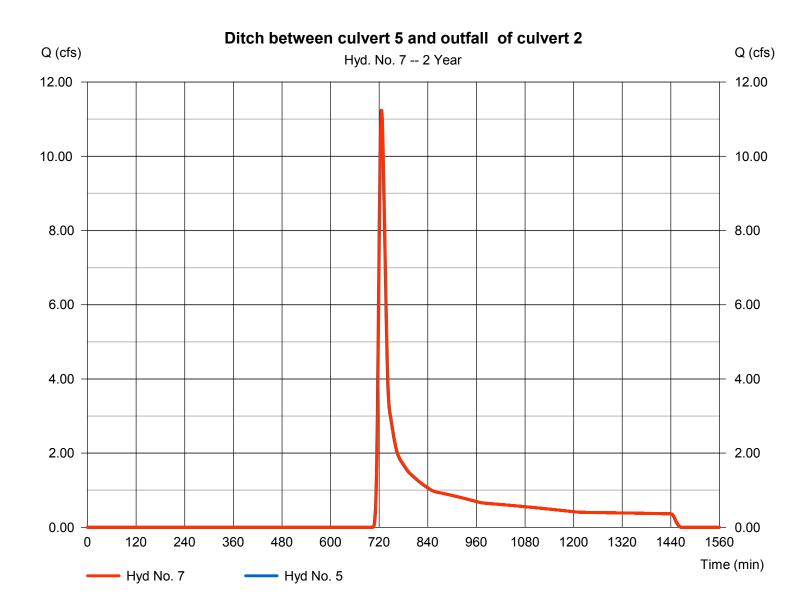
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Hyd. No. 7

Ditch between culvert 5 and outfall of culvert 2

= Reach Peak discharge = 11.24 cfsHydrograph type Storm frequency = 2 yrs Time to peak = 726 min Time interval = 1 min Hyd. volume = 42.926 cuft Inflow hyd. No. = 5 - Area above culvert 5 to c = Trapezoidal Reach length Channel slope = 3.8 % = 174.0 ftBottom width = 3.0 ftManning's n = 0.040Side slope Max. depth = 2.0 ft= 2.0:1Rating curve x = 3.490Rating curve m = 1.249Ave. velocity = 4.41 ft/sRouting coeff. = 0.9741



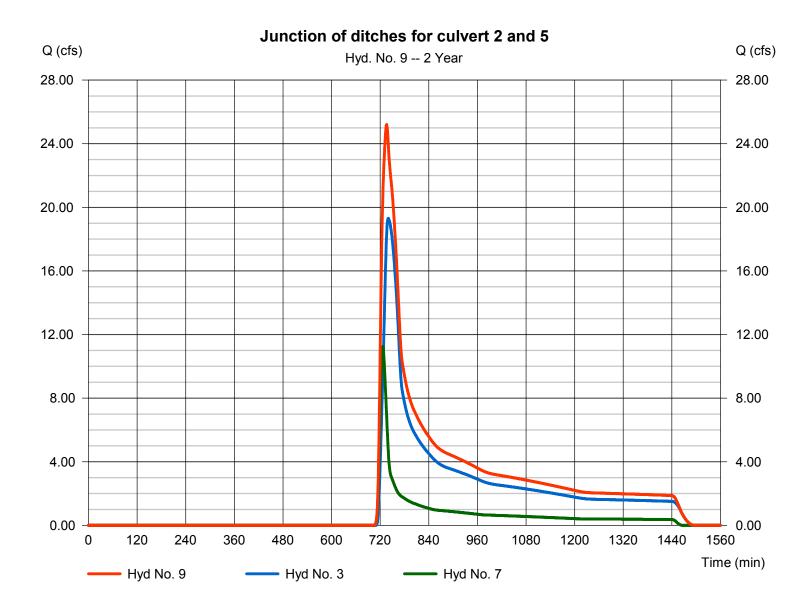
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Hyd. No. 9

Junction of ditches for culvert 2 and 5

Hydrograph type = Combine Peak discharge = 25.21 cfsStorm frequency Time to peak = 2 yrs= 736 min Time interval = 1 min Hyd. volume = 196,707 cuft Inflow hyds. = 3, 7 Contrib. drain. area = 0.000 ac



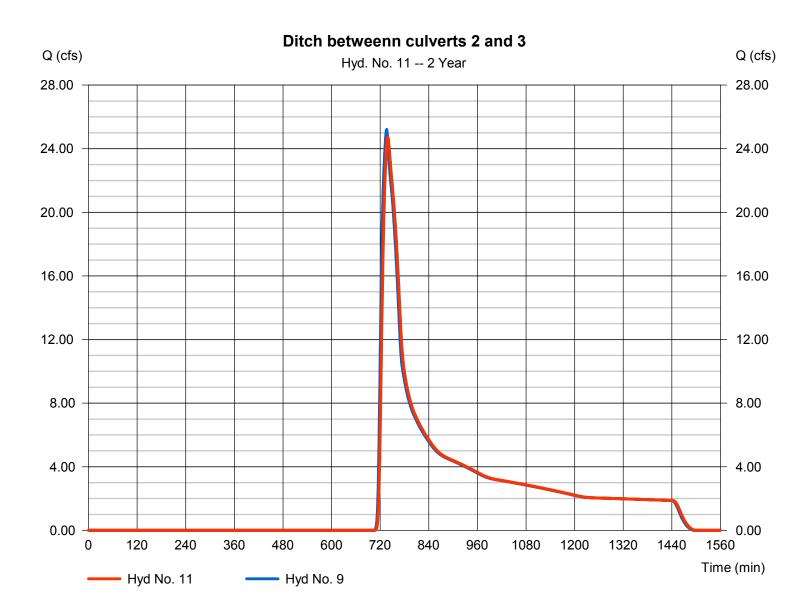
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Thursday, 03 / 2 / 2017

Hyd. No. 11

Ditch betweenn culverts 2 and 3

Hydrograph type = Reach Peak discharge = 24.73 cfsStorm frequency = 2 yrs Time to peak = 739 min Time interval = 1 min Hyd. volume = 196,705 cuft= 9 - Junction of ditches for culveste2tamdtspe Inflow hyd. No. = Trapezoidal Reach length Channel slope = 2.3 % = 815.0 ftBottom width = 5.0 ftManning's n = 0.040Side slope Max. depth = 3.0:1= 5.0 ftRating curve x Rating curve m = 1.341= 1.931Ave. velocity = 3.71 ft/sRouting coeff. = 0.3097



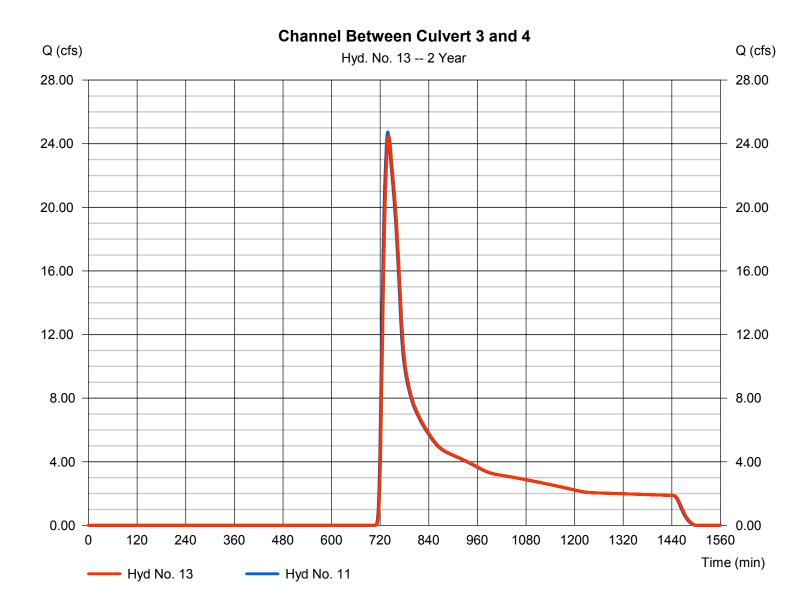
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Thursday, 03 / 2 / 2017

Hyd. No. 13

Channel Between Culvert 3 and 4

Hydrograph type Peak discharge = 24.49 cfs= Reach Storm frequency = 2 yrs Time to peak = 741 min Time interval = 1 min Hyd. volume = 196.704 cuft Inflow hyd. No. = 11 - Ditch betweenn culverts 2 Spection type = Trapezoidal Channel slope = 1.2 % Reach length = 450.0 ftBottom width = 5.0 ftManning's n = 0.040Side slope Max. depth = 3.0 ft= 3.0:1Rating curve x Rating curve m = 1.395= 1.321Ave. velocity Routing coeff. = 0.3961= 2.80 ft/s



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Hyd. No. 15

Sheet flow from houses to hwy 70

Hydrograph type = SCS Runoff Peak discharge = 12.98 cfsStorm frequency = 2 yrsTime to peak = 739 min Time interval = 1 min Hyd. volume = 71,713 cuft Drainage area Curve number = 20.330 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 39.60 min = TR55 Total precip. = 3.62 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



TR55 Tc Worksheet

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5 $\,$

Hyd. No. 15Sheet flow from houses to hwy 70

<u>Description</u>	<u>A</u>		<u>B</u>		<u>c</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.400 = 150.0 = 3.62 = 2.00		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 27.93	+	0.00	+	0.00	=	27.93
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 1602.00 = 2.00 = Unpaved =2.28	i	0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 11.70	+	0.00	+	0.00	=	11.70
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 10.00 = 9.00 = 5.00 = 0.025 =14.30		0.00 0.00 0.00 0.015 0.00		0.00 0.00 0.00 0.015		
Flow length (ft)	({0})0.0		0.0		0.0		
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc							39.60 min

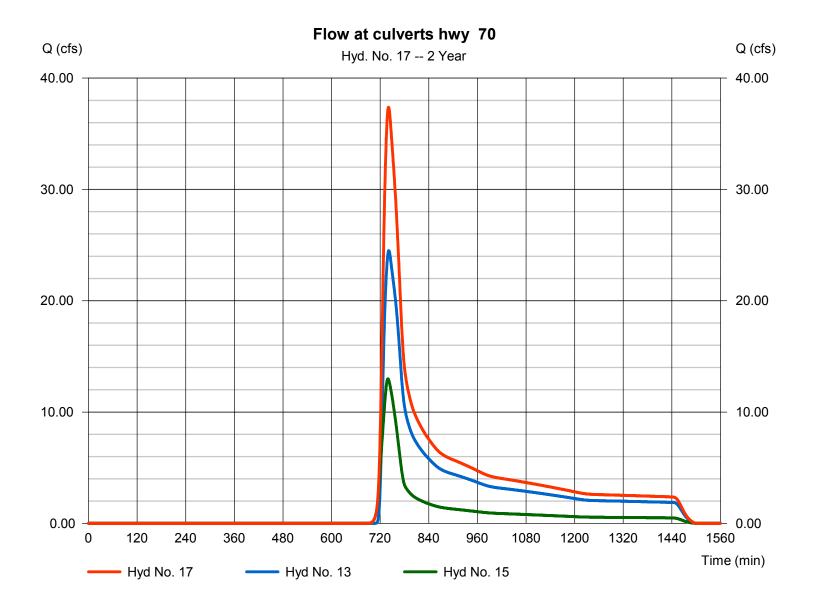
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 17

Flow at culverts hwy 70

Hydrograph type = Combine Peak discharge = 37.38 cfsStorm frequency Time to peak = 2 yrs= 741 min Time interval = 1 min Hyd. volume = 268,417 cuft Inflow hyds. = 13, 15 Contrib. drain. area = 20.330 ac



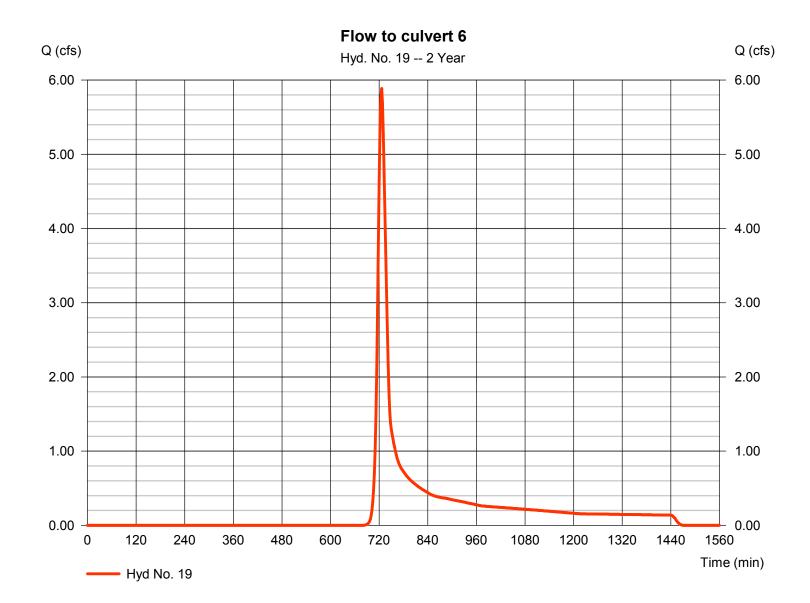
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Hyd. No. 19

Flow to culvert 6

Hydrograph type = SCS Runoff Peak discharge = 5.886 cfsStorm frequency = 2 yrsTime to peak = 726 min Time interval = 2 min Hyd. volume = 20,177 cuft Drainage area Curve number = 5.720 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = TR55 $= 17.80 \, \text{min}$ Total precip. Distribution = Type II = 3.62 inStorm duration = 24 hrs Shape factor = 484



TR55 Tc Worksheet

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Hyd. No. 19

Flow to culvert 6

Total Travel Time, Tc											
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00				
Flow length (ft)	({0})0.0		0.0		0.0						
			0.00		0.00						
X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 0.00 = 0.00 = 0.00 = 0.015 =0.00		0.00 0.00 0.00 0.015		0.00 0.00 0.00 0.015						
Travel Time (min) Channel Flow	= 6.48	+	0.00	+	0.00	=	6.48				
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 1030.00 = 2.70 = Unpaved =2.65		0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00						
Travel Time (min)	= 11.30	+	0.00	+	0.00	=	11.30				
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.150 = 150.0 = 3.62 = 2.70		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00						
<u>Description</u>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>				

Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	44.33	1	737	273,458				Area Above Hannah Ford leading to
3	Reach	44.38	1	738	273,458	1			Ditch between Culvert 1 and culver 2
5	SCS Runoff	21.71	1	724	71,414				Area above culvert 5 to culvert 5
7	Reach	21.72	1	725	71,413	5			Ditch between culvert 5 and outfall of
9	Combine	55.60	1	735	344,872	3, 7,			Junction of ditches for culvert 2 and 5
11	Reach	54.96	1	737	344,870	9			Ditch betweenn culverts 2 and 3
13	Reach	54.60	1	739	344,869	11			Channel Between Culvert 3 and 4
15	SCS Runoff	20.93	1	738	108,627				Sheet flow from houses to hwy 70
17	Combine	75.52	1	739	453,496	13, 15,			Flow at culverts hwy 70
19	SCS Runoff	9.331	2	726	30,563				Flow to culvert 6

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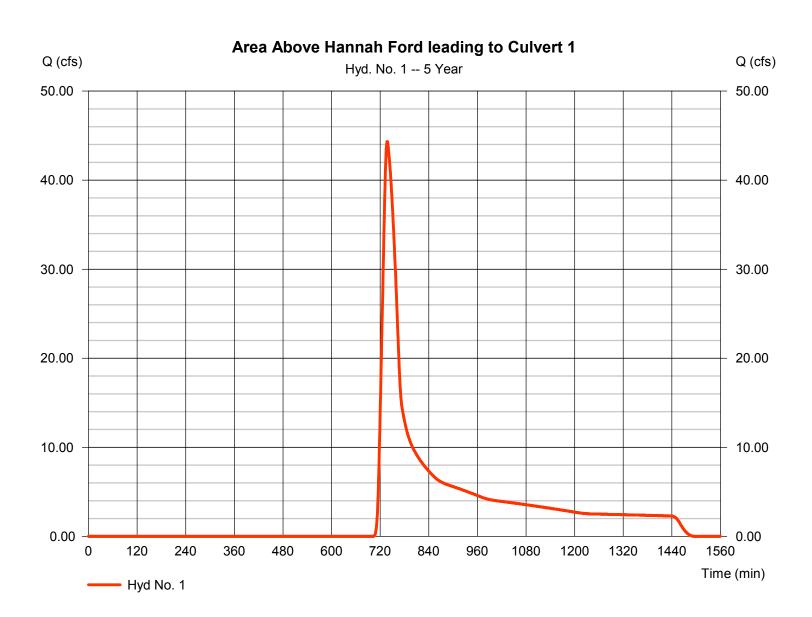
Thursday, 03 / 2 / 2017

Hyd. No. 1

Area Above Hannah Ford leading to Culvert 1

= SCS Runoff Peak discharge = 44.33 cfsHydrograph type Storm frequency Time to peak = 737 min = 5 yrsTime interval = 1 min Hyd. volume = 273.458 cuft Curve number Drainage area = 100.000 ac= 56* Basin Slope = 0.0 %Hydraulic length = 0 ftTime of conc. (Tc) = 34.70 min Tc method = TR55 Total precip. Distribution = Type II = 4.41 inShape factor Storm duration = 484 = 24 hrs

^{*} Composite (Area/CN) = $[(17.000 \times 36) + (83.000 \times 60)] / 100.000$



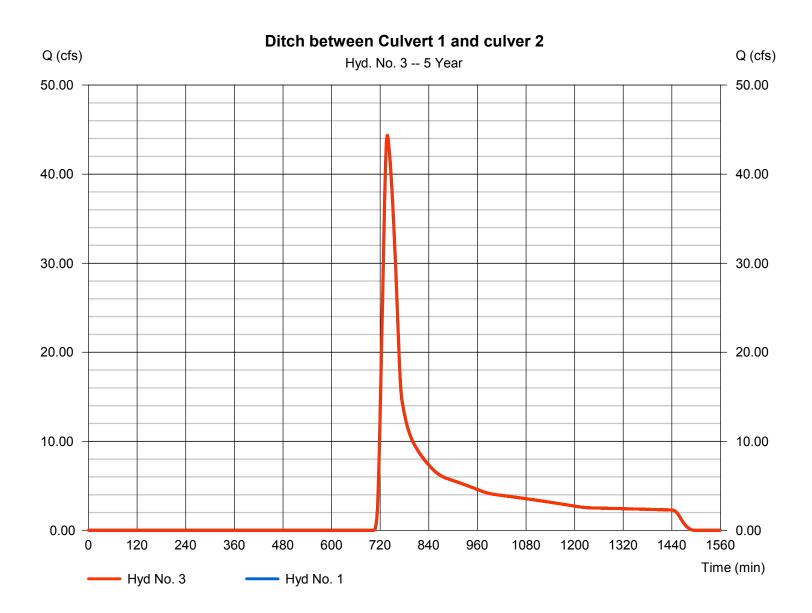
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 3

Ditch between Culvert 1 and culver 2

= Reach Peak discharge = 44.38 cfsHydrograph type Storm frequency = 5 yrsTime to peak = 738 min Time interval = 1 min Hyd. volume = 273.458 cuft = 1 - Area Above Hannah Ford leaching not your 1 Inflow hyd. No. = Trapezoidal Channel slope Reach length = 1.8 % = 118.0 ftBottom width = 3.0 ftManning's n = 0.030Side slope Max. depth = 3.0:1= 5.0 ftRating curve x Rating curve m = 3.202= 1.279Ave. velocity Routing coeff. = 1.2975= 5.68 ft/s



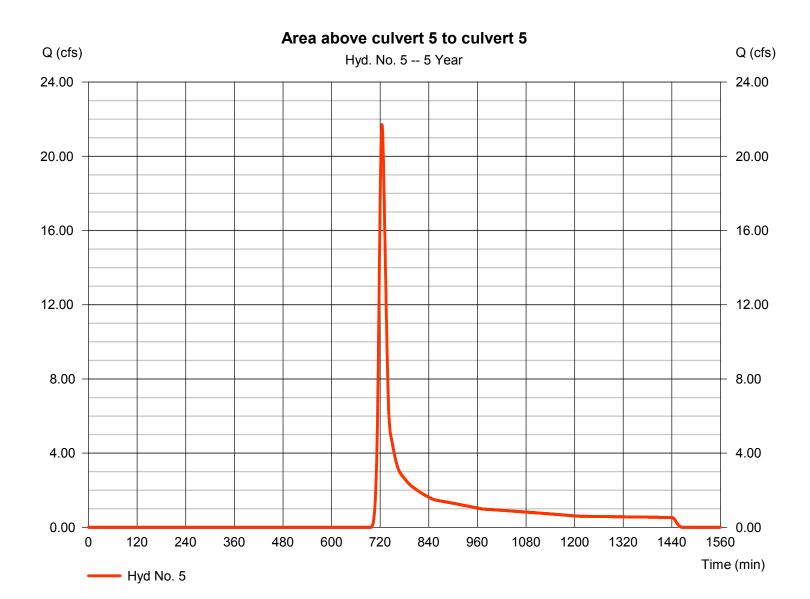
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 5

Area above culvert 5 to culvert 5

Hydrograph type = SCS Runoff Peak discharge = 21.71 cfsStorm frequency = 5 yrsTime to peak = 724 min = 71,414 cuft Time interval = 1 min Hyd. volume Drainage area Curve number = 20.000 ac= 60 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 16.77 min = TR55 Total precip. = 4.41 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



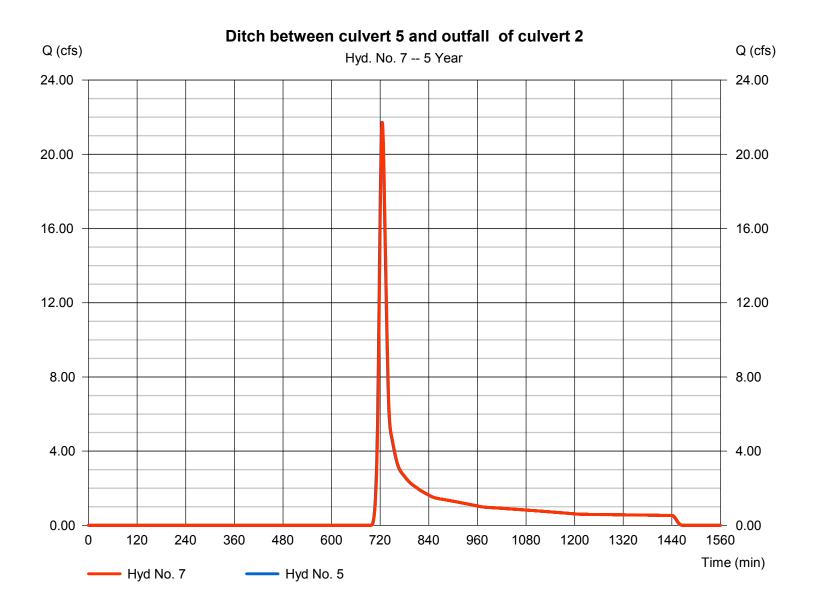
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 7

Ditch between culvert 5 and outfall of culvert 2

= Reach Peak discharge = 21.72 cfsHydrograph type Storm frequency Time to peak = 725 min = 5 yrsTime interval = 1 min Hyd. volume = 71.413 cuft Inflow hyd. No. = 5 - Area above culvert 5 to c = Trapezoidal Reach length Channel slope = 3.8 % = 174.0 ftBottom width = 3.0 ftManning's n = 0.040Side slope Max. depth = 2.0:1= 2.0 ftRating curve x Rating curve m = 1.249= 3.490Ave. velocity Routing coeff. = 5.03 ft/s= 1.0398



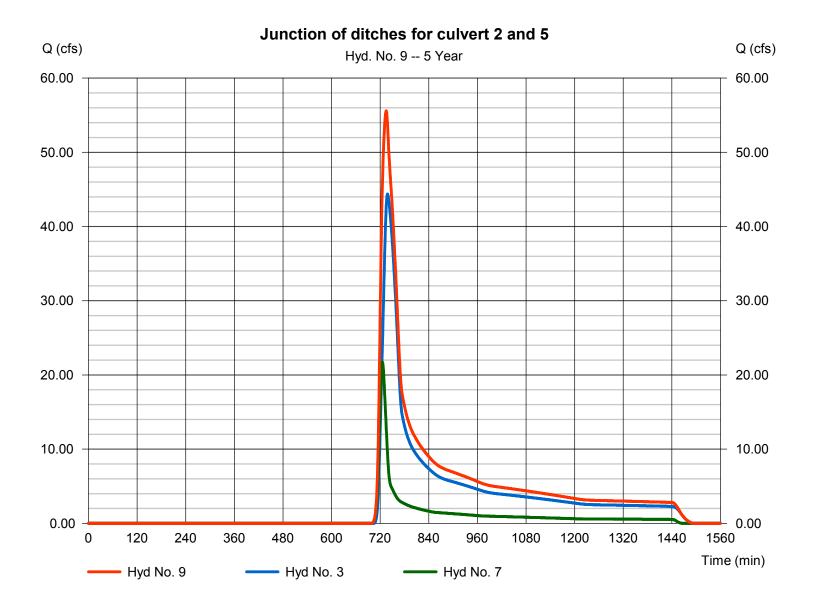
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Thursday, 03 / 2 / 2017

Hyd. No. 9

Junction of ditches for culvert 2 and 5

Hydrograph type = Combine Peak discharge = 55.60 cfsStorm frequency Time to peak = 5 yrs= 735 min Time interval = 1 min Hyd. volume = 344,872 cuft Inflow hyds. = 3, 7 Contrib. drain. area = 0.000 ac



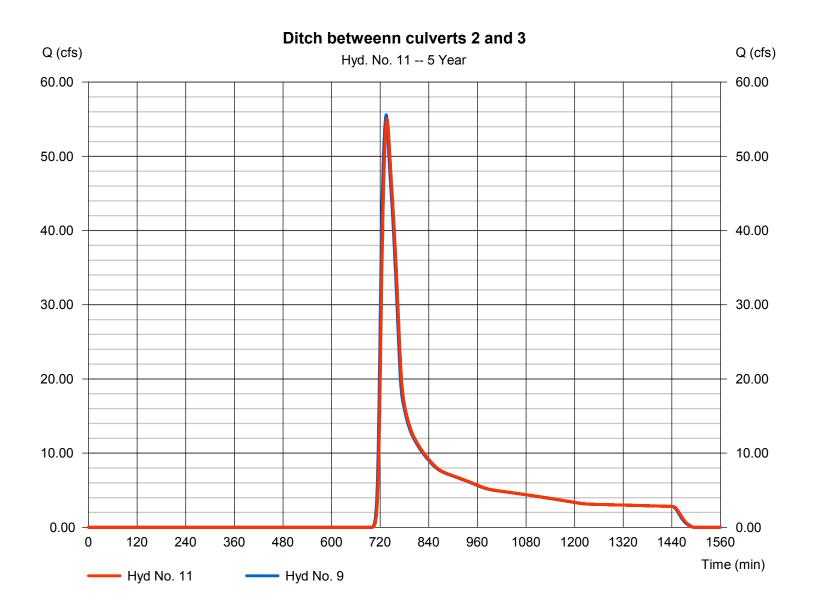
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Thursday, 03 / 2 / 2017

Hyd. No. 11

Ditch betweenn culverts 2 and 3

Peak discharge = Reach = 54.96 cfsHydrograph type Storm frequency = 5 yrsTime to peak = 737 min Time interval = 1 min Hyd. volume = 344.870 cuft = 9 - Junction of ditches for culveste2tamdtspe Inflow hyd. No. = Trapezoidal Reach length = 815.0 ftChannel slope = 2.3 % Bottom width = 5.0 ftManning's n = 0.040Side slope Max. depth = 3.0:1= 5.0 ftRating curve x Rating curve m = 1.341= 1.931Ave. velocity = 4.54 ft/sRouting coeff. = 0.3661



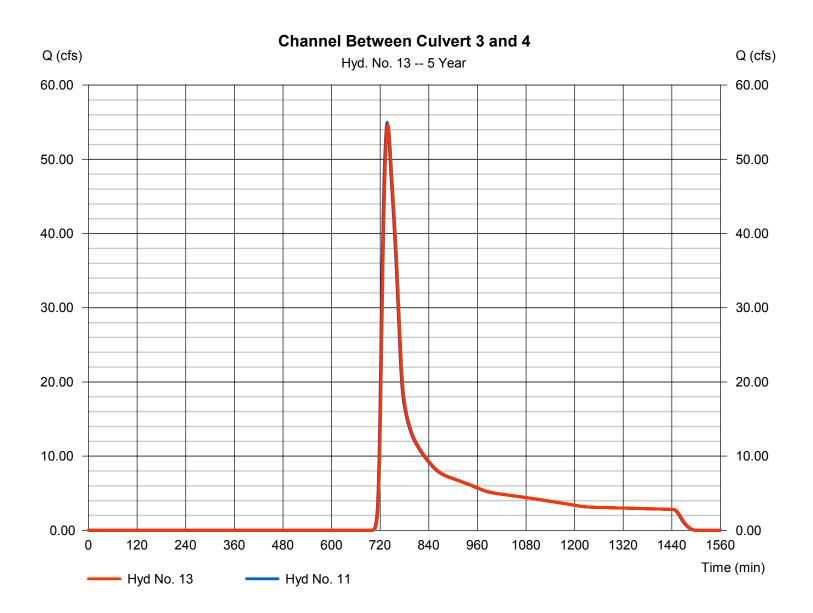
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Thursday, 03 / 2 / 2017

Hyd. No. 13

Channel Between Culvert 3 and 4

Peak discharge Hydrograph type = 54.60 cfs= Reach Storm frequency = 5 yrsTime to peak = 739 min Time interval = 1 min Hyd. volume = 344.869 cuft Inflow hyd. No. = 11 - Ditch betweenn culverts 2 Saedtion type = Trapezoidal Reach length = 450.0 ftChannel slope = 1.2 % Bottom width = 5.0 ftManning's n = 0.040Side slope Max. depth = 3.0 ft= 3.0:1Rating curve x Rating curve m = 1.395= 1.321Ave. velocity Routing coeff. = 0.4613= 3.40 ft/s



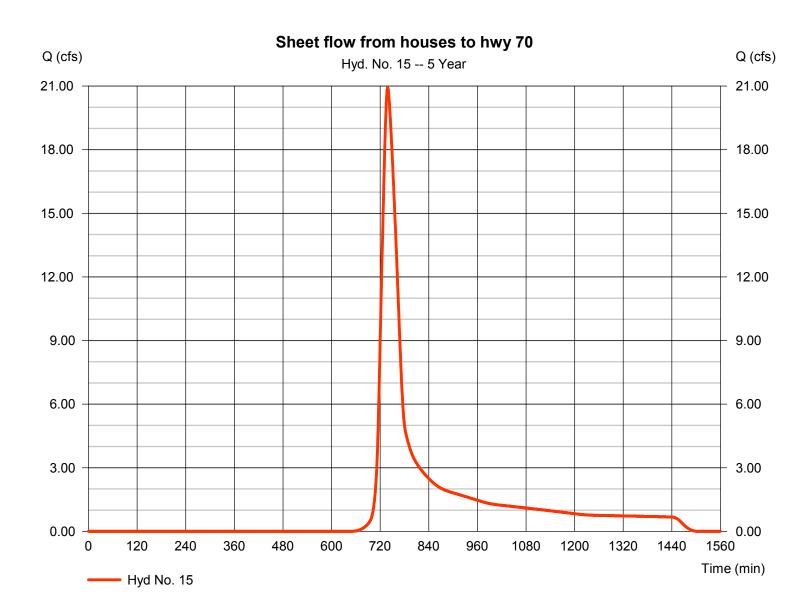
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Thursday, 03 / 2 / 2017

Hyd. No. 15

Sheet flow from houses to hwy 70

Hydrograph type = SCS Runoff Peak discharge = 20.93 cfsStorm frequency = 5 yrsTime to peak = 738 min Time interval = 1 min Hyd. volume = 108,627 cuft Drainage area Curve number = 20.330 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 39.60 min = TR55 Total precip. = 4.41 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



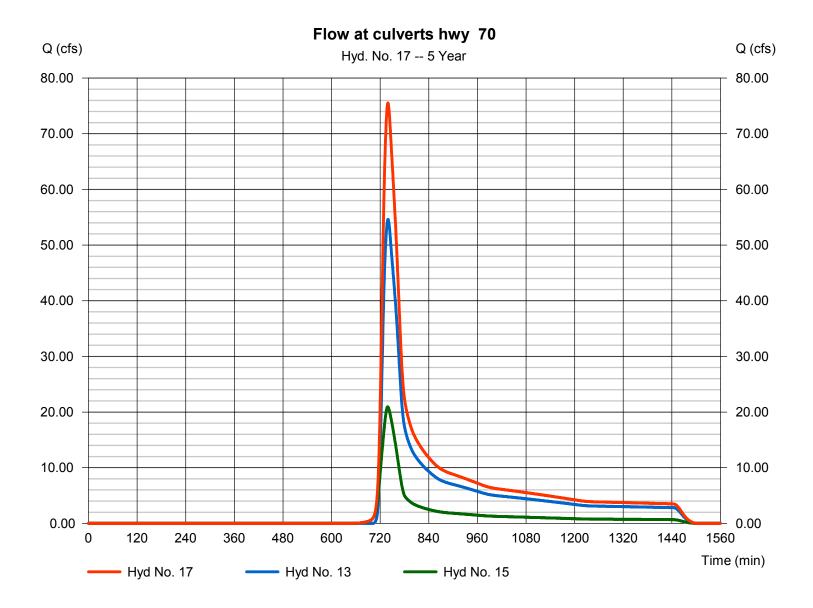
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Thursday, 03 / 2 / 2017

Hyd. No. 17

Flow at culverts hwy 70

Hydrograph type = Combine Peak discharge = 75.52 cfsStorm frequency Time to peak = 5 yrs= 739 min Time interval = 1 min Hyd. volume = 453,496 cuft Inflow hyds. = 13, 15 Contrib. drain. area = 20.330 ac



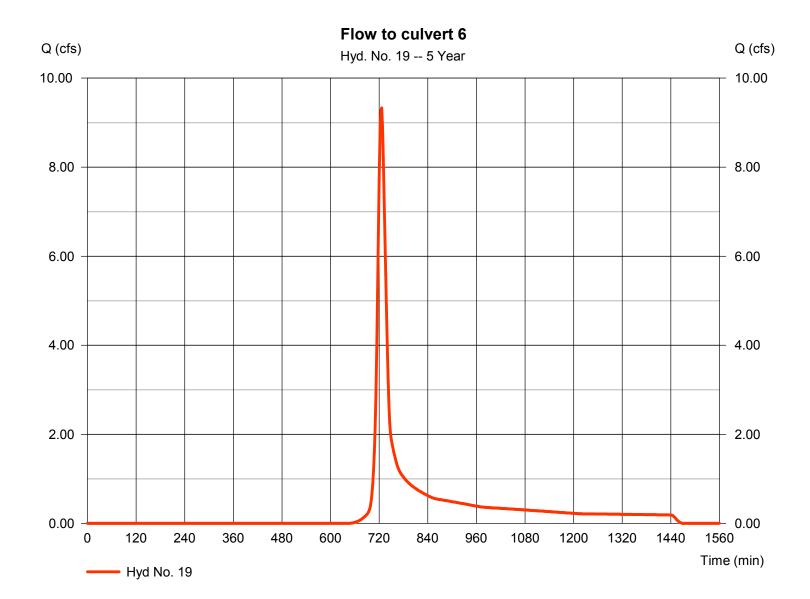
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Thursday, 03 / 2 / 2017

Hyd. No. 19

Flow to culvert 6

Hydrograph type = SCS Runoff Peak discharge = 9.331 cfsStorm frequency = 5 yrsTime to peak = 726 min Time interval = 2 min Hyd. volume = 30.563 cuft Drainage area = 5.720 acCurve number = 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 17.80 min = TR55 Total precip. = 4.41 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

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Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	69.68	1	737	385,603				Area Above Hannah Ford leading to
3	Reach	69.68	1	738	385,602	1			Ditch between Culvert 1 and culver 2
5	SCS Runoff	31.32	1	724	97,360				Area above culvert 5 to culvert 5
7	Reach	31.35	1	725	97,359	5			Ditch between culvert 5 and outfall of
9	Combine	85.98	1	734	482,962	3, 7,			Junction of ditches for culvert 2 and 5
11	Reach	85.22	1	736	482,960	9			Ditch betweenn culverts 2 and 3
13	Reach	84.84	1	738	482,960	11			Channel Between Culvert 3 and 4
15	SCS Runoff	27.87	1	738	140,815				Sheet flow from houses to hwy 70
17	Combine	112.71	1	738	623,775	13, 15,			Flow at culverts hwy 70
19	SCS Runoff	12.30	2	726	39,619				Flow to culvert 6

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= 24 hrs

Thursday, 03 / 2 / 2017

= 484

Hyd. No. 1

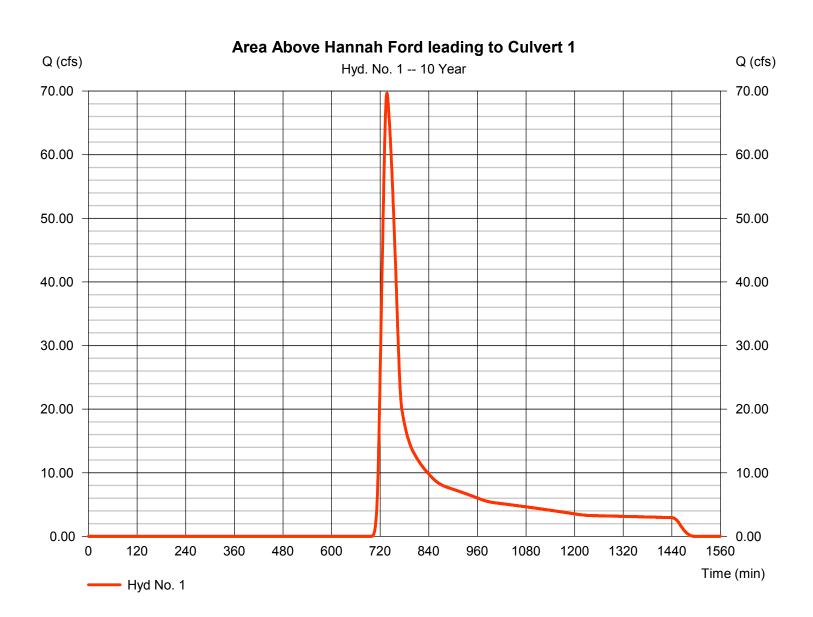
Storm duration

Area Above Hannah Ford leading to Culvert 1

= SCS Runoff Peak discharge = 69.68 cfsHydrograph type Storm frequency = 10 yrsTime to peak = 737 min Time interval = 1 min Hyd. volume = 385.603 cuft Curve number Drainage area = 100.000 ac= 56* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 34.70 min = TR55 Total precip. Distribution = Type II = 5.04 in

Shape factor

^{*} Composite (Area/CN) = [(17.000 x 36) + (83.000 x 60)] / 100.000



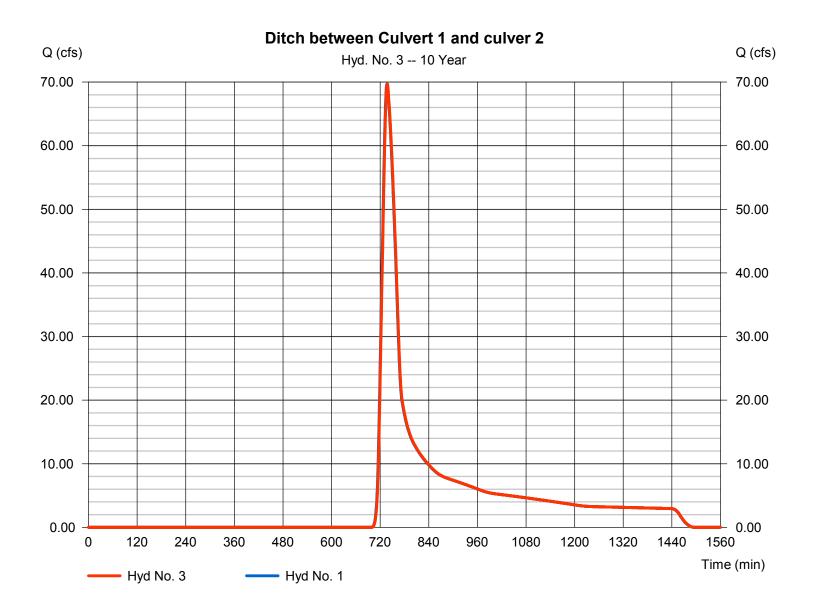
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Thursday, 03 / 2 / 2017

Hyd. No. 3

Ditch between Culvert 1 and culver 2

= Reach Peak discharge = 69.68 cfsHydrograph type Storm frequency = 10 yrsTime to peak = 738 min Time interval = 1 min Hyd. volume = 385.602 cuft = 1 - Area Above Hannah Ford leachtigrtdy@elvert 1 Inflow hyd. No. = Trapezoidal Channel slope Reach length = 1.8 % = 118.0 ftBottom width = 3.0 ftManning's n = 0.030Side slope Max. depth = 5.0 ft= 3.0:1Rating curve x Rating curve m = 3.202= 1.279Ave. velocity = 6.27 ft/sRouting coeff. = 1.3418



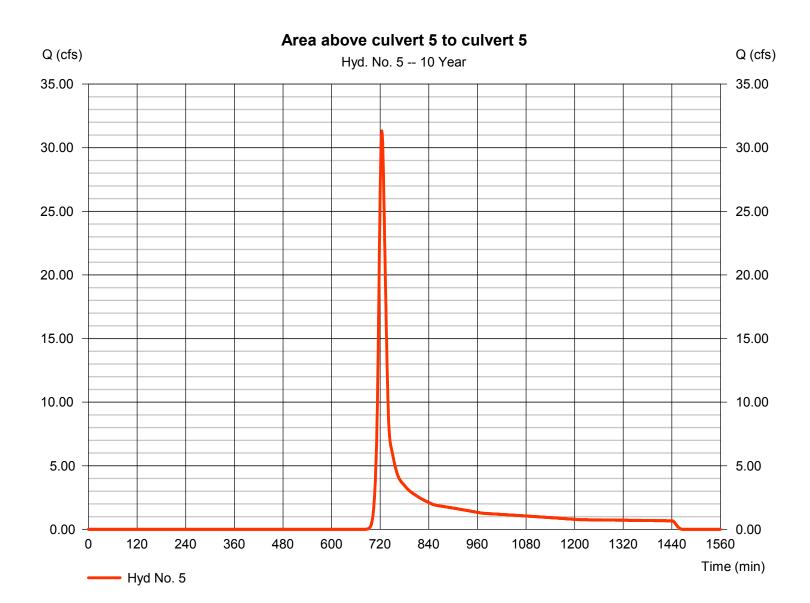
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Thursday, 03 / 2 / 2017

Hyd. No. 5

Area above culvert 5 to culvert 5

Hydrograph type = SCS Runoff Peak discharge = 31.32 cfsStorm frequency = 10 yrsTime to peak = 724 min Time interval = 1 min Hyd. volume = 97,360 cuftDrainage area Curve number = 20.000 ac= 60 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 16.77 min = TR55 Total precip. = 5.04 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



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= 5.41 ft/s

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= 1.0762

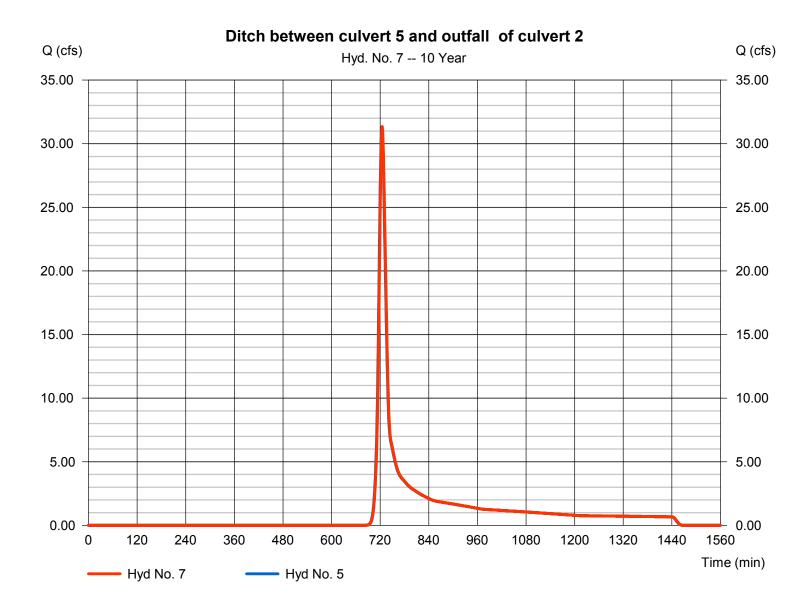
Hyd. No. 7

Ave. velocity

Ditch between culvert 5 and outfall of culvert 2

= Reach Peak discharge = 31.35 cfsHydrograph type Storm frequency = 10 yrsTime to peak = 725 min Time interval = 1 min Hyd. volume = 97.359 cuft Inflow hyd. No. = 5 - Area above culvert 5 to c = Trapezoidal Reach length = 174.0 ftChannel slope = 3.8 % Bottom width = 3.0 ftManning's n = 0.040Side slope Max. depth = 2.0 ft= 2.0:1Rating curve x Rating curve m = 1.249= 3.490

Routing coeff.



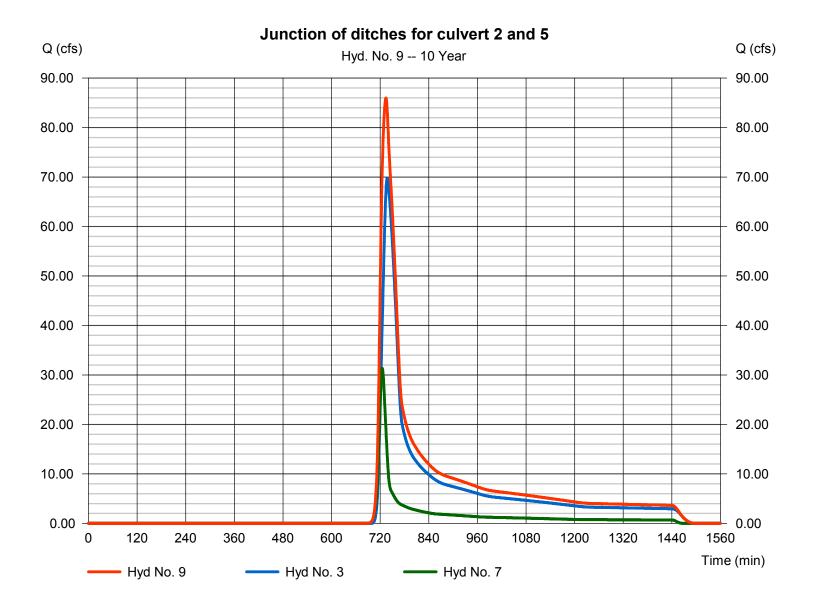
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Thursday, 03 / 2 / 2017

Hyd. No. 9

Junction of ditches for culvert 2 and 5

Hydrograph type = Combine Peak discharge = 85.98 cfsStorm frequency Time to peak = 10 yrs= 734 min = 482,962 cuft Time interval = 1 min Hyd. volume Inflow hyds. = 3, 7 Contrib. drain. area = 0.000 ac



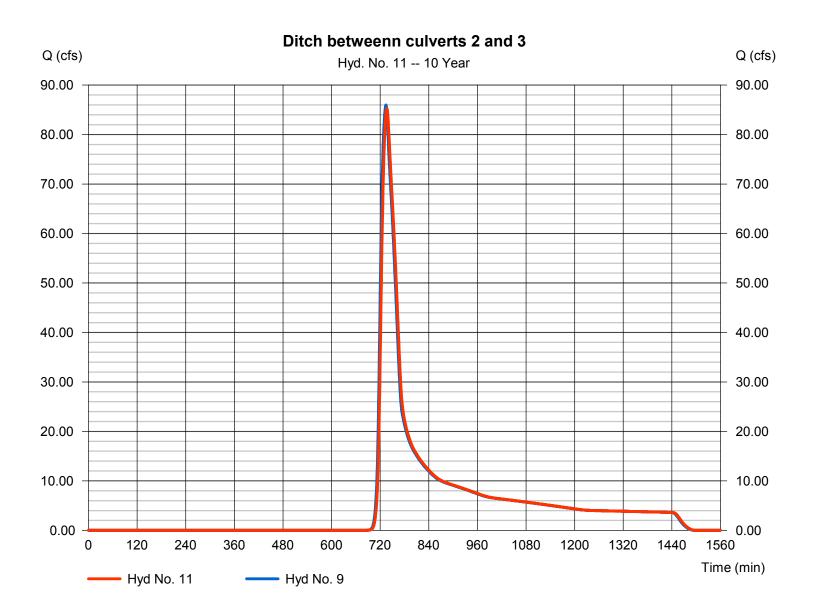
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Thursday, 03 / 2 / 2017

Hyd. No. 11

Ditch betweenn culverts 2 and 3

Hydrograph type = Reach Peak discharge = 85.22 cfsStorm frequency = 10 yrsTime to peak = 736 min Time interval = 1 min Hyd. volume = 482.960 cuft = 9 - Junction of ditches for culveste2tamdtspe Inflow hyd. No. = Trapezoidal Reach length Channel slope = 815.0 ft= 2.3 % Bottom width = 5.0 ftManning's n = 0.040Side slope Max. depth = 3.0:1= 5.0 ftRating curve x Rating curve m = 1.341= 1.931Ave. velocity = 5.07 ft/sRouting coeff. = 0.4005



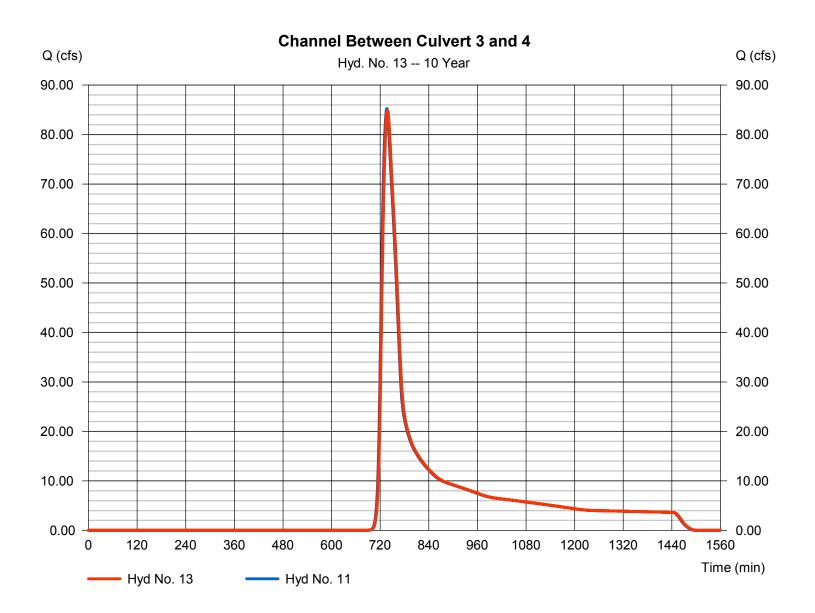
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Thursday, 03 / 2 / 2017

Hyd. No. 13

Channel Between Culvert 3 and 4

Hydrograph type Peak discharge = 84.84 cfs= Reach Storm frequency = 10 yrsTime to peak = 738 min Time interval = 1 min Hyd. volume = 482.960 cuft Inflow hyd. No. = 11 - Ditch betweenn culverts 2 Spection type = Trapezoidal Channel slope = 1.2 % Reach length = 450.0 ftBottom width $= 5.0 \, \text{ft}$ Manning's n = 0.040Side slope Max. depth = 3.0 ft= 3.0:1Rating curve x Rating curve m = 1.395= 1.321Ave. velocity = 3.79 ft/sRouting coeff. = 0.5002



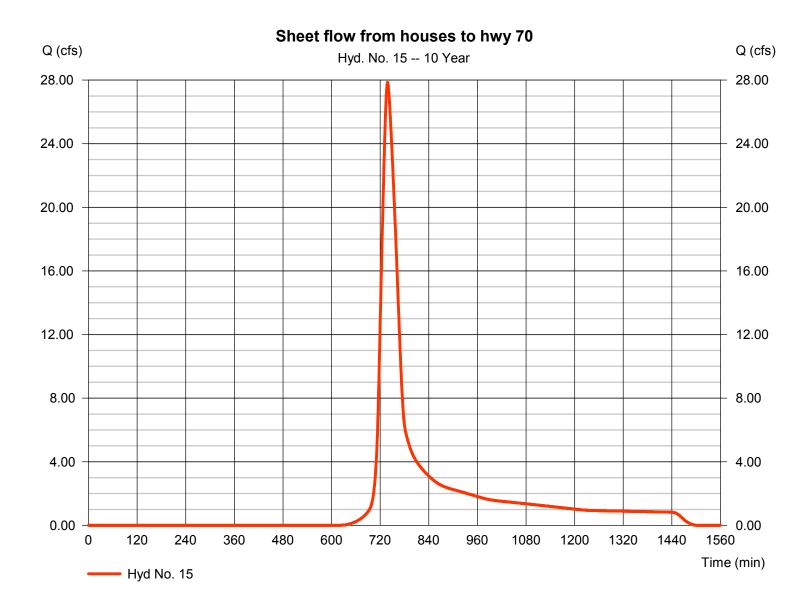
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Thursday, 03 / 2 / 2017

Hyd. No. 15

Sheet flow from houses to hwy 70

Hydrograph type = SCS Runoff Peak discharge = 27.87 cfsStorm frequency = 10 yrsTime to peak = 738 min Time interval = 1 min Hyd. volume = 140,815 cuft Drainage area Curve number = 20.330 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 39.60 min = TR55 Total precip. = 5.04 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



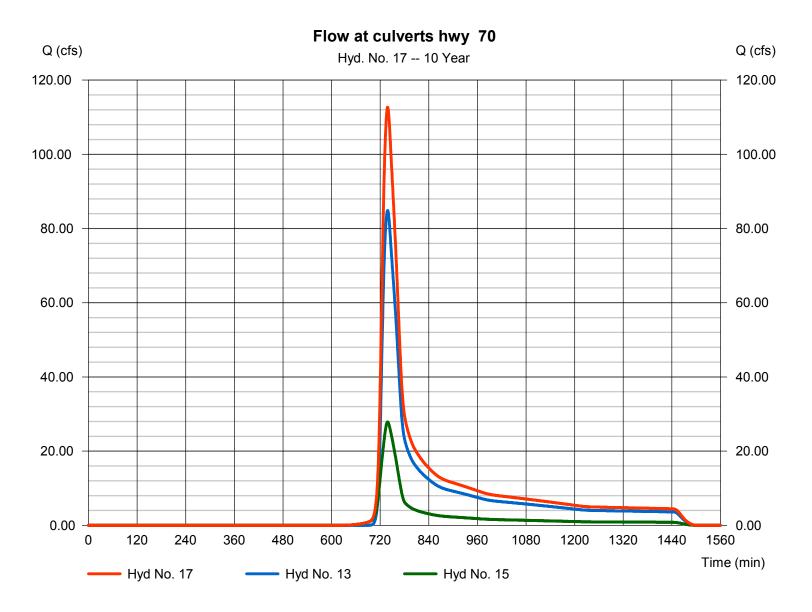
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Thursday, 03 / 2 / 2017

Hyd. No. 17

Flow at culverts hwy 70

Hydrograph type = Combine Peak discharge = 112.71 cfsStorm frequency = 10 yrsTime to peak = 738 min Time interval = 1 min Hyd. volume = 623,775 cuft Inflow hyds. Contrib. drain. area = 13, 15 = 20.330 ac



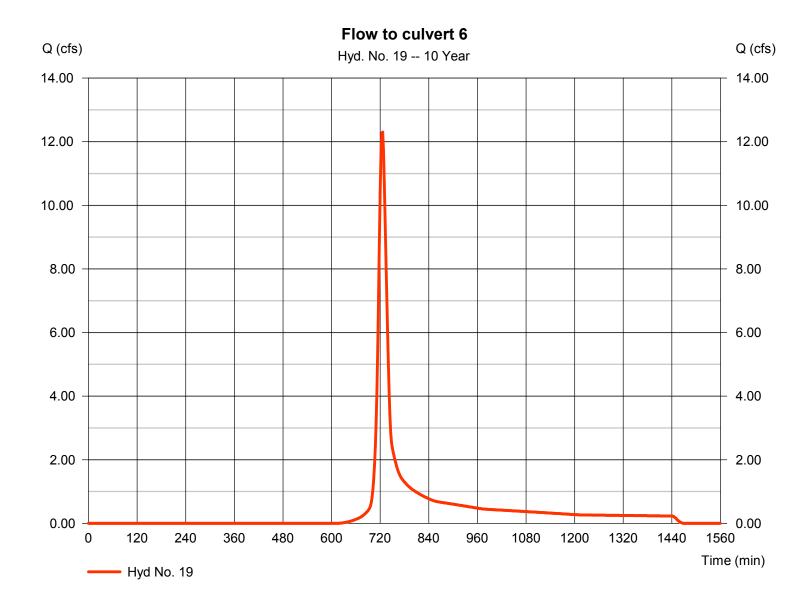
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Thursday, 03 / 2 / 2017

Hyd. No. 19

Flow to culvert 6

Hydrograph type = SCS Runoff Peak discharge = 12.30 cfsStorm frequency = 10 yrsTime to peak = 726 min Time interval = 2 min Hyd. volume = 39.619 cuft Drainage area Curve number = 5.720 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 17.80 min = TR55 Total precip. = 5.04 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

lyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	112.65	1	736	568,777				Area Above Hannah Ford leading to
3	Reach	112.65	1	737	568,777	1			Ditch between Culvert 1 and culver 2
5	SCS Runoff	46.54	1	724	138,852				Area above culvert 5 to culvert 5
7	Reach	46.56	1	725	138,852	5			Ditch between culvert 5 and outfall of
9	Combine	137.16	1	734	707,628	3, 7,			Junction of ditches for culvert 2 and 5
11	Reach	136.38	1	736	707,627	9			Ditch betweenn culverts 2 and 3
13	Reach	135.91	1	737	707,626	11			Channel Between Culvert 3 and 4
15	SCS Runoff	38.53	1	738	190,584				Sheet flow from houses to hwy 70
17	Combine	174.39	1	738	898,210	13, 15,			Flow at culverts hwy 70
19	SCS Runoff	16.91	2	724	53,622				Flow to culvert 6

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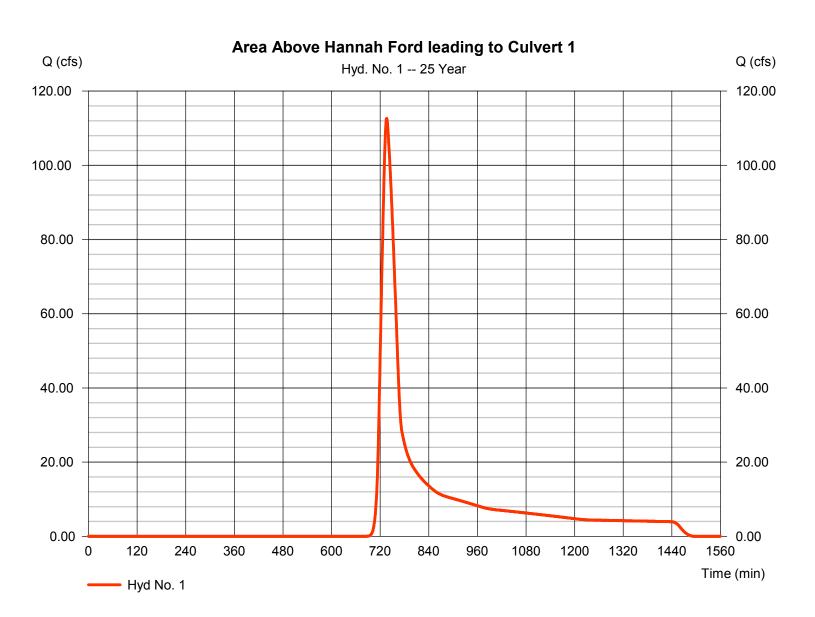
Thursday, 03 / 2 / 2017

Hyd. No. 1

Area Above Hannah Ford leading to Culvert 1

= SCS Runoff Peak discharge = 112.65 cfsHydrograph type Storm frequency = 25 yrsTime to peak = 736 min Time interval = 1 min Hyd. volume = 568,777 cuft Curve number Drainage area = 100.000 ac= 56* Basin Slope = 0.0 %Hydraulic length = 0 ftTime of conc. (Tc) Tc method = TR55 $= 34.70 \, \text{min}$ Total precip. Distribution = Type II = 5.95 inStorm duration Shape factor = 484 = 24 hrs

^{*} Composite (Area/CN) = [(17.000 x 36) + (83.000 x 60)] / 100.000



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Hyd. No. 3

Ditch between Culvert 1 and culver 2

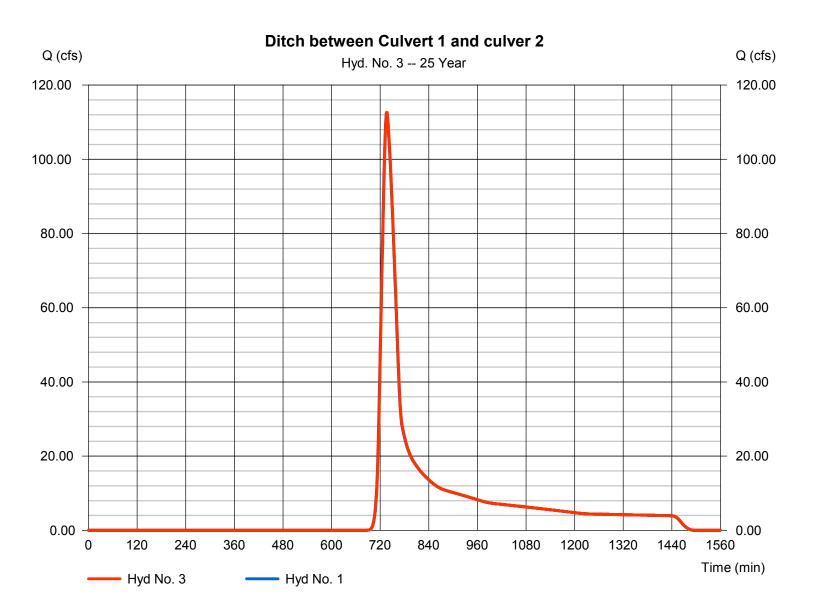
= Reach Peak discharge = 112.65 cfsHydrograph type Storm frequency = 25 yrsTime to peak = 737 min Time interval = 1 min Hyd. volume = 568,777 cuft = 1 - Area Above Hannah Ford leaching not your 1 Inflow hyd. No. = Trapezoidal Channel slope Reach length = 1.8 % = 118.0 ftBottom width = 3.0 ftManning's n = 0.030

 Manning's n
 = 0.030
 Bottom width
 = 3.0 ft

 Side slope
 = 3.0:1
 Max. depth
 = 5.0 ft

 Rating curve x
 = 3.202
 Rating curve m
 = 1.279

 Ave. velocity
 = 6.96 ft/s
 Routing coeff.
 = 1.3872



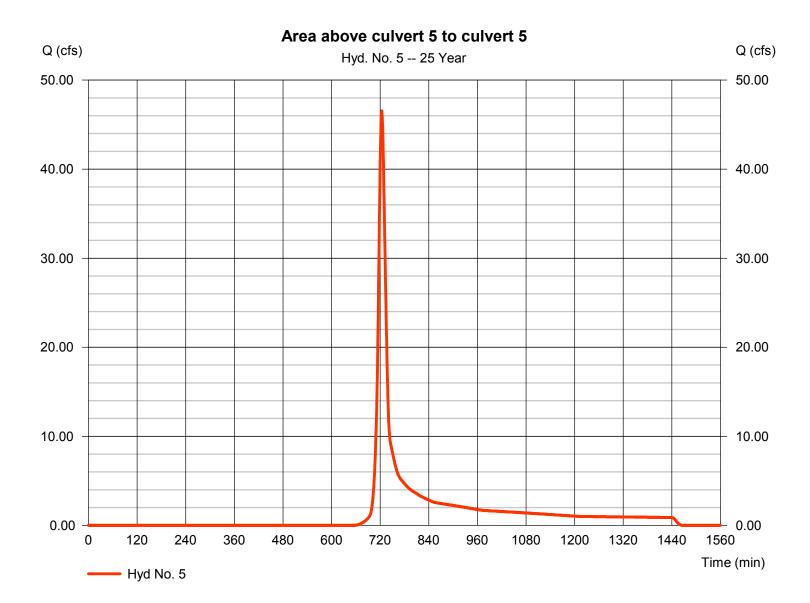
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Thursday, 03 / 2 / 2017

Hyd. No. 5

Area above culvert 5 to culvert 5

Hydrograph type = SCS Runoff Peak discharge = 46.54 cfsStorm frequency = 25 yrs Time to peak = 724 min Time interval = 1 min Hyd. volume = 138,852 cuft Drainage area Curve number = 20.000 ac= 60 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 16.77 min = TR55 Total precip. = 5.95 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



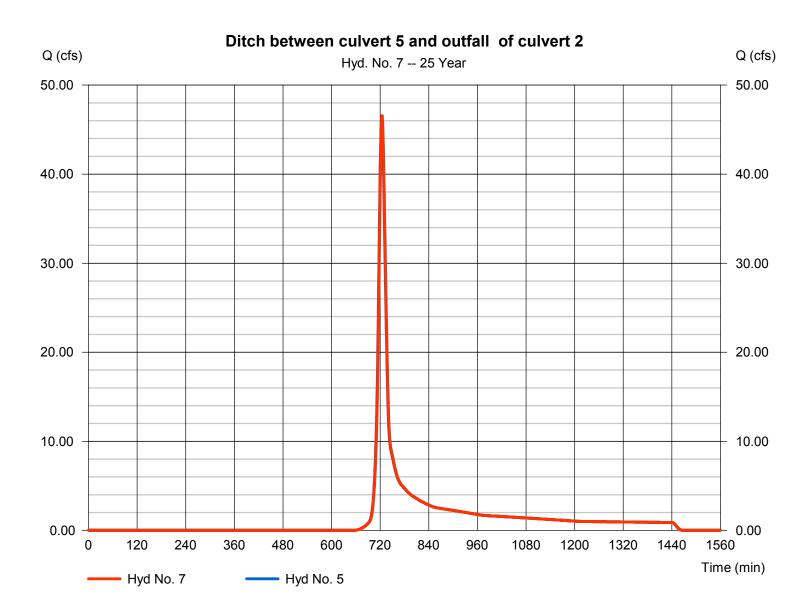
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Hyd. No. 7

Ditch between culvert 5 and outfall of culvert 2

= Reach Peak discharge = 46.56 cfsHydrograph type Storm frequency = 25 yrsTime to peak = 725 min Time interval = 1 min Hyd. volume = 138.852 cuft Inflow hyd. No. = 5 - Area above culvert 5 to c = Trapezoidal Reach length Channel slope = 3.8 % = 174.0 ft= 3.0 ftManning's n = 0.040Bottom width Side slope Max. depth = 2.0 ft= 2.0:1Rating curve x Rating curve m = 1.249= 3.490Ave. velocity Routing coeff. = 1.1154= 5.85 ft/s



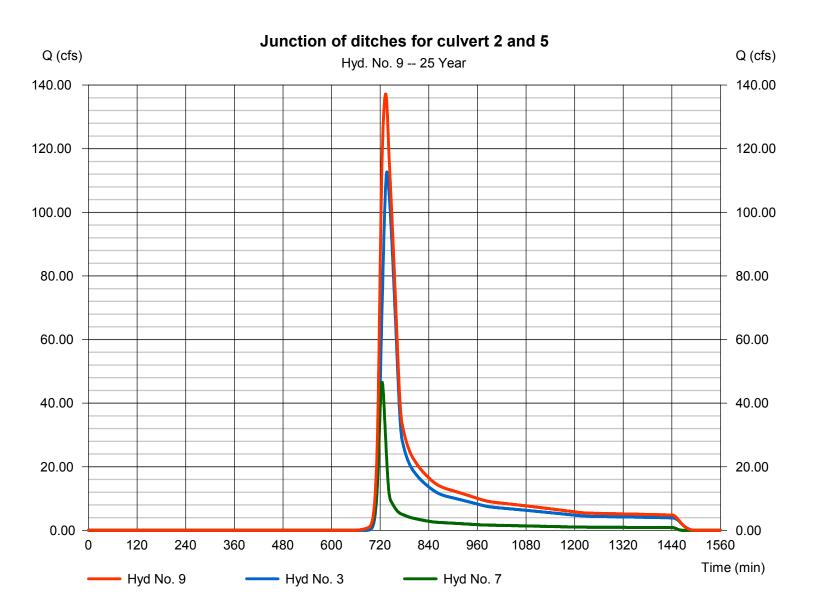
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Hyd. No. 9

Junction of ditches for culvert 2 and 5

Hydrograph type = Combine Peak discharge = 137.16 cfsStorm frequency Time to peak = 25 yrs= 734 min Time interval = 1 min Hyd. volume = 707,628 cuft Inflow hyds. = 3, 7Contrib. drain. area = 0.000 ac



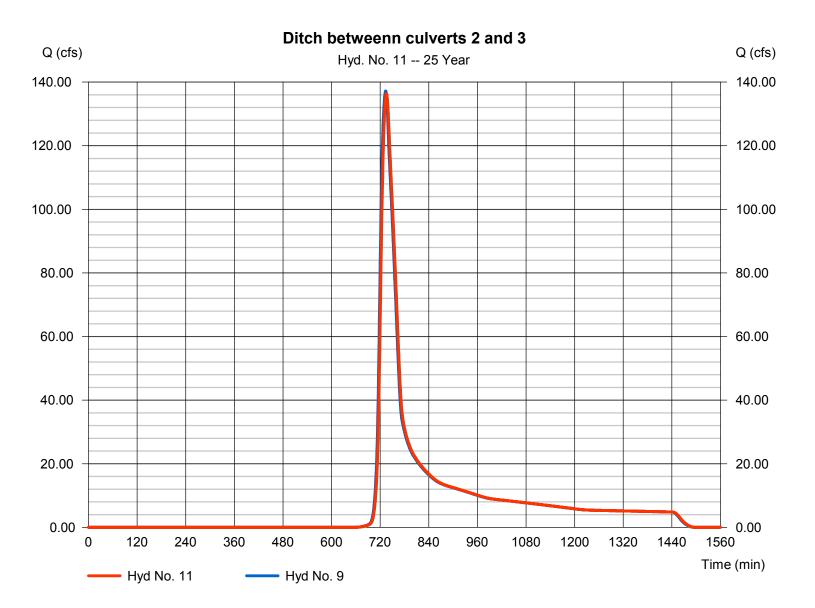
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Hyd. No. 11

Ditch betweenn culverts 2 and 3

Peak discharge = Reach = 136.38 cfsHydrograph type Storm frequency = 25 yrsTime to peak = 736 min = 707,627 cuft Time interval = 1 min Hyd. volume = 9 - Junction of ditches for culveste2tamdtspe Inflow hyd. No. = Trapezoidal Channel slope Reach length = 815.0 ft= 2.3 % Bottom width = 5.0 ftManning's n = 0.040Side slope Max. depth = 3.0:1= 5.0 ftRating curve x Rating curve m = 1.931= 1.341Ave. velocity = 5.71 ft/sRouting coeff. = 0.4399



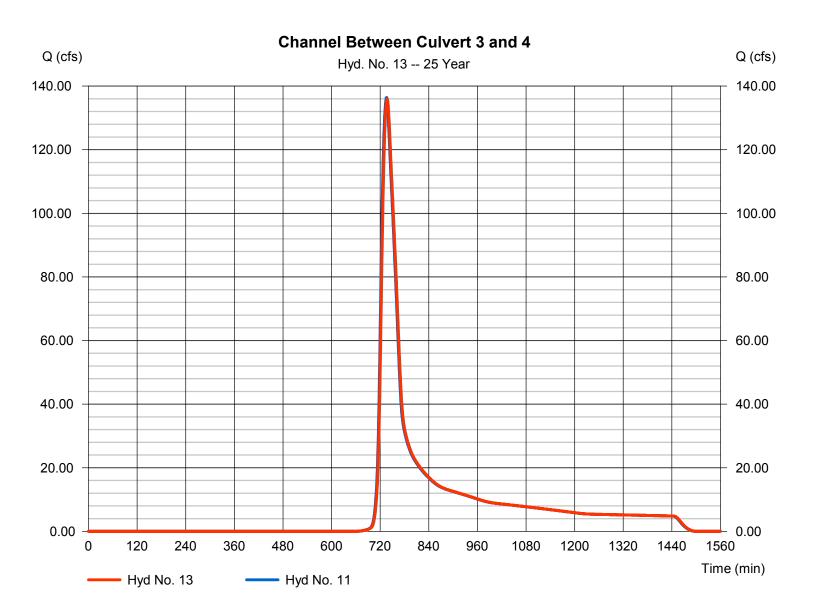
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 13

Channel Between Culvert 3 and 4

Peak discharge Hydrograph type = Reach = 135.91 cfsStorm frequency = 25 yrsTime to peak = 737 min = 707,626 cuft Time interval = 1 min Hyd. volume Inflow hyd. No. = 11 - Ditch betweenn culverts 2 Saedtion type = Trapezoidal Reach length Channel slope = 1.2 % = 450.0 ftBottom width = 5.0 ftManning's n = 0.040Side slope Max. depth = 3.0:1= 3.0 ftRating curve x Rating curve m = 1.395= 1.321Ave. velocity = 4.25 ft/sRouting coeff. = 0.5443



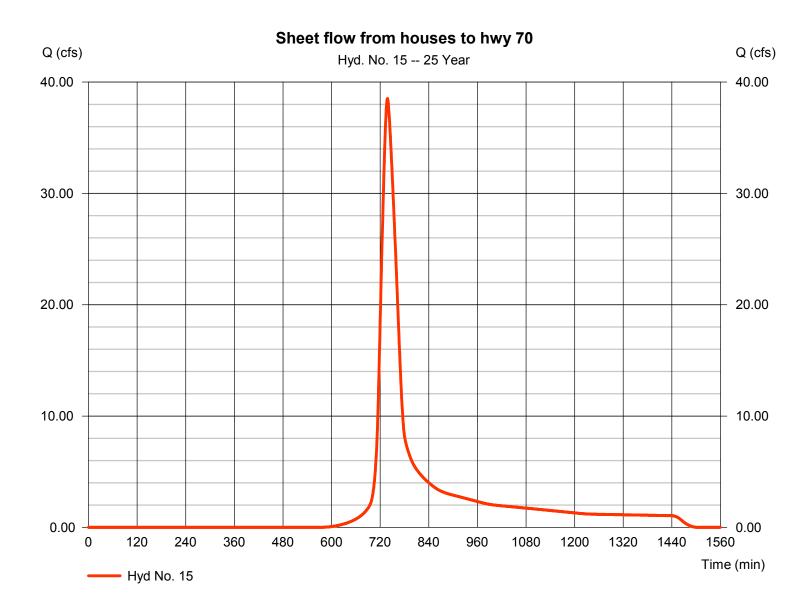
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 15

Sheet flow from houses to hwy 70

Hydrograph type = SCS Runoff Peak discharge = 38.53 cfsStorm frequency = 25 yrs Time to peak = 738 min Time interval = 1 min Hyd. volume = 190,584 cuft Drainage area Curve number = 20.330 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 39.60 min = TR55 Total precip. = 5.95 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



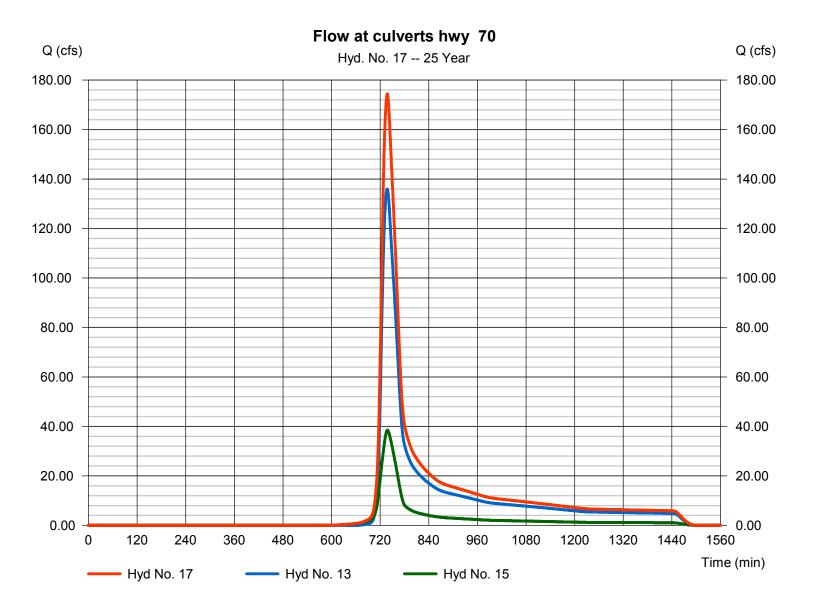
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 17

Flow at culverts hwy 70

Hydrograph type = Combine Peak discharge = 174.39 cfsStorm frequency Time to peak = 25 yrs= 738 min Time interval = 1 min Hyd. volume = 898,210 cuft Inflow hyds. Contrib. drain. area = 13, 15 = 20.330 ac



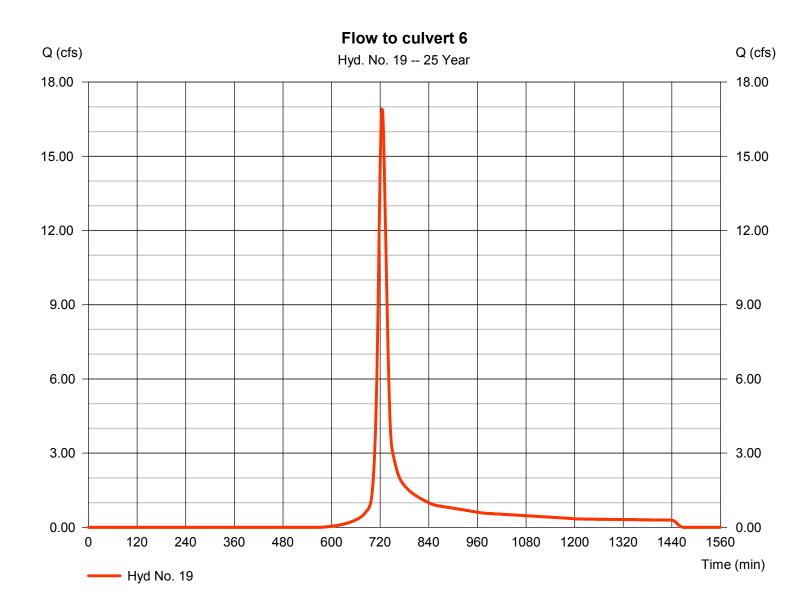
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 19

Flow to culvert 6

Hydrograph type = SCS Runoff Peak discharge = 16.91 cfsStorm frequency = 25 yrs Time to peak = 724 min Time interval = 2 min Hyd. volume = 53,622 cuft Drainage area Curve number = 5.720 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 17.80 min = TR55 Total precip. = 5.95 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	150.27	1	736	728,353				Area Above Hannah Ford leading to
3	Reach	150.52	1	736	728,354	1			Ditch between Culvert 1 and culver 2
5	SCS Runoff	59.46	1	724	174,409				Area above culvert 5 to culvert 5
7	Reach	59.47	1	725	174,409	5			Ditch between culvert 5 and outfall of
9	Combine	182.11	1	733	902,763	3, 7,			Junction of ditches for culvert 2 and 5
11	Reach	181.23	1	735	902,761	9			Ditch betweenn culverts 2 and 3
13	Reach	180.75	1	737	902,761	11			Channel Between Culvert 3 and 4
15	SCS Runoff	47.37	1	738	232,111				Sheet flow from houses to hwy 70
17	Combine	228.03	1	737	1,134,870	13, 15,			Flow at culverts hwy 70
19	SCS Runoff	20.75	2	724	65,306				Flow to culvert 6

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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

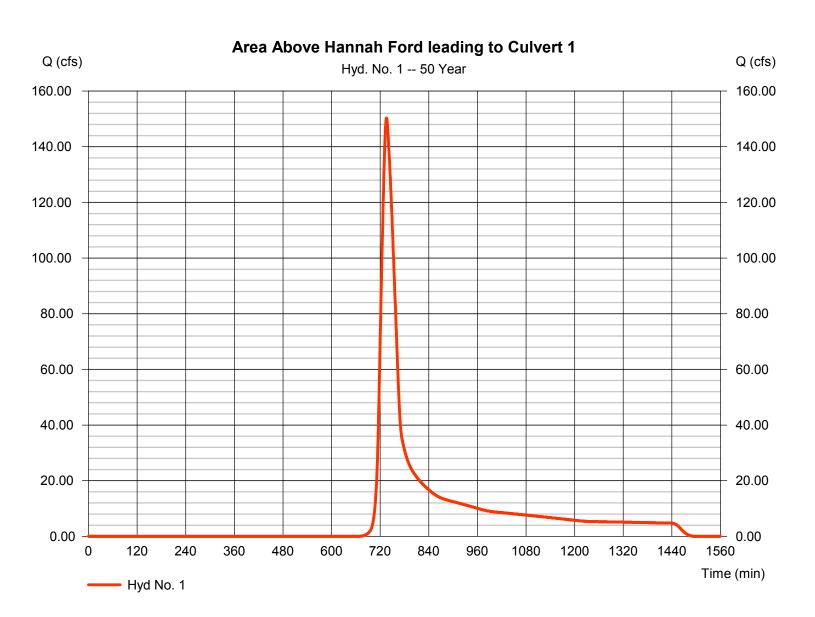
Thursday, 03 / 2 / 2017

Hyd. No. 1

Area Above Hannah Ford leading to Culvert 1

= SCS Runoff Peak discharge = 150.27 cfsHydrograph type Storm frequency = 50 yrsTime to peak = 736 min Time interval = 1 min Hyd. volume = 728.353 cuft Curve number Drainage area = 100.000 ac= 56* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 34.70 min = TR55 Total precip. Distribution = Type II = 6.67 inStorm duration Shape factor = 484 = 24 hrs

^{*} Composite (Area/CN) = [(17.000 x 36) + (83.000 x 60)] / 100.000



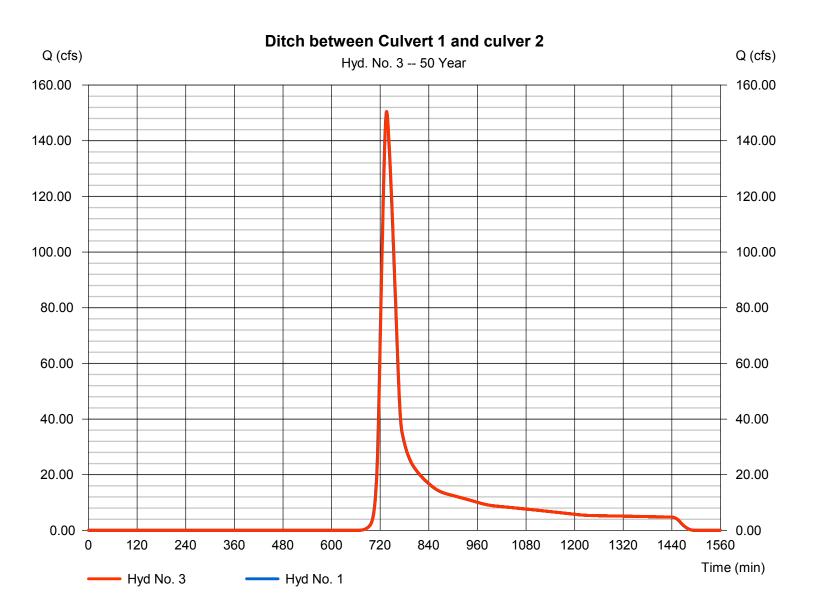
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 3

Ditch between Culvert 1 and culver 2

= Reach Peak discharge = 150.52 cfsHydrograph type Storm frequency = 50 yrsTime to peak = 736 min Time interval = 1 min Hyd. volume = 728.354 cuft = 1 - Area Above Hannah Ford leachtigrtdy@elvert 1 Inflow hyd. No. = Trapezoidal Channel slope = 1.8 % Reach length = 118.0 ftBottom width = 3.0 ftManning's n = 0.030Side slope Max. depth = 3.0:1= 5.0 ftRating curve x Rating curve m = 3.202= 1.279Ave. velocity = 7.41 ft/sRouting coeff. = 1.4136



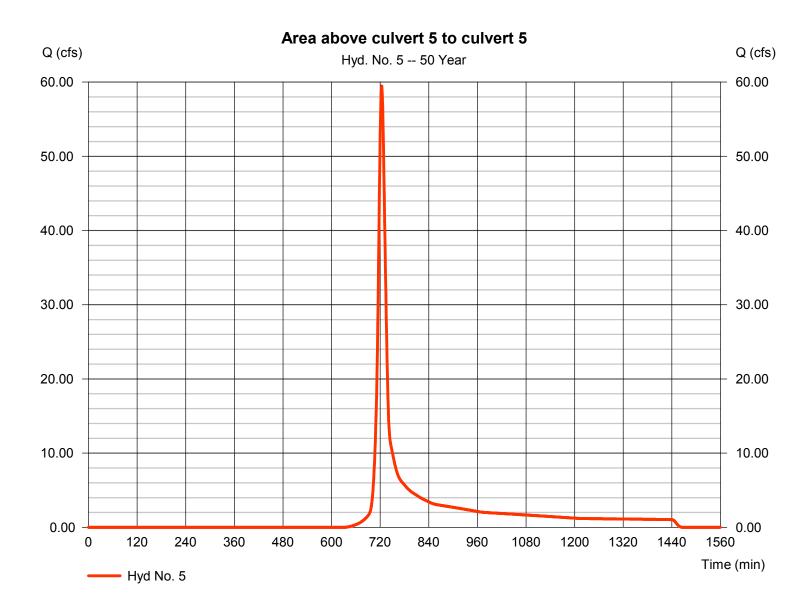
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 5

Area above culvert 5 to culvert 5

Hydrograph type = SCS Runoff Peak discharge = 59.46 cfsStorm frequency = 50 yrsTime to peak = 724 min Time interval = 1 min Hyd. volume = 174,409 cuft Drainage area Curve number = 20.000 ac= 60 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 16.77 min = TR55 Total precip. = 6.67 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



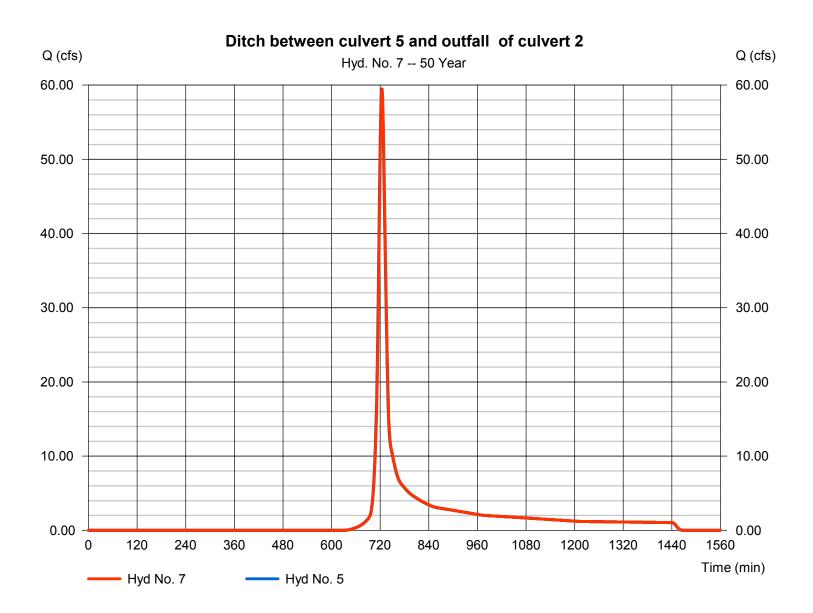
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 7

Ditch between culvert 5 and outfall of culvert 2

= Reach Peak discharge = 59.47 cfsHydrograph type Storm frequency = 50 yrsTime to peak = 725 min Time interval = 1 min Hyd. volume = 174.409 cuft Inflow hyd. No. = 5 - Area above culvert 5 to c = Trapezoidal Reach length Channel slope = 3.8 % = 174.0 ftBottom width = 3.0 ftManning's n = 0.040Side slope Max. depth = 2.0:1= 2.0 ftRating curve x Rating curve m = 1.249= 3.490Ave. velocity Routing coeff. = 6.15 ft/s= 1.1395



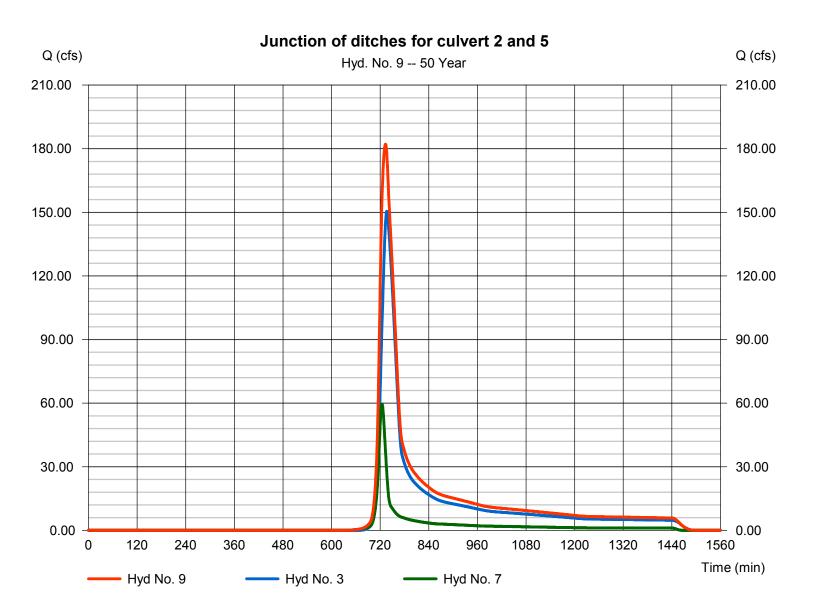
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 9

Junction of ditches for culvert 2 and 5

Hydrograph type = Combine Peak discharge = 182.11 cfsStorm frequency Time to peak = 50 yrs= 733 min Time interval = 1 min Hyd. volume = 902,763 cuft Inflow hyds. = 3, 7Contrib. drain. area = 0.000 ac



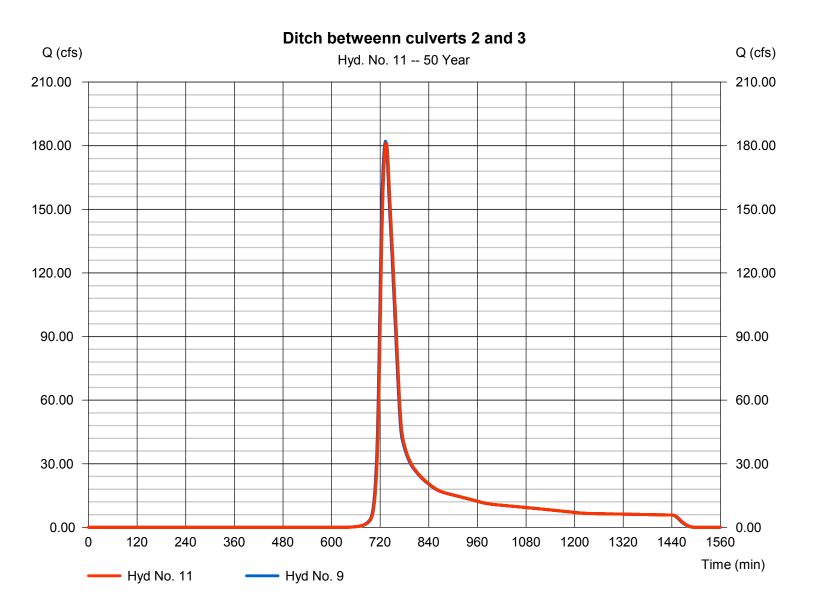
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 11

Ditch betweenn culverts 2 and 3

Hydrograph type = Reach Peak discharge = 181.23 cfsStorm frequency = 50 yrsTime to peak = 735 min Time interval = 1 min Hyd. volume = 902,761 cuft = 9 - Junction of ditches for culveste2tamdtspe Inflow hyd. No. = Trapezoidal Reach length Channel slope = 2.3 % = 815.0 ftManning's n Bottom width = 5.0 ft= 0.040Side slope Max. depth = 3.0:1= 5.0 ftRating curve x Rating curve m = 1.341= 1.931Routing coeff. Ave. velocity = 6.14 ft/s= 0.4651



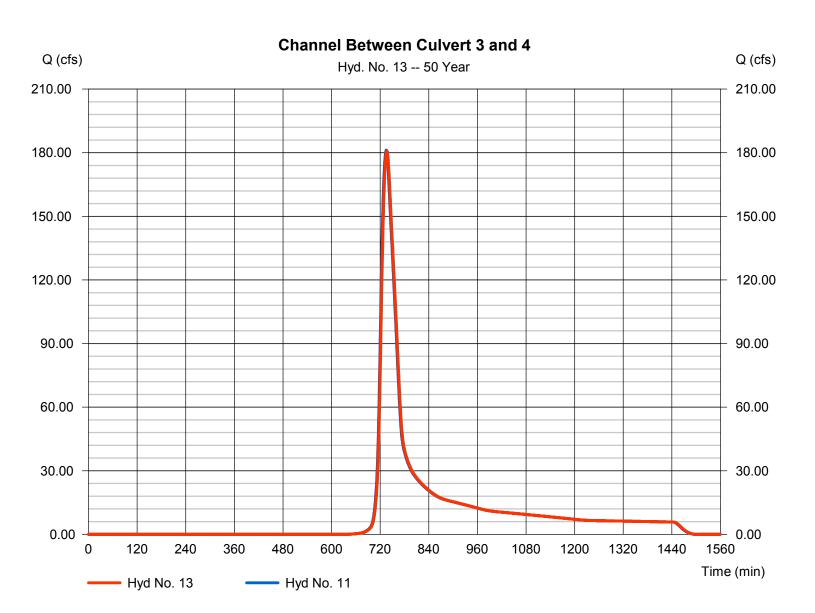
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 13

Channel Between Culvert 3 and 4

Peak discharge Hydrograph type = Reach = 180.75 cfsStorm frequency = 50 yrsTime to peak = 737 min Time interval = 1 min Hyd. volume = 902,761 cuft Inflow hyd. No. = 11 - Ditch betweenn culverts 2 Saedtion type = Trapezoidal Channel slope = 1.2 % Reach length = 450.0 ftBottom width $= 5.0 \, \text{ft}$ Manning's n = 0.040Side slope Max. depth = 3.0:1= 3.0 ftRating curve x Rating curve m = 1.395= 1.321Ave. velocity Routing coeff. = 4.55 ft/s= 0.5720



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 15

Sheet flow from houses to hwy 70

Hydrograph type = SCS Runoff Peak discharge = 47.37 cfsStorm frequency = 50 yrsTime to peak = 738 min Time interval = 1 min Hyd. volume = 232.111 cuft Curve number Drainage area = 20.330 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 39.60 min = TR55 Total precip. = 6.67 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

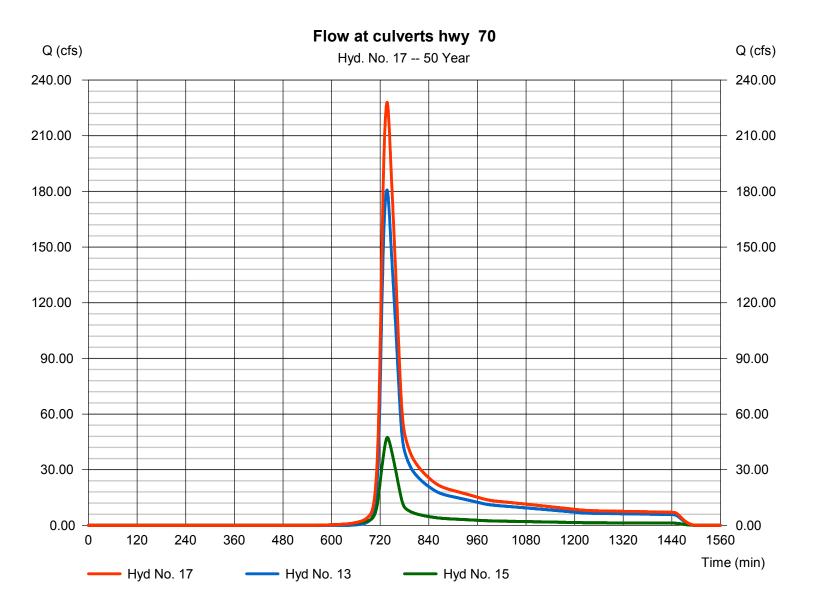
Thursday, 03 / 2 / 2017

Hyd. No. 17

Flow at culverts hwy 70

Hydrograph type = Combine Peak discharge = 228.03 cfs Storm frequency = 50 yrs Time to peak = 737 min

Time interval = 1 min Hyd. volume = 1,134,870 cuft Contrib. drain. area = 20.330 ac



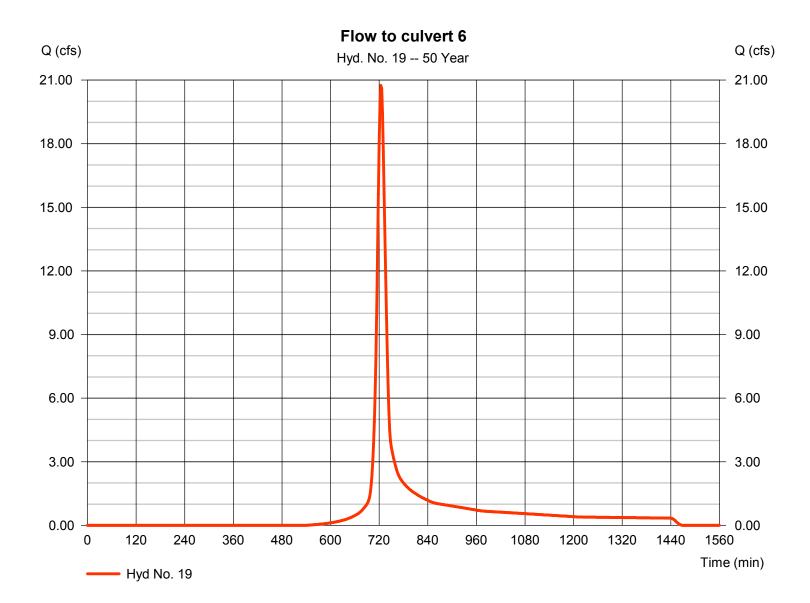
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 19

Flow to culvert 6

Hydrograph type = SCS Runoff Peak discharge = 20.75 cfsStorm frequency = 50 yrsTime to peak = 724 min Time interval = 2 min Hyd. volume = 65,306 cuftDrainage area Curve number = 5.720 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 17.80 min = TR55 Total precip. = 6.67 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

lyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	192.30	1	735	905,950				Area Above Hannah Ford leading to
3	Reach	192.53	1	736	905,950	1			Ditch between Culvert 1 and culver 2
5	SCS Runoff	73.57	1	724	213,534				Area above culvert 5 to culvert 5
7	Reach	73.68	1	724	213,534	5			Ditch between culvert 5 and outfall of
9	Combine	231.88	1	733	1,119,485	3, 7,			Junction of ditches for culvert 2 and 5
11	Reach	230.94	1	735	1,119,484	9			Ditch betweenn culverts 2 and 3
13	Reach	230.39	1	736	1,119,483	11			Channel Between Culvert 3 and 4
15	SCS Runoff	56.85	1	738	276,957				Sheet flow from houses to hwy 70
17	Combine	287.05	1	737	1,396,440	13, 15,			Flow at culverts hwy 70
19	SCS Runoff	24.86	2	724	77,924				Flow to culvert 6

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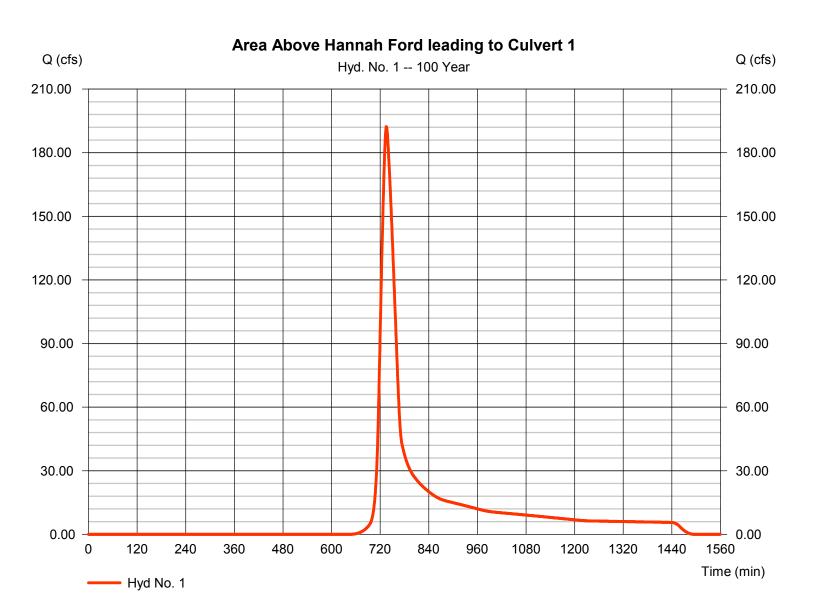
Thursday, 03 / 2 / 2017

Hyd. No. 1

Area Above Hannah Ford leading to Culvert 1

= SCS Runoff Peak discharge = 192.30 cfsHydrograph type Storm frequency = 100 yrsTime to peak = 735 min Time interval = 1 min Hyd. volume = 905.950 cuft Curve number Drainage area = 100.000 ac= 56* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 34.70 min = TR55 Total precip. Distribution = Type II = 7.42 inStorm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = [(17.000 x 36) + (83.000 x 60)] / 100.000



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

= 7.82 ft/s

Thursday, 03 / 2 / 2017

= 1.4357

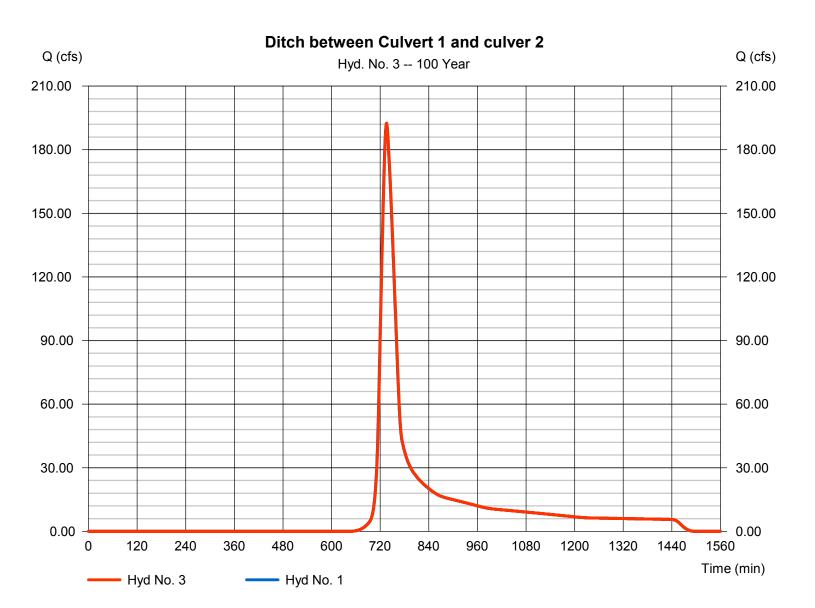
Hyd. No. 3

Ave. velocity

Ditch between Culvert 1 and culver 2

= Reach Peak discharge = 192.53 cfsHydrograph type Storm frequency = 100 yrsTime to peak = 736 min Time interval = 1 min Hyd. volume = 905.950 cuft = 1 - Area Above Hannah Ford leachtigrtdy@elvert 1 Inflow hyd. No. = Trapezoidal Channel slope Reach length = 1.8 % = 118.0 ftBottom width = 3.0 ftManning's n = 0.030Side slope Max. depth = 3.0:1= 5.0 ftRating curve x Rating curve m = 3.202= 1.279

Routing coeff.



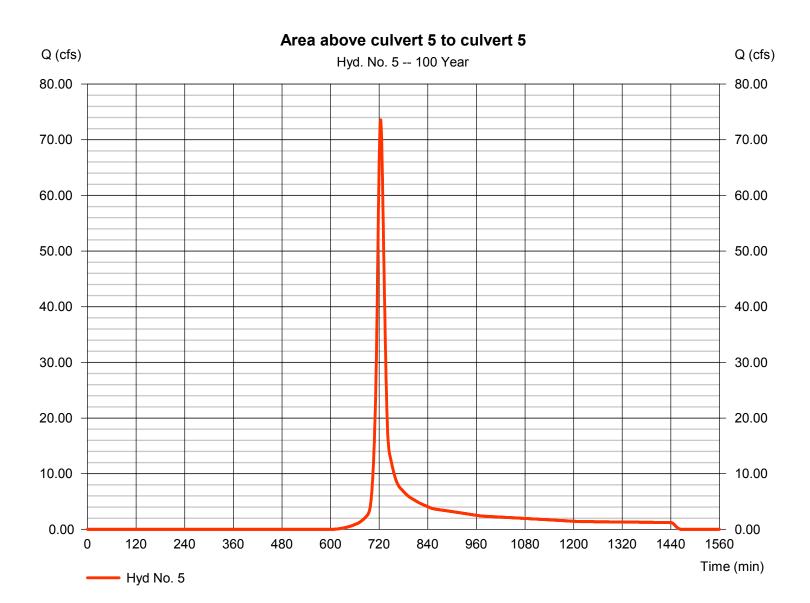
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 5

Area above culvert 5 to culvert 5

Hydrograph type = SCS Runoff Peak discharge = 73.57 cfsStorm frequency Time to peak = 100 yrs= 724 min Time interval = 1 min Hyd. volume = 213,534 cuft Drainage area Curve number = 20.000 ac= 60 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 16.77 min = TR55 Total precip. = 7.42 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



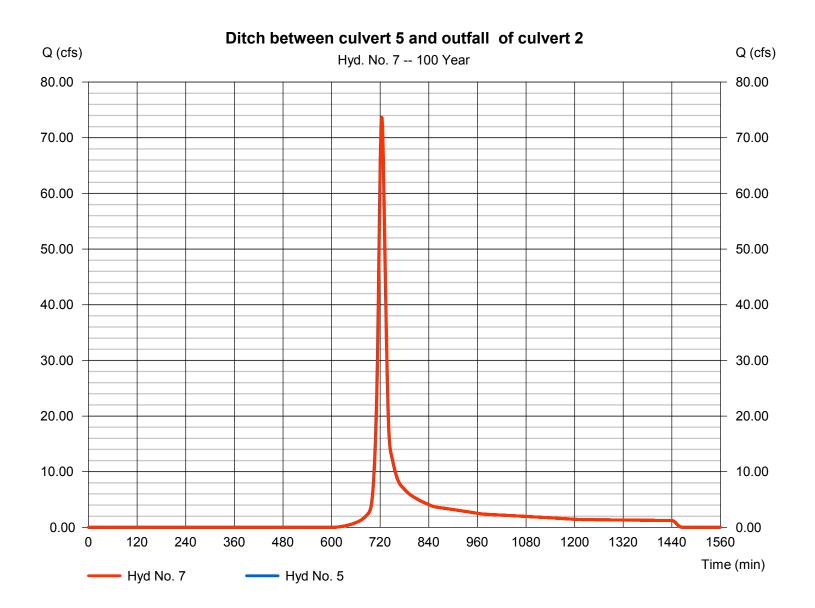
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 7

Ditch between culvert 5 and outfall of culvert 2

= Reach Peak discharge = 73.68 cfsHydrograph type Storm frequency = 100 yrsTime to peak = 724 min Time interval = 1 min Hyd. volume = 213.534 cuft Inflow hyd. No. = 5 - Area above culvert 5 to c = Trapezoidal Channel slope Reach length = 174.0 ft= 3.8 % Bottom width = 3.0 ftManning's n = 0.040Side slope Max. depth = 2.0 ft= 2.0:1Rating curve x Rating curve m = 1.249= 3.490Ave. velocity = 6.41 ft/sRouting coeff. = 1.1603



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Thursday, 03 / 2 / 2017

= 231.88 cfs

Hyd. No. 9

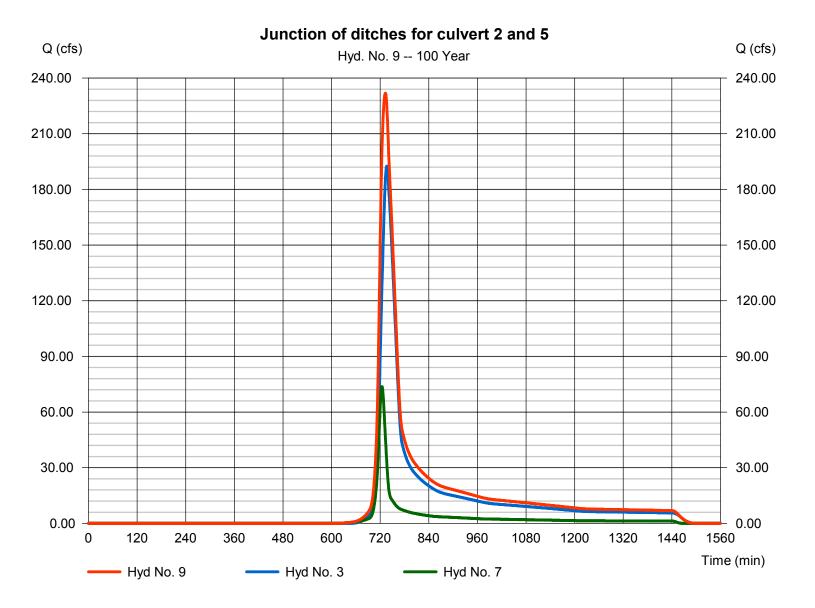
Junction of ditches for culvert 2 and 5

Hydrograph type = Combine Storm frequency = 100 yrs Time interval = 1 min

Time to peak = 733 min Hyd. volume = 1,119,485 cuft

Peak discharge

Inflow hyds. = 3, 7 Contrib. drain. area = 0.000 ac



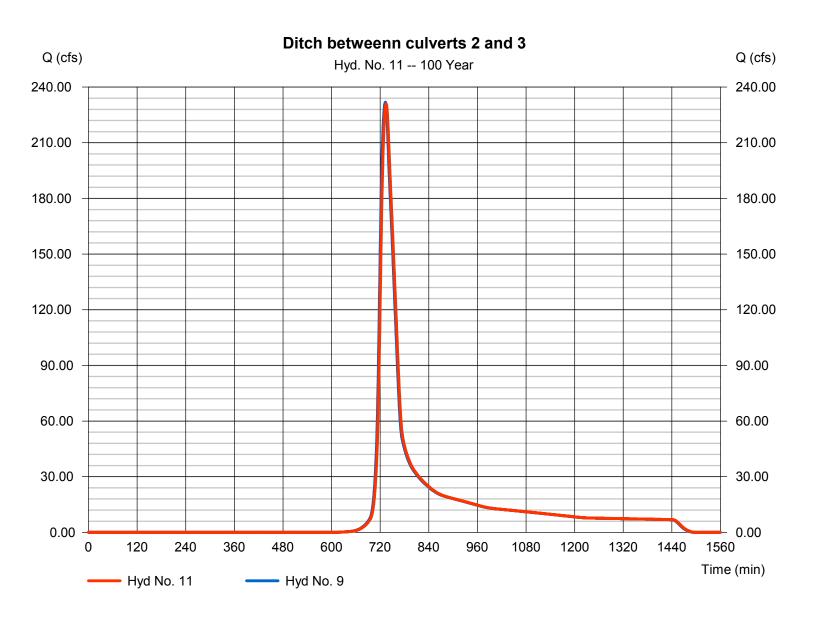
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Thursday, 03 / 2 / 2017

Hyd. No. 11

Ditch betweenn culverts 2 and 3

Peak discharge = Reach = 230.94 cfsHydrograph type Storm frequency = 100 yrsTime to peak = 735 min Time interval = 1 min Hyd. volume = 1,119,484 cuft = 9 - Junction of ditches for culveste2tamdtspe Inflow hyd. No. = Trapezoidal Reach length Channel slope = 2.3 % = 815.0 ftBottom width = 5.0 ftManning's n = 0.040Side slope Max. depth = 3.0:1= 5.0 ftRating curve x Rating curve m = 1.931= 1.341Ave. velocity = 6.53 ft/sRouting coeff. = 0.4874



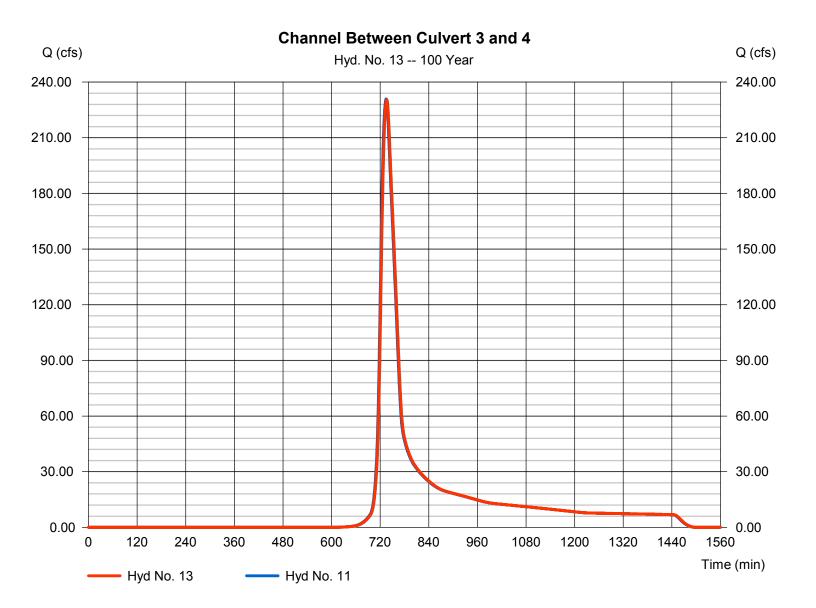
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 13

Channel Between Culvert 3 and 4

Peak discharge = 230.39 cfsHydrograph type = Reach Storm frequency = 100 yrsTime to peak = 736 min Time interval = 1 min Hyd. volume = 1,119,483 cuft Inflow hyd. No. = 11 - Ditch betweenn culverts 2 Saedtion type = Trapezoidal Channel slope = 1.2 % Reach length = 450.0 ftBottom width = 5.0 ftManning's n = 0.040Side slope Max. depth = 3.0:1= 3.0 ftRating curve x Rating curve m = 1.395= 1.321Ave. velocity Routing coeff. = 4.83 ft/s= 0.5964



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 15

Sheet flow from houses to hwy 70

Hydrograph type = SCS Runoff Peak discharge = 56.85 cfsStorm frequency = 100 yrsTime to peak = 738 min Time interval = 1 min Hyd. volume = 276,957 cuft Drainage area Curve number = 20.330 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 39.60 min = TR55 Total precip. = 7.42 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

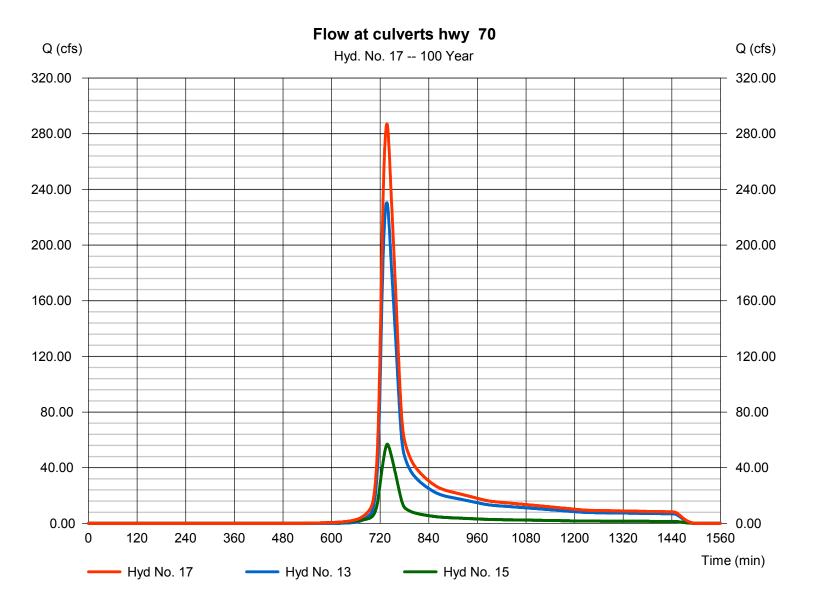
Thursday, 03 / 2 / 2017

Hyd. No. 17

Flow at culverts hwy 70

Hydrograph type = Combine Peak discharge = 287.05 cfs
Storm frequency = 100 yrs Time to peak = 737 min

Time interval = 1 min Hyd. volume = 1,396,440 cuft Contrib. drain. area = 20.330 ac



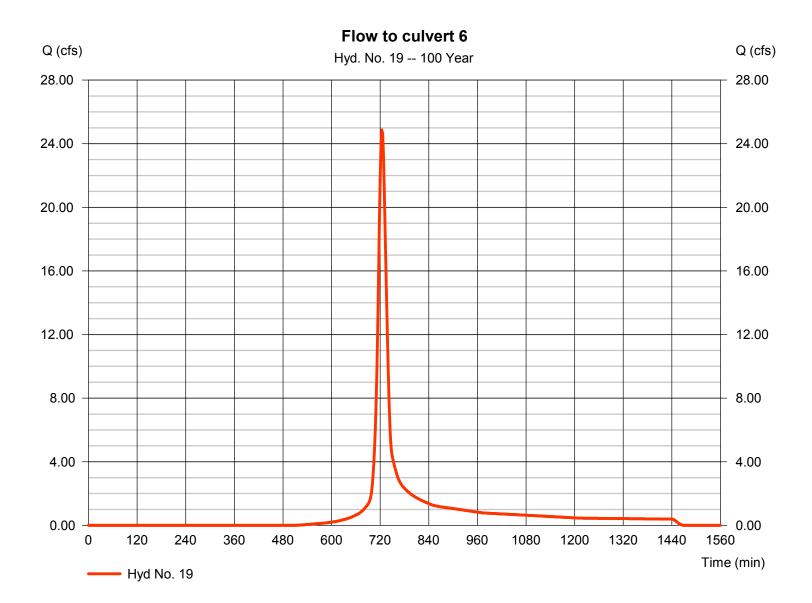
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Hyd. No. 19

Flow to culvert 6

Hydrograph type = SCS Runoff Peak discharge = 24.86 cfsStorm frequency = 100 yrsTime to peak = 724 min Time interval = 2 min Hyd. volume = 77,924 cuft Drainage area Curve number = 5.720 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 17.80 min = TR55 Total precip. = 7.42 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



Hydraflow Rainfall Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v10.5

Thursday, 03 / 2 / 2017

Return Period	Intensity-Duration-Frequency Equation Coefficients (FHA)							
(Yrs)	В	D	E	(N/A)				
1	0.0000	0.0000	0.0000					
2	69.8703	13.1000	0.8658					
3	0.0000	0.0000	0.0000					
5	79.2597	14.6000	0.8369					
10	88.2351	15.5000	0.8279					
25	102.6072	16.5000	0.8217					
50	114.8193	17.2000	0.8199					
100	127.1596	17.8000	0.8186					

File name: SampleFHA.idf

Intensity = $B / (Tc + D)^E$

Return	Intensity Values (in/hr)											
Period (Yrs)	5 min	10	15	20	25	30	35	40	45	50	55	60
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	5.69	4.61	3.89	3.38	2.99	2.69	2.44	2.24	2.07	1.93	1.81	1.70
3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	6.57	5.43	4.65	4.08	3.65	3.30	3.02	2.79	2.59	2.42	2.27	2.15
10	7.24	6.04	5.21	4.59	4.12	3.74	3.43	3.17	2.95	2.77	2.60	2.46
25	8.25	6.95	6.03	5.34	4.80	4.38	4.02	3.73	3.48	3.26	3.07	2.91
50	9.04	7.65	6.66	5.92	5.34	4.87	4.49	4.16	3.88	3.65	3.44	3.25
100	9.83	8.36	7.30	6.50	5.87	5.36	4.94	4.59	4.29	4.03	3.80	3.60

Tc = time in minutes. Values may exceed 60.

e: C:\Users\Christian\OneDrive\PEGRAM SR DESIGN\006 Design\Hydraulic Analysis\Catchment Area\Precip data.pcp

	Rainfall Precipitation Table (in)								
Storm Distribution	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	
SCS 24-hour	0.00	3.62	0.00	4.41	5.04	5.95	6.67	7.42	
SCS 6-Hr	0.00	2.48	0.00	3.01	3.46	4.08	4.60	5.14	
Huff-1st	0.00	1.55	0.00	2.75	4.00	5.38	6.50	8.00	
Huff-2nd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Huff-3rd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Huff-4th	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Huff-Indy	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Custom	0.00	1.75	0.00	2.80	3.90	5.25	6.00	7.10	



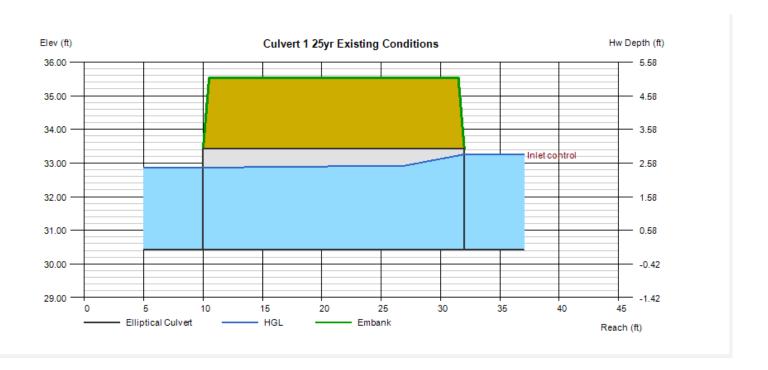
ENCLOSURE (F)

CULVERT ANALYSIS REPORTS

Monday, Mar 6 2017

Culvert 1 25yr Existing Conditions

= 30.42	Calculations	
= 22.01	Qmin (cfs)	= 50.00
= 0.00	Qmax (cfs)	= 112.65
= 30.42	Tailwater Elev (ft)	= Normal
= 36.0		
= Elliptical	Highlighted	
= 60.0	Qtotal (cfs)	= 50.00
= 1	Qpipe (cfs)	= 50.00
= 0.013	Qovertop (cfs)	= 0.00
 Horizontal Ellipse Concrete 	Veloc Dn (ft/s)	= 4.69
Square edge w/headwall (H)	Veloc Up (ft/s)	= 4.69
= 0.01, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 32.86
	HGL Up (ft)	= 32.94
	Hw Elev (ft)	= 33.26
= 35.53	Hw/D (ft)	= 0.95
= 21.00	Flow Regime	= Inlet Control
= 300.00		
	= 22.01 = 0.00 = 30.42 = 36.0 = Elliptical = 60.0 = 1 = 0.013 = Horizontal Ellipse Concrete = Square edge w/headwall (H) = 0.01, 2, 0.0398, 0.67, 0.5	= 22.01



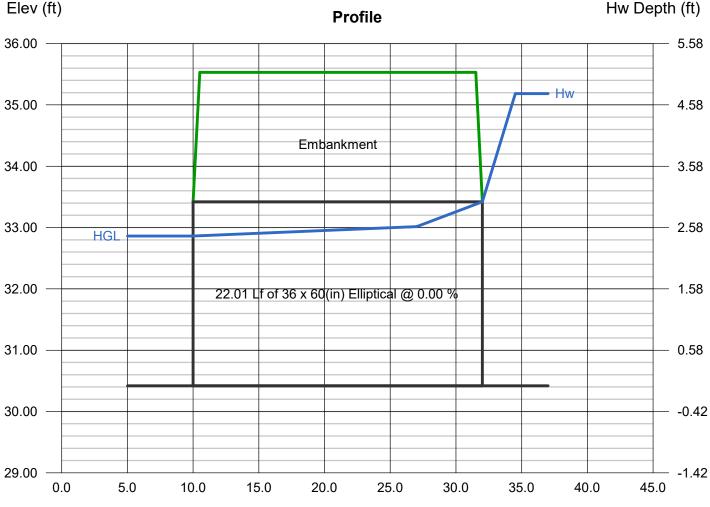
Culvert Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Monday, Mar 6 2017

Culvert 1 50yr

Invert Elev Dn (ft)	= 30.42	Calculations	
Pipe Length (ft)	= 22.01	Qmin (cfs)	= 98.00
Slope (%)	= 0.00	Qmax (cfs)	= 150.27
Invert Elev Up (ft)	= 30.42	Tailwater Élev (ft)	= Normal
Rise (in)	= 36.0	, ,	
Shape	= Elliptical	Highlighted	
Span (in)	= 60.0	Qtotal (cfs)	= 98.00
No. Barrels	= 1	Qpipe (cfs)	= 98.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	 Horizontal Ellipse Concrete 	Veloc Dn (ft/s)	= 9.19
Culvert Entrance	Square edge w/headwall (H)	Veloc Up (ft/s)	= 8.90
Coeff. K,M,c,Y,k	= 0.01, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 32.86
		HGL Up (ft)	= 33.06
Embankment		Hw Elev (ft)	= 35.18
Top Elevation (ft)	= 35.53	Hw/D (ft)	= 1.59
Top Width (ft)	= 21.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 300.00		
Elev (ft)	Profile		Hw Depth (ft)



Reach (ft)

Culvert Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Sunday, Mar 5 2017

Culvert 2, 25yr Storm

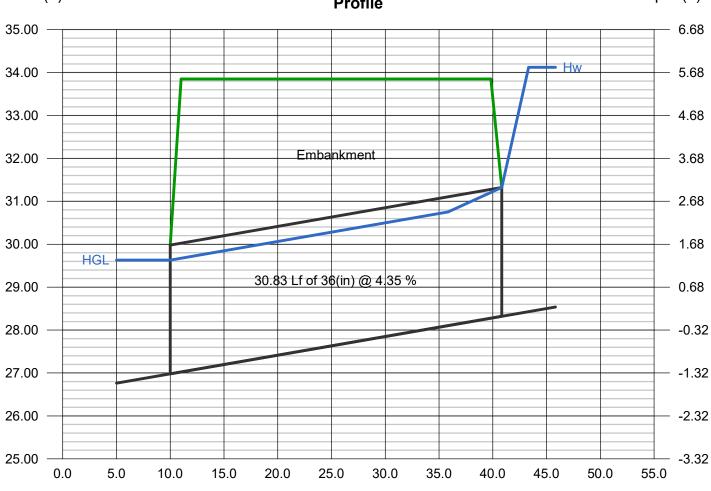
Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 26.98 = 30.83 = 4.35 = 28.32 = 36.0	Calculations Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 13.00 = 112.65 = Normal
Shape Span (in) No. Barrels n-Value Culvert Type Culvert Entrance Coeff. K,M,c,Y,k	= Circular = 36.0 = 1 = 0.013 = Circular Concrete = Square edge w/headwall (C) = 0.0098, 2, 0.0398, 0.67, 0.5	Highlighted Qtotal (cfs) Qpipe (cfs) Qovertop (cfs) Veloc Dn (ft/s) Veloc Up (ft/s) HGL Dn (ft) HGL Up (ft)	= 103.00 = 68.06 = 34.94 = 10.36 = 10.36 = 29.61 = 30.95
Embankment Top Elevation (ft) Top Width (ft) Crest Width (ft)	= 33.85 = 28.80 = 300.00	Hw Elev (ft) Hw/D (ft) Flow Regime	= 33.95 = 1.88 = Inlet Control
Elev (ft)	Profile		Hw Depth (ft)
34.00			5.68
33.00			4.68
32.00	Embankment		3.68
31.00			2.68
30.00 HGL			1.68
29.00	30.83 Lf of 36(in) @ 4.35	%	0.68
28.00			-0.32
27.00			-1.32
26.00			-2.32
25.00 0.0 5.0 1	10.0 15.0 20.0 25.0 30.0	35.0 40.0 45.0	50.0 55.0 -3.32

Reach (ft)

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Culvert 2 50 yr Existing Conditions

Cuiveit 2 30 yi Lx	isting conditions		
Invert Elev Dn (ft)	= 26.98	Calculations	
Pipe Length (ft)	= 30.83	Qmin (cfs)	= 13.00
Slope (%)	= 4.35	Qmax (cfs)	= 112.00
Invert Elev Up (ft)	= 28.32	Tailwater Élev (ft)	= Normal
Rise (in)	= 36.0		
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 112.00
No. Barrels	= 1	Qpipe (cfs)	= 69.57
n-Value	= 0.013	Qovertop (cfs)	= 42.43
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 10.53
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 10.53
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 29.63
		HGL Up (ft)	= 30.97
Embankment	00.05	Hw Elev (ft)	= 34.12
Top Elevation (ft)	= 33.85	Hw/D (ft)	= 1.93
Top Width (ft)	= 28.80	Flow Regime	= Inlet Control
Crest Width (ft)	= 100.00		II D (I (II)
Elev (ft)	Profile		Hw Depth (ft)
35.00			6.68
34.00			1 w 5.68
J 4 .00			5.06



Reach (ft)

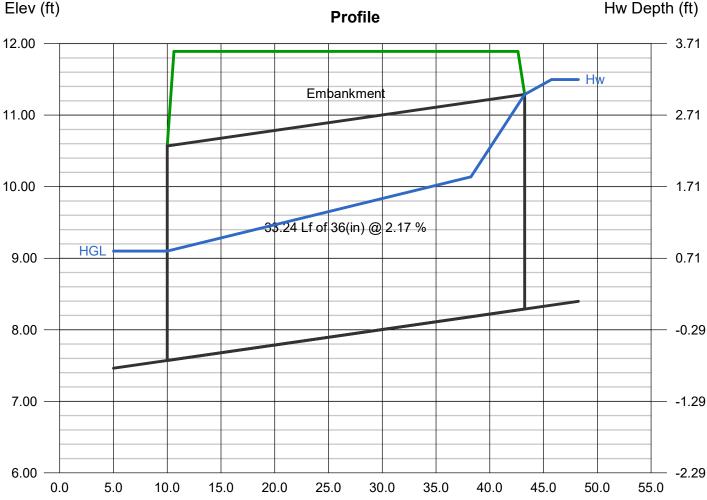
Culvert Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Sunday, Mar 5 2017

Culvert 3, 25 yr Storm

Invert Elev Dn (ft)	= 7.57	Calculations	
Pipe Length (ft)	= 33.24	Qmin (cfs)	= 37.00
Slope (%)	= 2.17	Qmax (cfs)	= 136.38
Invert Elev Up (ft)	= 8.29	Tailwater Elev (ft)	= Normal
Rise (in)	= 36.0		
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 117.00
No. Barrels	= 3	Qpipe (cfs)	= 117.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 10.77
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 7.66
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 9.10
		HGL Up (ft)	= 10.32
Embankment		Hw Elev (ft)	= 11.50
Top Elevation (ft)	= 11.89	Hw/D (ft)	= 1.07
Top Width (ft)	= 32.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 100.00		
Elev (ft)	Profile		Hw Depth (ft)



Reach (ft)

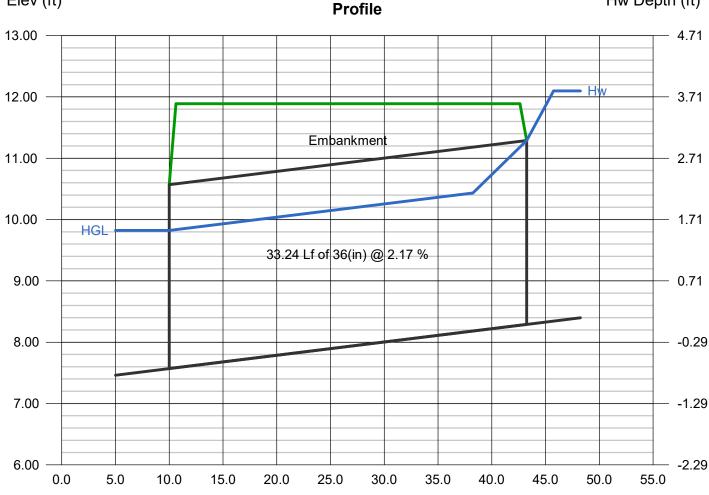
Culvert Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Monday, Feb 13 2017

Culvert 3 50yr Existing Conditions

Invert Elev Dn (ft)	= 7.57	Calculations	
Pipe Length (ft)	= 33.24	Qmin (cfs)	= 82.00
Slope (%)	= 2.17	Qmax (cfs)	= 181.23
Invert Elev Up (ft)	= 8.29	Tailwater Elev (ft)	= Normal
Rise (in)	= 36.0		
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 172.00
No. Barrels	= 3	Qpipe (cfs)	= 143.82
n-Value	= 0.013	Qovertop (cfs)	= 28.18
Culvert Type	 Circular Concrete 	Veloc Dn (ft/s)	= 8.42
Culvert Entrance	Square edge w/headwall (C)	Veloc Up (ft/s)	= 8.42
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 9.82
		HGL Up (ft)	= 10.54
Embankment		Hw Elev (ft)	= 12.10
Top Elevation (ft)	= 11.89	Hw/D (ft)	= 1.27
Top Width (ft)	= 32.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 100.00		
Elev (ft)	Profile		Hw Depth (ft)



Reach (ft)

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Sunday, Mar 5 2017

Culvert 2, 25yr Storm

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 26.98 = 30.83 = 4.35 = 28.32 = 36.0	Q Q	alculations emin (cfs) emax (cfs) ailwater Elev (ft)	= 13.00 = 112.65 = Normal
Shape Span (in) No. Barrels n-Value Culvert Type Culvert Entrance Coeff. K,M,c,Y,k	= Circular = 36.0 = 1 = 0.013 = Circular Concre = Square edge w = 0.0098, 2, 0.039	Q Q Q ete V v/headwall (C) V 98, 0.67, 0.5 H	ighlighted Itotal (cfs) Ipipe (cfs) Iovertop (cfs) Ieloc Dn (ft/s) Ieloc Up (ft/s) Ieloc Up (ft/s) Ieloc Up (ft)	= 103.00 = 68.06 = 34.94 = 10.36 = 10.36 = 29.61 = 30.95
Embankment Top Elevation (ft) Top Width (ft) Crest Width (ft) Elev (ft)	= 33.85 = 28.80 = 300.00	H H	w Elev (ft) w/D (ft) low Regime	= 33.95 = 1.88 = Inlet Control
34.00		FIOTHE	HV	N 5.68
33.00				4.68
32.00	E	Embankment		3.68
31.00				2.68
30.00				1.68
29.00 HGL	30.83 Lf	of 36(in) @ 4.35 %		0.68
28.00				-0.32
27.00				-1.32
26.00				-2.32
25.00 0.0 5.0	10.0 15.0 20.0	25.0 30.0 3	5.0 40.0 45.0	50.0 55.0 -3.32

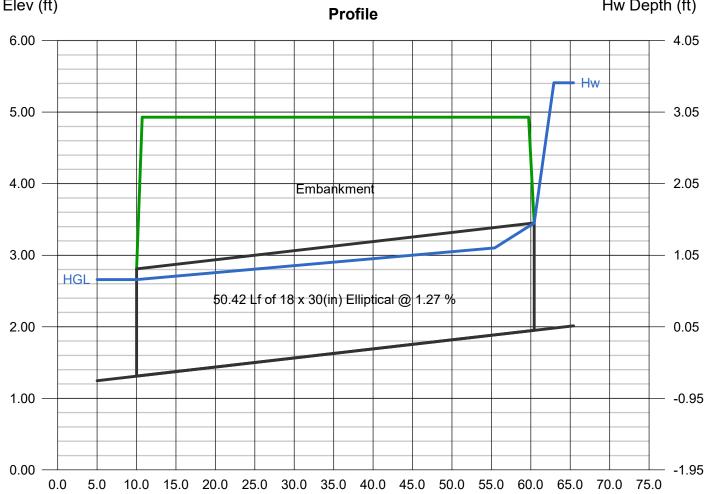
Reach (ft)

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Wednesday, Apr 5 2017

Culvert 4 25yr Existing Conditions

Invert Elev Dn (ft)	= 1.31	Calculations	
Pipe Length (ft)	= 50.42	Qmin (cfs)	= 75.00
Slope (%)	= 1.27	Qmax (cfs)	= 175.00
Invert Elev Up (ft)	= 1.95	Tailwater Élev (ft)	= (dc+D)/2
Rise (in)	= 18.0	, ,	, ,
Shape	= Elliptical	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 175.00
No. Barrels	= 3	Qpipe (cfs)	= 69.54
n-Value	= 0.013	Qovertop (cfs)	= 105.46
Culvert Type	= Horizontal Ellipse Concrete	Veloc Dn (ft/s)	= 8.20
Culvert Entrance	= Square edge w/headwall (H)	Veloc Up (ft/s)	= 9.05
Coeff. K,M,c,Y,k	= 0.01, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 2.66
		HGL Up (ft)	= 3.15
Embankment		Hw Elev (ft)	= 5.41
Top Elevation (ft)	= 4.93	Hw/D (ft)	= 2.31
Top Width (ft)	= 49.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 100.00	-	
Fley (ft)			Hw Denth (ft)

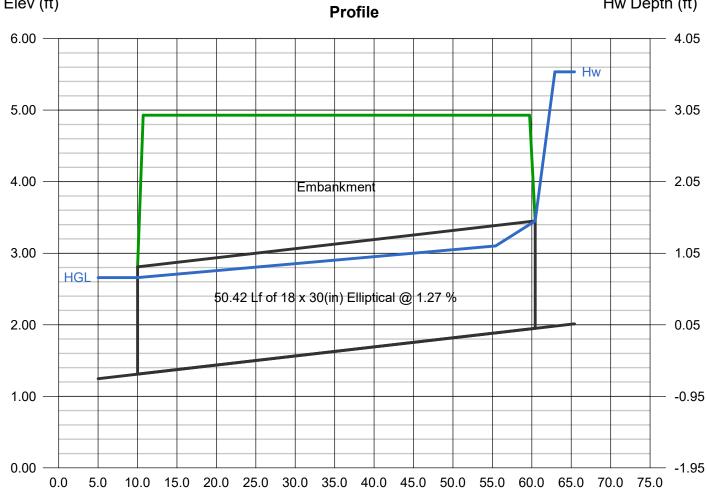


Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Wednesday, Apr 5 2017

Culvert 4 50yr Existing Conditions

Invert Elev Dn (ft)	= 1.31	Calculations	
Pipe Length (ft)	= 50.42	Qmin (cfs)	= 0.00
Slope (%)	= 1.27	Qmax (cfs)	= 228.03
Invert Elev Up (ft)	= 1.95	Tailwater Élev (ft)	= (dc+D)/2
Rise (in)	= 18.0		
Shape	= Elliptical	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 220.00
No. Barrels	= 3	Qpipe (cfs)	= 71.29
n-Value	= 0.013	Qovertop (cfs)	= 148.71
Culvert Type	 Horizontal Ellipse Concrete 	Veloc Dn (ft/s)	= 8.40
Culvert Entrance	Square edge w/headwall (H)	Veloc Up (ft/s)	= 9.27
Coeff. K,M,c,Y,k	= 0.01, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 2.66
		HGL Up (ft)	= 3.15
Embankment		Hw Elev (ft)	= 5.54
Top Elevation (ft)	= 4.93	Hw/D (ft)	= 2.39
Top Width (ft)	= 49.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 100.00		
Elev (ft)	— 411		Hw Depth (ft)



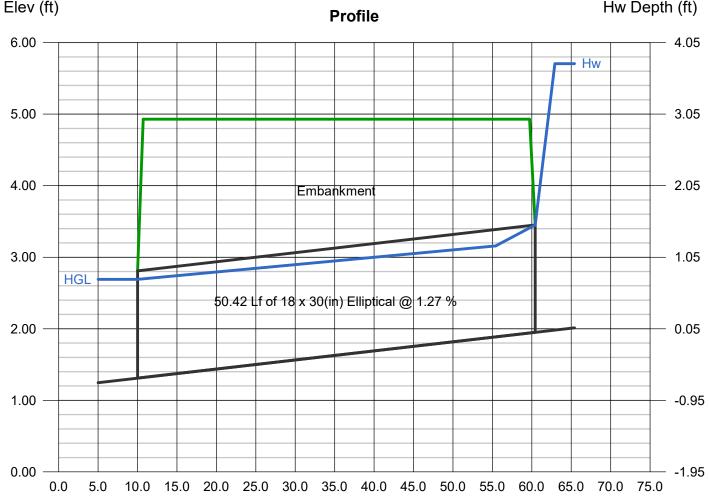
Reach (ft)

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Wednesday, Apr 5 2017

Culvert 4 100yr Existing Conditions

Invert Elev Dn (ft)	= 1.31	Calculations	
Pipe Length (ft)	= 50.42	Qmin (cfs)	= 200.00
Slope (%)	= 1.27	Qmax (cfs)	= 287.00
Invert Elev Up (ft)	= 1.95	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 18.0	. ,	, ,
Shape	= Elliptical	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 287.00
No. Barrels	= 3	Qpipe (cfs)	= 73.57
n-Value	= 0.013	Qovertop (cfs)	= 213.43
Culvert Type	 Horizontal Ellipse Concrete 	Veloc Dn (ft/s)	= 8.45
Culvert Entrance	Square edge w/headwall (H)	Veloc Up (ft/s)	= 9.20
Coeff. K,M,c,Y,k	= 0.01, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 2.69
		HGL Up (ft)	= 3.21
Embankment		Hw Elev (ft)	= 5.70
Top Elevation (ft)	= 4.93	Hw/D (ft)	= 2.50
Top Width (ft)	= 49.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 100.00		
Flev (ft)			Hw Depth (ft)



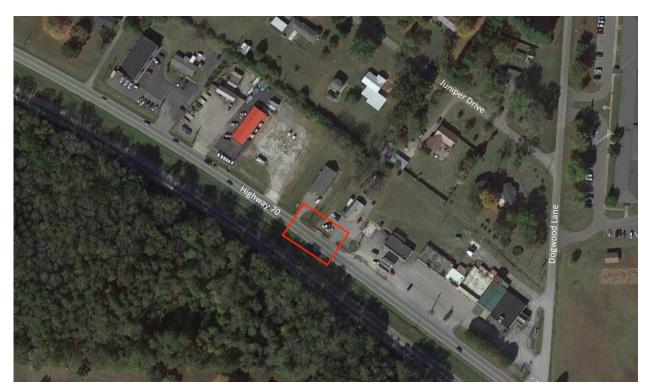


Enclosure (E): Design Development Package



Pegram Highway 70 Flood Remediation

Final Design Narrative (FOR THEORETICAL USE ONLY – NOT FOR CONSTRUCTION) April 2017



Highway 70 Shopping Area 500 Block Hwy 70 Pegram, TN 37143

Enclosures:

- A. Design Development Drawings
- B. Hydrology Report
- C. Culvert / Channel Analysis Reports
- D. Construction Cost Estimate
- E. Maintenance Agreement

Contributors:

Nathan Curtis David Lowery Cody Glenn Abigail Queen Christian Reid



Introduction:

The Lipscomb University senior design team was asked by the city of Pegram to address a flooding issue that takes place at three culverts running under Highway 70 near the 500 block. It was suspected that these culverts were not meeting TDOT standards, however there was no qualitative data to back up the claim. The following is our analysis of the existing conditions of the culverts at the 500 block of Hwy 70 as well as the culverts along the flow path to Hwy 70.

Research & Analysis:

We set out in the fall of 2017 to gather survey data around the place of flooding, in hopes that it would help inform our hydraulic analysis. Our survey covered the area bounded by Highway 70, Dogwood Lane, and Hannah Ford Road. The completed survey can be seen in enclosure (A). This data, along with GIS data, was used to analyze the watershed and current culvert conditions. We found that each of the culverts along the flow path of interest (flowing south from Hannah Ford Rd along the ditch to HWY 70), are failing per TDOT standards as seen in Figure 1.

TDOT Standards:

	Interstate System and Arterial With Full Access Control	Arterial Without Full Access Control	Collector	Local Road
Inlet Design Frequency	50-yr	10-yr ¹	10-yr ¹	10-yr
Sewer Design Frequency	50-yr	10-yr ¹	10-yr ¹	10-yr
Culvert Design Frequency	50-yr Check for 100-yr	50-yr Check for 100-yr	50-yr Check for 100-yr	50-yr Check for 100-yr
Roadway Freeboard ²	50-yr	50-yr	50-yr	50-yr
Ditch Design Frequency	50-yr	10-yr ¹	10-yr ¹	10-yr

Figure 1 TDOT Current Culvert Standards

Per the TDOT standards shown above, all culverts are to be designed for a 50 year storm, and if feasible, for the 100 year storm. Each of the culverts along the flow path are failing under the 50-year storm conditions.

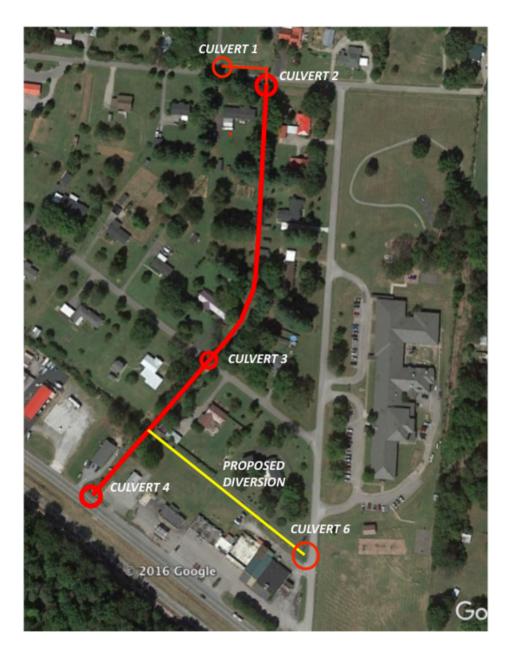


Figure 2. Naming Convention

For ease of reference, *Figure 2 (Above)* shows the naming convention used for each of the culverts along the flow path. This can be seen in more detail in *Enclosure (A)*.

The results of our analysis for a both the existing conditions, as well as proposed conditions during a 50 year storm event can be seen summarized in *Table 1* (below).

	CUL	VERT DATA ALONG FLOWP.	ATH FOR 50 YEA	AR STORM	- EXISTING	
CULVERT NAME	# OF CULVERTS	SIZE OF CULVERTS	CULVERT CAPACITY (CFS)	TOTAL INCOMING FLOW (CFS)	FLOW OVERTOPPING (CFS)	DEPTH OF FLOW OVERTOPPING ROAD
1	1	36X60" ELLIPTICAL	106	148	41	3 IN.
2	1	36" ROUND	68	103	34	1.8 IN.
3	3	36" ROUND	143	172	28	2.4 IN.
4	3	18X30" ELLIPTICAL	64	220	125	5 IN.

CULVERT DATA ALONG FLOWPATH FOR 50 YEAR STORM — AFTER PROPOSED CONSTRUCTION						
CULVERT NAME	# OF CULVERTS	SIZE OF CULVERTS	CULVERT CAPACITY (CFS)	TOTAL INCOMING FLOW (CFS)	FLOW OVERTOPPING (CFS)	
1	1	36X60" ELLIPTICAL	106	37	0	
2	1	36" ROUND	68	37	0	
3	3	36" ROUND	143	65	0	
4	3	18X30" ELLIPTICAL	64	47	0	
6	3	24X40" ELLIPTICAL	100	95	0	

Table 1 Culvert Analysis under 50-yr Storm Conditions

Proposed Solution:

Diversion:

It has been concluded that diverting 75cfs of water toward culvert 6 is the best course of action as it affords the use of a much smaller pond than is necessary without diversion. Because there is only 0.4% grade difference between the diversion location along the existing flow path, and the inflow invert of culvert 6, it is necessary to use a concrete channel to divert the water. A concrete channel 8' wide and 2' deep accommodates the needed 75cfs.



Detention & Diversion:

The use of a detention pond of approximately 1.5 acres, in conjunction with the diversion of 75cfs to culvert 6, is the cheapest and most efficient solution to remediate the flooding issues at Hwy 70 and allow all culverts along the flow path to pass under 50 year storm conditions. Without diverting any water away from the existing flow path, the needed pond area would consist of one 3 acre pond, and a second ½ acre pond. With use of diversion, we were able to consolidate the needed pond area to a single 1.5 acre pond placed north of Hannah Ford Rd. In order to aid in acquiring permission from the landowner to allow the placement of the pond on her property, the pond was designed as a wet pond intended for the livestock. The pond will hold a 3ft depth of water across the entire 1.5 acre pond, and when the water level rises in a storm event, the pond can hold up to 8ft of water over its entire length, and will drain slowly back to 3 ft.

Sincerely,

David Lowery

(615) 881-3973

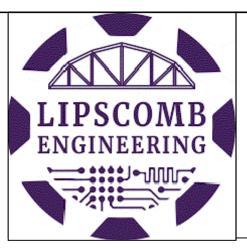
loweryda@mail.lipscomb.edu

David A Lower



ENCLOSURE (A)

CONSTRUCTION DRAWINGS



LIPSCOMB UNIVERSITY RAYMOND B. JONES COLLEGE OF ENGINEERING

PEGRAM FLOOD REMEDIATION PROJECT DESIGN DEVELOPMENT DRAWINGS - NOT FOR CONSTRUCTION



SITE LOCATION: HIGHWAY 70 SHOPPING AREA 500 BLOCK HIGHWAY 70 PEGRAM, TN 37143

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C1.0 COVER SHEET

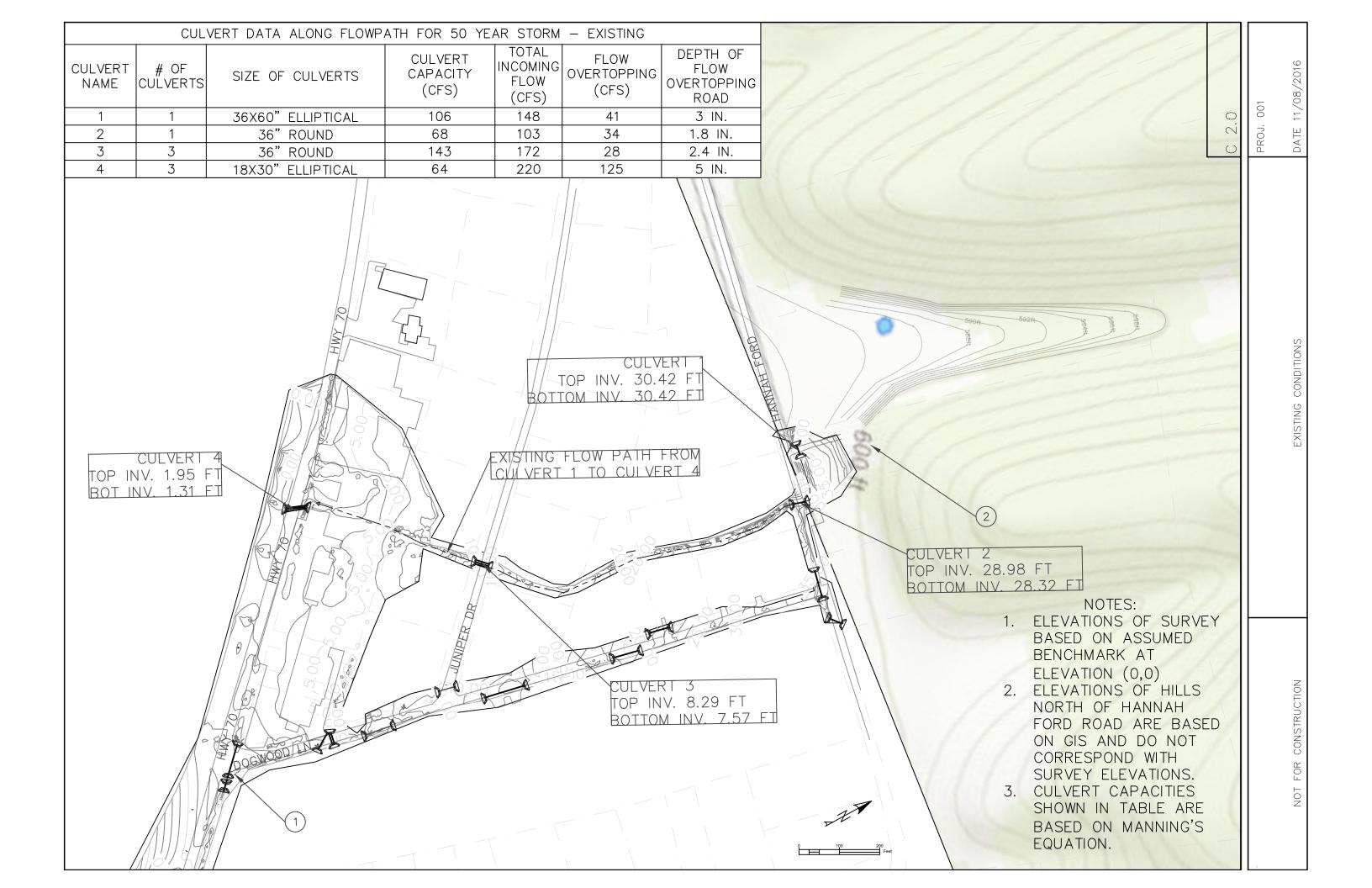
C2.0 EXISTING CONDITIONS

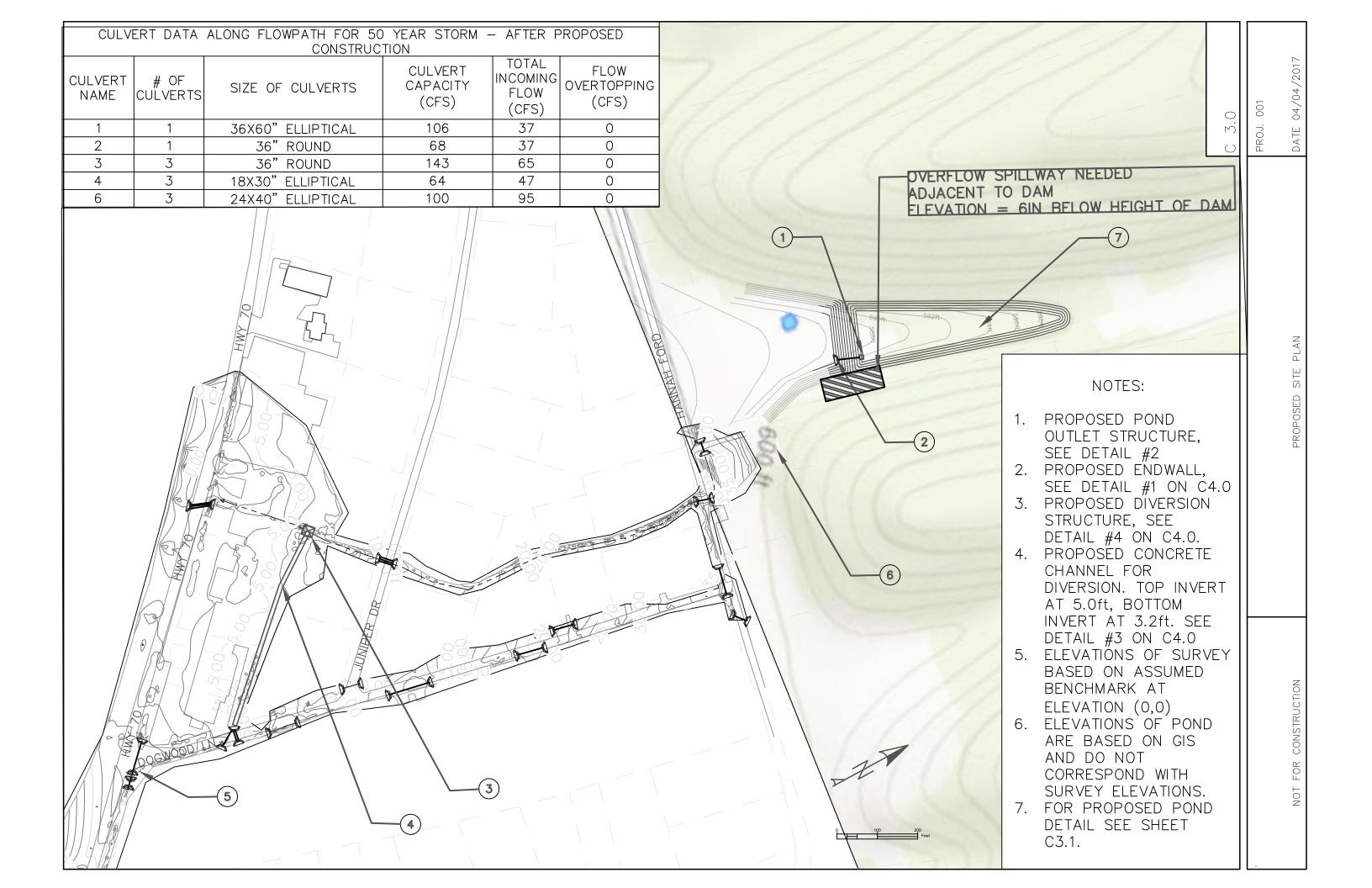
C3.0 PROPOSED SITE PLAN

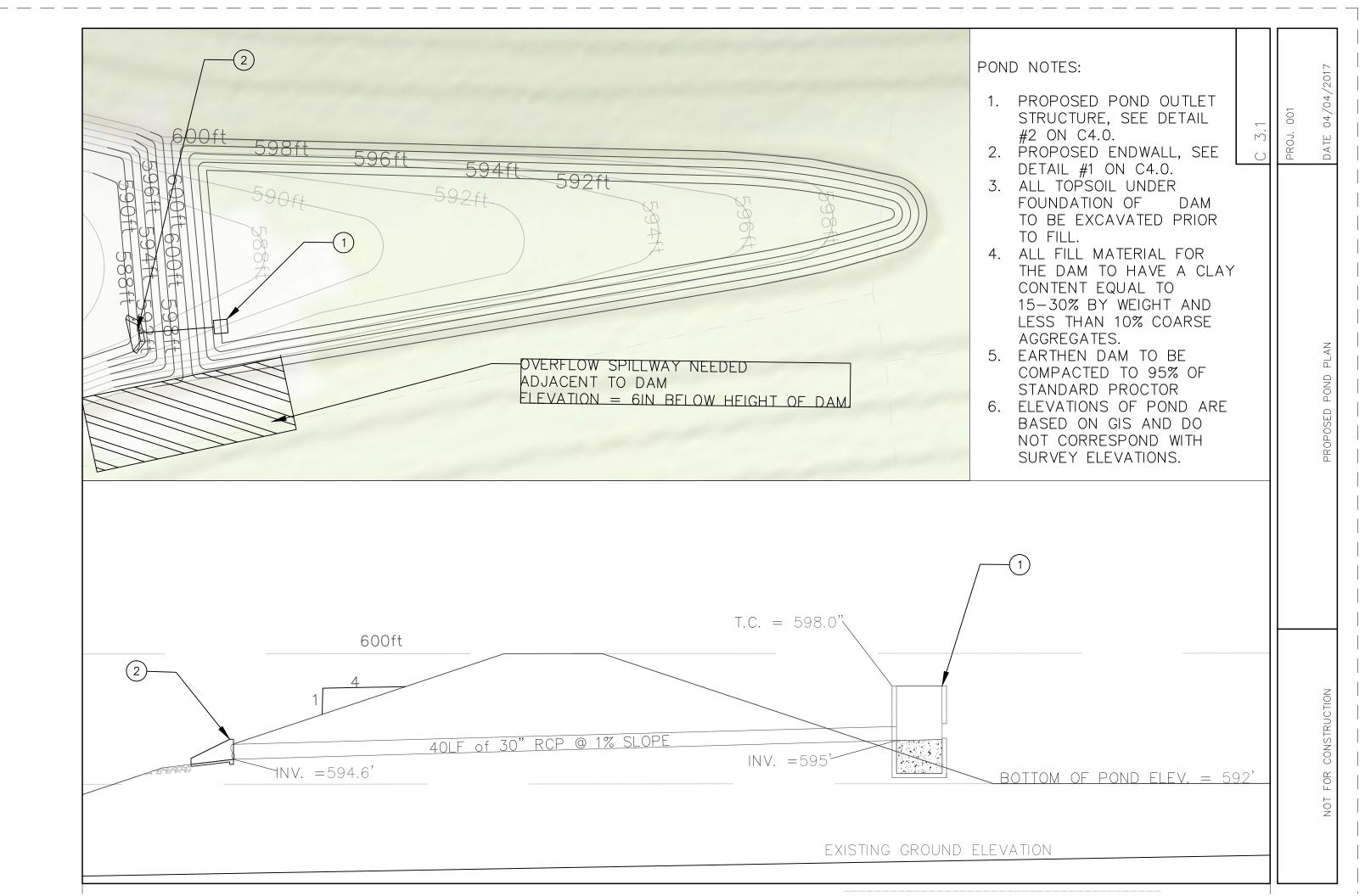
C3.1 PROPOSED POND PLAN

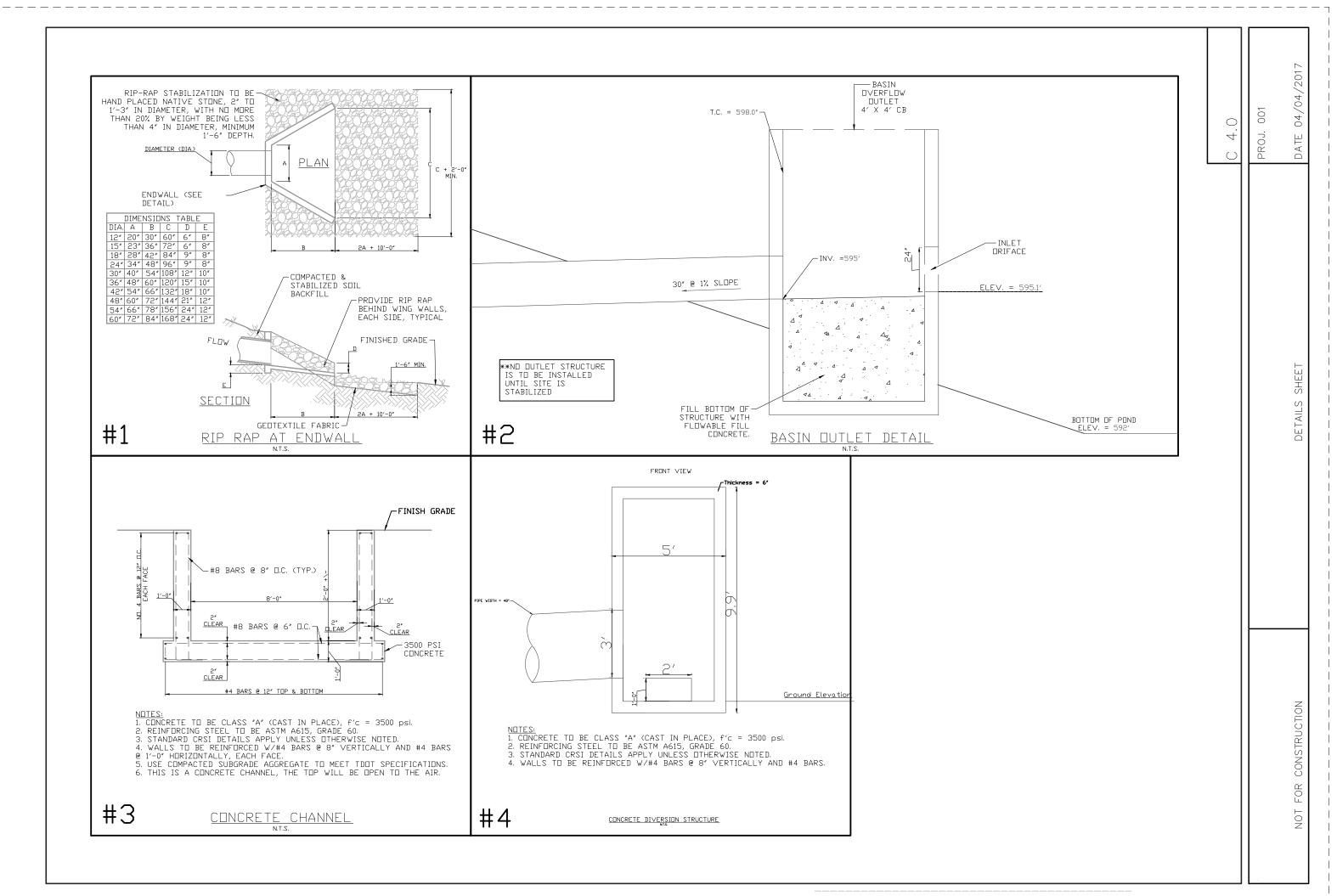
C4.0 DETAIL SHEET

PRESENTED BY: NATHAN CURTIS CODY GLENN DAVID LOWERY ABBY QUEEN CHRISTIAN REID











ENCLOSURE (B)

HYDROLOGY REPORT

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Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

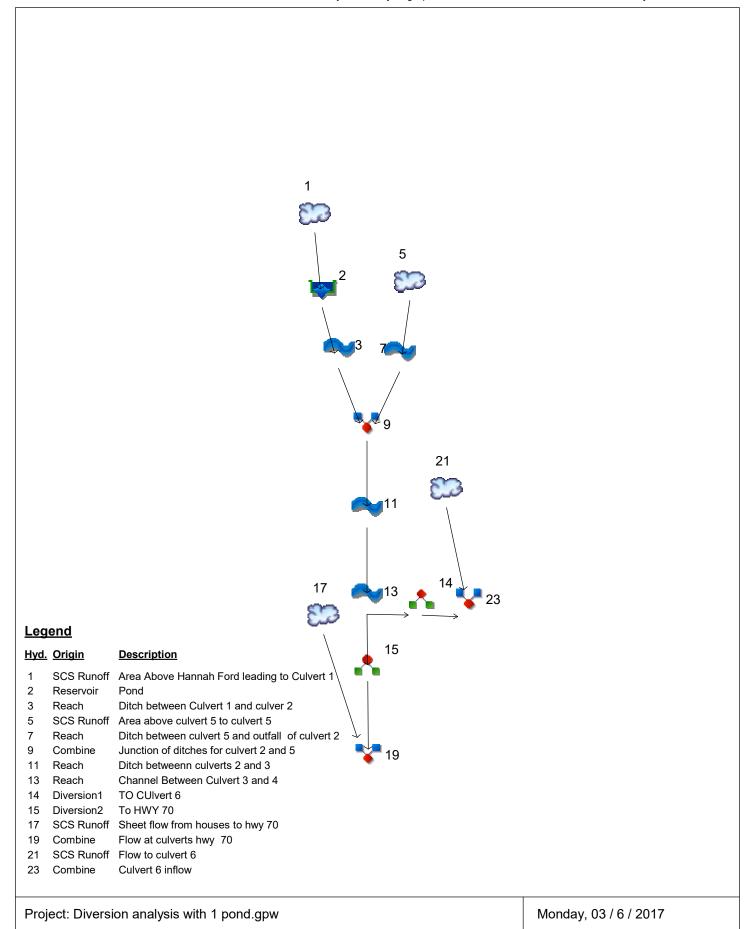
Tuesday, 03 / 28 / 2017

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Watershed Model Schematic Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11



Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	19.31	1	739	153,782				Area Above Hannah Ford leading to
2	Reservoir	0.481	1	1470	13,393	1	38.37	151,119	Pond
3	Reach	0.481	1	1472	13,390	2			Ditch between Culvert 1 and culver 2
5	SCS Runoff	11.25	1	725	42,927				Area above culvert 5 to culvert 5
7	Reach	11.24	1	726	42,926	5			Ditch between culvert 5 and outfall of
9	Combine	11.24	1	726	56,316	3, 7,			Junction of ditches for culvert 2 and 5
11	Reach	10.35	1	730	56,305	9			Ditch betweenn culverts 2 and 3
13	Reach	9.930	1	733	56,296	11			Channel Between Culvert 3 and 4
14	Diversion1	9.930	1	733	56,296	13			TO CUlvert 6
15	Diversion2	0.000	1	n/a	0	13			To HWY 70
17	SCS Runoff	12.98	1	739	71,713				Sheet flow from houses to hwy 70
19	Combine	12.98	1	739	71,713	15, 17,			Flow at culverts hwy 70
21	SCS Runoff	6.184	1	725	19,948				Flow to culvert 6
23	Combine	14.51	1	731	76,244	14, 21,			Culvert 6 inflow
	ersion analys	is with 1	nond (1)	anw	Return F	Period: 2 Ye	ear	Tuesday	03 / 28 / 2017

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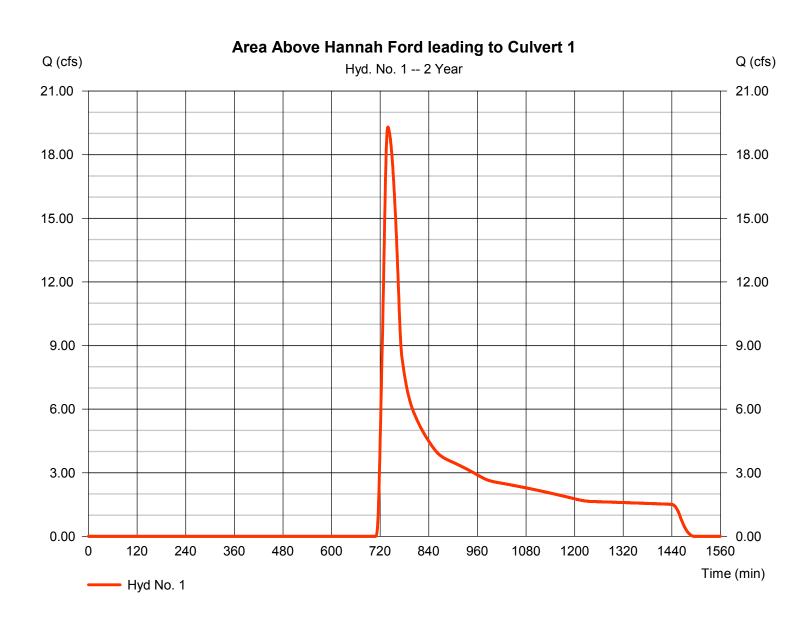
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Hyd. No. 1

Area Above Hannah Ford leading to Culvert 1

Hydrograph type = SCS Runoff Peak discharge = 19.31 cfsStorm frequency Time to peak = 739 min = 2 yrsTime interval = 1 min Hyd. volume = 153.782 cuft Curve number Drainage area = 100.000 ac= 56* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 34.70 min = TR55 Total precip. Distribution = Type II = 3.62 inStorm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = [(17.000 x 36) + (83.000 x 60)] / 100.000



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Hyd. No. 1Area Above Hannah Ford leading to Culvert 1

<u>Description</u>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>	
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.400 = 150.0 = 3.62 = 5.00		0.400 0.0 3.62 0.00		0.050 0.0 3.62 0.00			
Travel Time (min)	= 19.36	+	0.00	+	0.00	=	19.36	
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 1610.00 = 4.00 = Unpaved =3.23	l	0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00			
Travel Time (min)	= 8.32	+	0.00	+	0.00	=	8.32	
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 12.00 = 8.00 = 2.00 = 0.050 =5.53		0.00 0.00 0.00 0.015 0.00		0.00 0.00 0.00 0.015			
X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value	= 8.00 = 2.00 = 0.050		0.00 0.00 0.015		0.00 0.00 0.015			
X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 8.00 = 2.00 = 0.050 =5.53	+	0.00 0.00 0.015 0.00	+	0.00 0.00 0.015 0.00	=	7.07	

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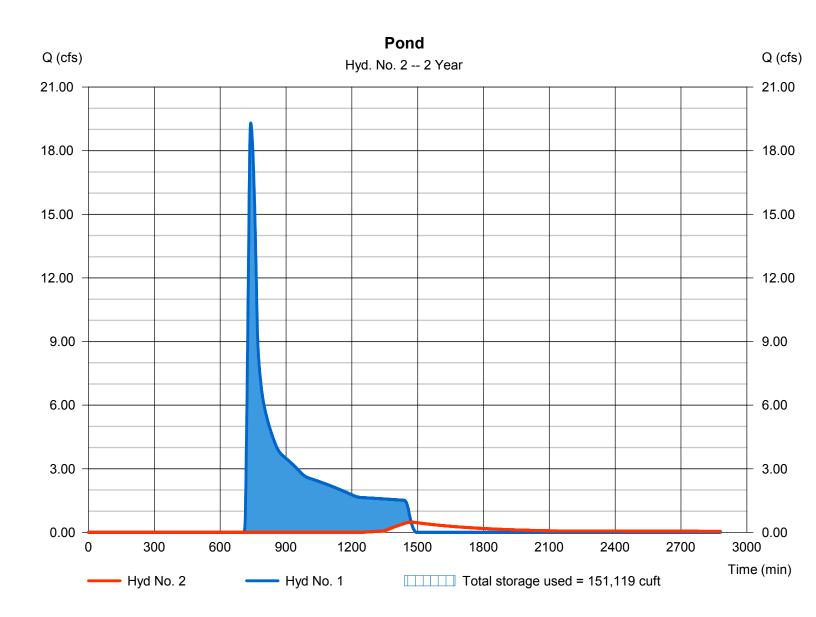
Tuesday, 03 / 28 / 2017

Hyd. No. 2

Pond

Hydrograph type Peak discharge = 0.481 cfs= Reservoir Storm frequency Time to peak = 2 yrs = 1470 min Time interval = 1 min Hyd. volume = 13,393 cuft Inflow hyd. No. = 1 - Area Above Hannah Ford levading tevatibrert 1 = 38.37 ftMax. Storage = Pond Paired with Diversion Reservoir name = 151,119 cuft

Storage Indication method used.



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Tuesday, 03 / 28 / 2017

Pond No. 1 - Pond Paired with Diversion

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 35.00 ft

Stage / Storage Table

Stage (ft)	Elevation (ft) Contour are		Incr. Storage (cuft)	Total storage (cuft)		
0.00	35.00	38,532	0	0		
2.00	37.00	45,517	83,944	83,944		
4.00	39.00	52,844	98,260	182,204		
6.00	41.00	60,287	113,038	295,242		
8.00	43.00	67,801	128,002	423,243		

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 30.00	24.00	0.00	0.00	Crest Len (ft)	= 4.00	3.00	0.00	0.00
Span (in)	= 30.00	24.00	0.00	0.00	Crest El. (ft)	= 42.50	42.00	0.00	0.00
No. Barrels	= 2	1	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 38.00	38.10	0.00	0.00	Weir Type	= 1	Rect		
Length (ft)	= 50.00	0.00	0.00	0.00	Multi-Stage	= Yes	Yes	No	No
Slope (%)	= 1.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 0.000 (by	Wet area)		
Multi-Stage	= n/a	Yes	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	35.00	0.00	0.00			0.00	0.00					0.000
2.00	83,944	37.00	0.00	0.00			0.00	0.00					0.000
4.00	182,204	39.00	4.42 ic	4.40 ic			0.00	0.00					4.398
6.00	295,242	41.00	20.11 ic	19.78 ic			0.00	0.00					19.78
8.00	423,243	43.00	39.47 oc	24.77 ic			4.71	9.99					39.47

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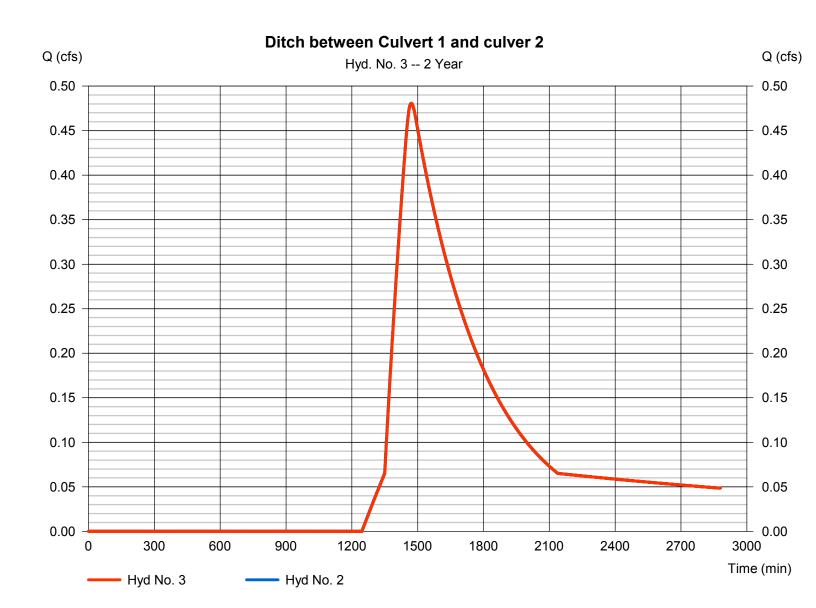
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Hyd. No. 3

Ditch between Culvert 1 and culver 2

Hydrograph type	= Reach	Peak discharge	= 0.481 cfs
Storm frequency	= 2 yrs	Time to peak	= 1472 min
Time interval	= 1 min	Hyd. volume	= 13,390 cuft
Inflow hyd. No.	= 2 - Pond	Section type	= Trapezoidal
Reach length	= 118.0 ft	Channel slope	= 1.8 %
Manning's n	= 0.030	Bottom width	= 3.0 ft
Side slope	= 3.0:1	Max. depth	= 5.0 ft
Rating curve x	= 3.202	Rating curve m	= 1.279
Ave. velocity	= 0.00 ft/s	Routing coeff.	= 0.8155

Modified Att-Kin routing method used.



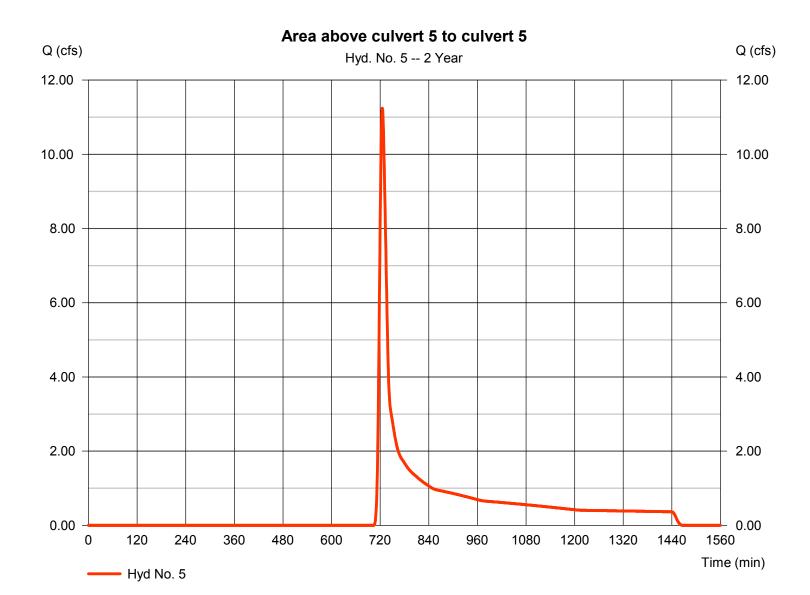
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Tuesday, 03 / 28 / 2017

Hyd. No. 5

Area above culvert 5 to culvert 5

= 11.25 cfsHydrograph type = SCS Runoff Peak discharge Storm frequency = 2 yrsTime to peak = 725 min Time interval = 1 min Hyd. volume = 42,927 cuft Drainage area Curve number = 20.000 ac= 60 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 16.77 min = TR55 Total precip. = 3.62 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



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Hyd. No. 5Area above culvert 5 to culvert 5

<u>Description</u>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.400 = 150.0 = 3.62 = 14.00		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 12.82	+	0.00	+	0.00	=	12.82
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 1350.00 = 12.50 = Unpave =5.70		0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 3.94	+	0.00	+	0.00	=	3.94
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 0.00 = 0.00 = 0.00 = 0.015 =0.00		0.00 0.00 0.00 0.015 0.00		0.00 0.00 0.00 0.015		
Flow length (ft)	({0})0.0		0.0		0.0		
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc							16.77 min

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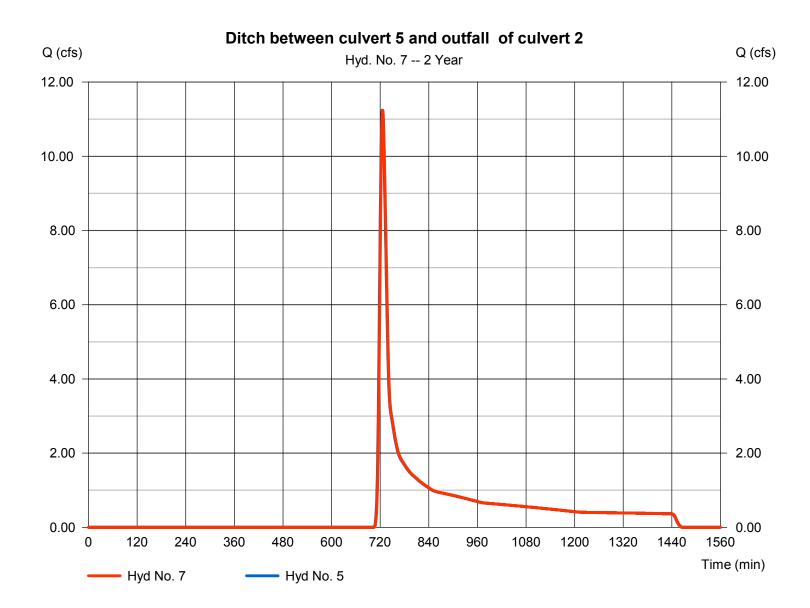
Tuesday, 03 / 28 / 2017

Hyd. No. 7

Ditch between culvert 5 and outfall of culvert 2

= Reach Peak discharge = 11.24 cfsHydrograph type Storm frequency = 2 yrs Time to peak = 726 min Time interval = 1 min Hyd. volume = 42.926 cuft Inflow hyd. No. = 5 - Area above culvert 5 to c = Trapezoidal Reach length Channel slope = 3.8 % = 174.0 ftBottom width = 3.0 ftManning's n = 0.040Side slope Max. depth = 2.0 ft= 2.0:1Rating curve x Rating curve m = 1.249= 3.490Ave. velocity Routing coeff. = 0.9741= 0.00 ft/s

Modified Att-Kin routing method used.



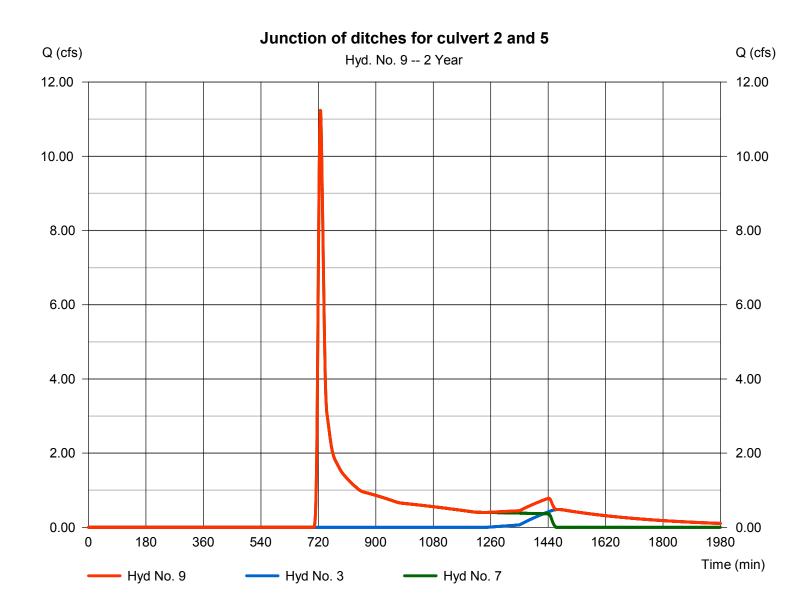
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Tuesday, 03 / 28 / 2017

Hyd. No. 9

Junction of ditches for culvert 2 and 5

= 11.24 cfsHydrograph type = Combine Peak discharge Storm frequency Time to peak = 726 min = 2 yrsTime interval = 1 min Hyd. volume = 56,316 cuft Inflow hyds. = 3, 7 Contrib. drain. area = 0.000 ac



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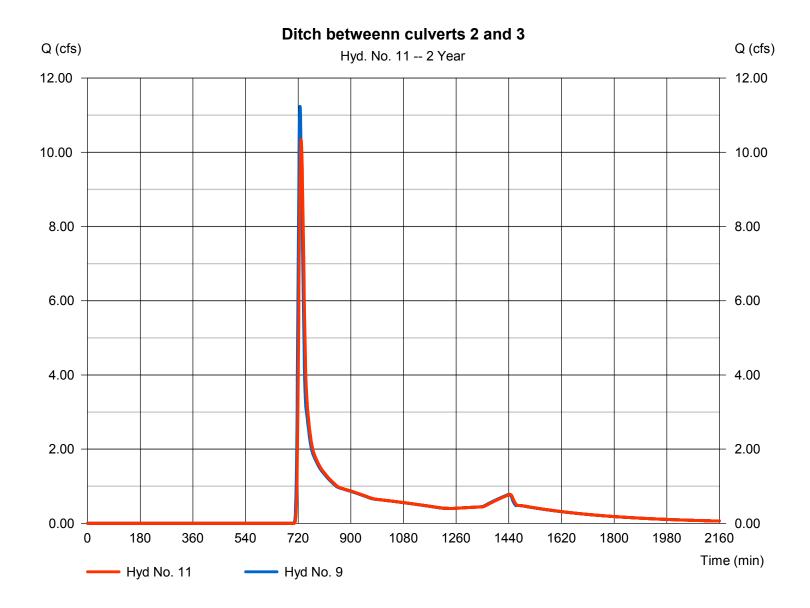
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Hyd. No. 11

Ditch betweenn culverts 2 and 3

Hydrograph type = Reach Peak discharge = 10.35 cfsStorm frequency = 2 yrs Time to peak = 730 min Time interval = 1 min Hyd. volume = 56.305 cuft = 9 - Junction of ditches for culveste2tandtspe Inflow hyd. No. = Trapezoidal Reach length Channel slope = 815.0 ft= 2.3 % Bottom width = 5.0 ftManning's n = 0.040Side slope Max. depth = 3.0:1= 5.0 ftRating curve x Rating curve m = 1.931= 1.341Ave. velocity Routing coeff. = 0.00 ft/s= 0.2597

Modified Att-Kin routing method used.



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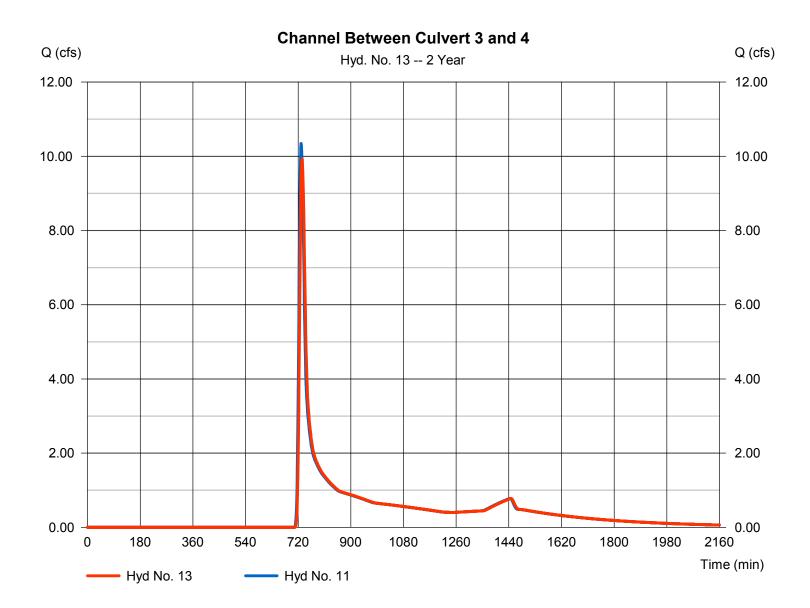
Tuesday, 03 / 28 / 2017

Hyd. No. 13

Channel Between Culvert 3 and 4

Hydrograph type Peak discharge = 9.930 cfs= Reach Storm frequency = 2 yrs Time to peak = 733 min Time interval = 1 min Hyd. volume = 56.296 cuft Inflow hyd. No. = 11 - Ditch betweenn culverts 2 Spection type = Trapezoidal = 1.2 % Reach length = 450.0 ftChannel slope Bottom width = 5.0 ftManning's n = 0.040Side slope Max. depth = 3.0 ft= 3.0:1Rating curve x Rating curve m = 1.395= 1.321Ave. velocity Routing coeff. = 0.3331= 0.00 ft/s

Modified Att-Kin routing method used.



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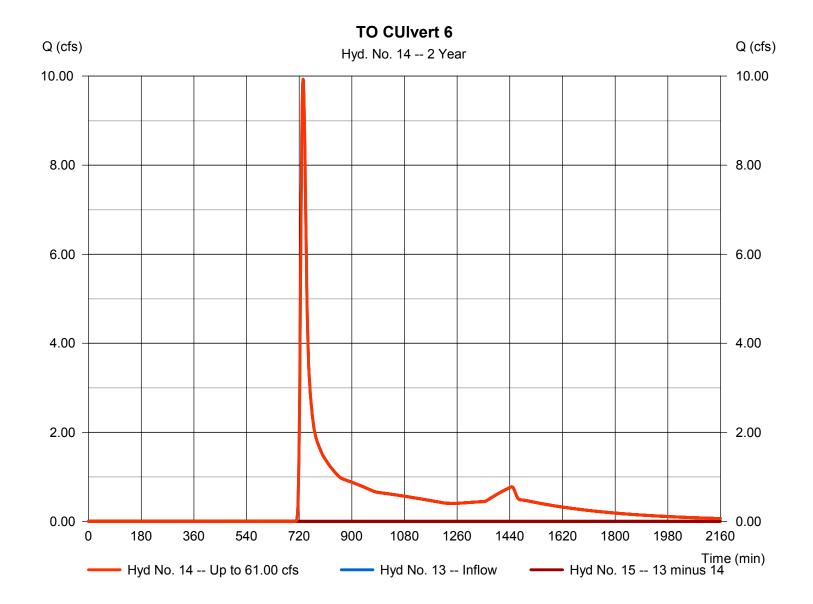
Hyd. No. 14

TO CUIvert 6

Hydrograph type= Diversion1Peak discharge= 9.930 cfsStorm frequency= 2 yrsTime to peak= 733 minTime interval= 1 minHyd. volume= 56,296 cuft

Inflow hydrograph = 13 - Channel Between Culvert 2 mathdli 4 erted hyd. = 15

Diversion method = Constant Q Constant Q = 61.00 cfs



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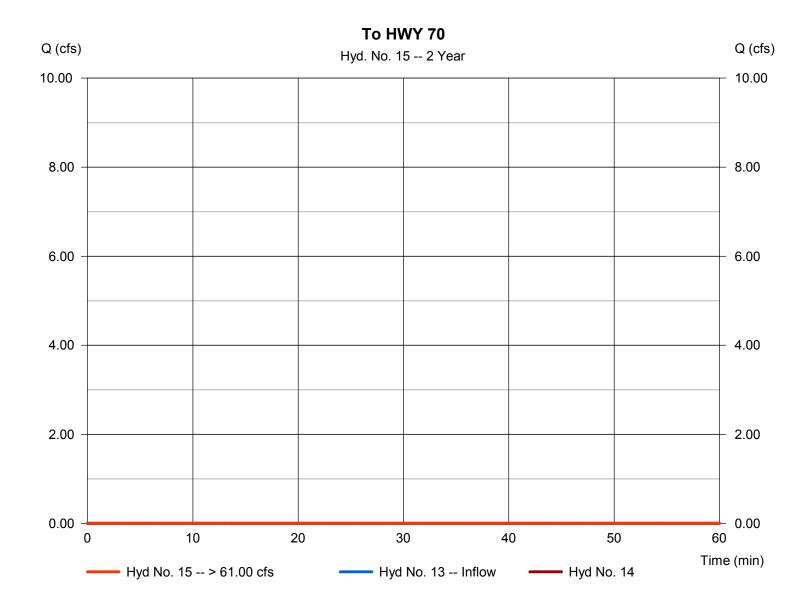
Tuesday, 03 / 28 / 2017

Hyd. No. 15

To HWY 70

Hydrograph type= Diversion2Peak discharge= 0.000 cfsStorm frequency= 2 yrsTime to peak= n/aTime interval= 1 minHyd. volume= 0 cuftInflow hydrograph= 13 - Channel Between Culvert 2nathdiverted hyd.= 14

Diversion method = Constant Q Constant Q = 61.00 cfs



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Tuesday, 03 / 28 / 2017

Hyd. No. 17

Sheet flow from houses to hwy 70

Hydrograph type = SCS Runoff Peak discharge = 12.98 cfsStorm frequency = 2 yrsTime to peak = 739 min Time interval = 1 min Hyd. volume = 71,713 cuft Drainage area Curve number = 20.330 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 39.63 min = TR55 Total precip. Distribution = Type II = 3.62 inShape factor Storm duration = 24 hrs = 484



TR55 Tc Worksheet

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Hyd. No. 17Sheet flow from houses to hwy 70

<u>Description</u>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%) Travel Time (min)	= 0.400 = 150.0 = 3.62 = 2.00	+	0.011 0.0 0.00 0.00 0.00	+	0.011 0.0 0.00 0.00 0.00	=	27.93
, ,							
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 1602.00 = 2.00 = Unpaved =2.28		0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 11.70	+	0.00	+	0.00	=	11.70
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 0.00 = 0.00 = 0.00 = 0.015 =0.00		0.00 0.00 0.00 0.015 0.00		0.00 0.00 0.00 0.015		
Flow length (ft)	({0})0.0		0.0		0.0		
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc							39.63 min

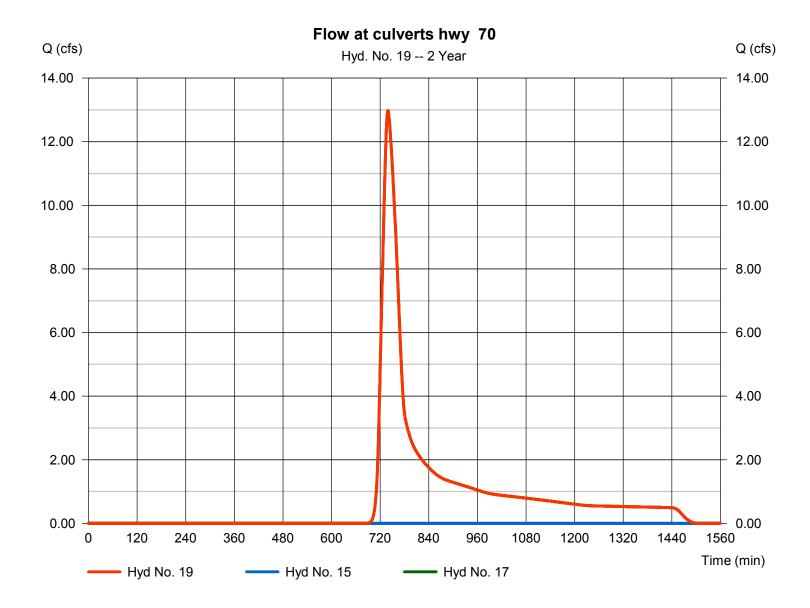
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Tuesday, 03 / 28 / 2017

Hyd. No. 19

Flow at culverts hwy 70

Hydrograph type = Combine Peak discharge = 12.98 cfsStorm frequency = 2 yrsTime to peak = 739 min Time interval = 1 min Hyd. volume = 71,713 cuft Inflow hyds. = 15, 17 Contrib. drain. area = 20.330 ac



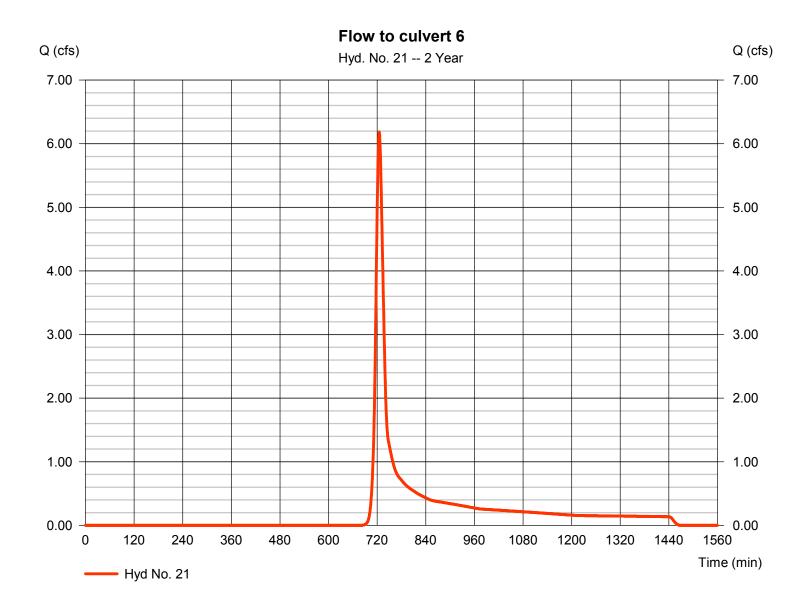
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Tuesday, 03 / 28 / 2017

Hyd. No. 21

Flow to culvert 6

Hydrograph type = SCS Runoff Peak discharge = 6.184 cfsStorm frequency = 2 yrsTime to peak = 725 min Time interval = 1 min Hyd. volume = 19.948 cuft Drainage area Curve number = 5.720 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 17.80 min = TR55 Total precip. = 3.62 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



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Hyd. No. 21

Flow to culvert 6

<u>Description</u>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.150 = 150.0 = 3.62 = 2.70		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 11.30	+	0.00	+	0.00	=	11.30
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 1030.00 = 2.70 = Unpaved =2.65	t	0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 6.48	+	0.00	+	0.00	=	6.48
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 0.00 = 0.00 = 0.00 = 0.015 =0.00		0.00 0.00 0.00 0.015 0.00		0.00 0.00 0.00 0.015		
Flow length (ft)	({0})0.0		0.0		0.0		
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc							17.80 min

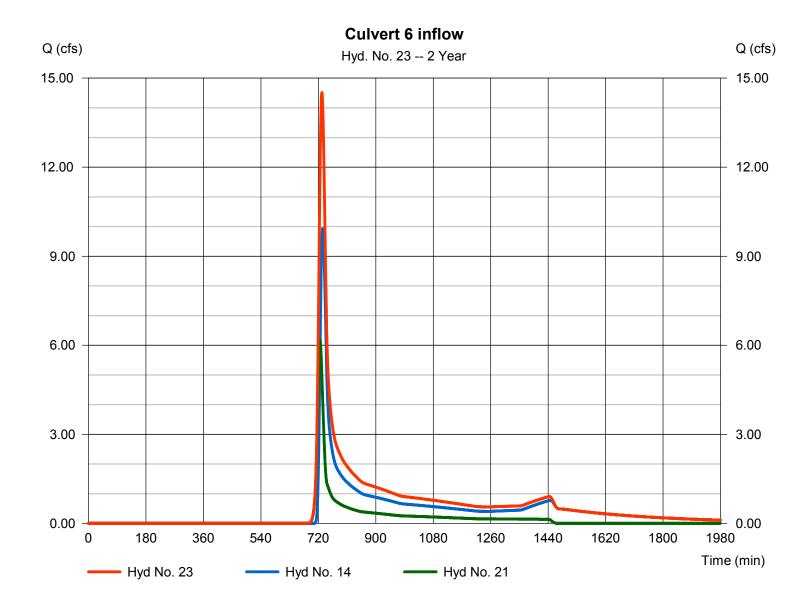
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Tuesday, 03 / 28 / 2017

Hyd. No. 23

Culvert 6 inflow

Hydrograph type = Combine Peak discharge = 14.51 cfsStorm frequency Time to peak = 2 yrs= 731 min Time interval = 1 min Hyd. volume = 76,244 cuft Inflow hyds. = 14, 21 Contrib. drain. area = 5.720 ac



Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	44.33	1	737	273,458				Area Above Hannah Ford leading to
2	Reservoir	3.563	1	1078	132,237	1	38.89	177,037	Pond
3	Reach	3.563	1	1079	132,234	2			Ditch between Culvert 1 and culver 2
5	SCS Runoff	21.71	1	724	71,414				Area above culvert 5 to culvert 5
7	Reach	21.72	1	725	71,413	5			Ditch between culvert 5 and outfall of
9	Combine	21.72	1	725	203,647	3, 7,			Junction of ditches for culvert 2 and 5
11	Reach	20.44	1	729	203,636	9			Ditch betweenn culverts 2 and 3
13	Reach	19.82	1	731	203,628	11			Channel Between Culvert 3 and 4
14	Diversion1	19.82	1	731	203,628	13			TO CUIvert 6
15	Diversion2	0.000	1	n/a	0	13			To HWY 70
17	SCS Runoff	20.93	1	738	108,627				Sheet flow from houses to hwy 70
19	Combine	20.93	1	738	108,627	15, 17,			Flow at culverts hwy 70
21	SCS Runoff	9.799	1	725	30,216				Flow to culvert 6
23	Combine	27.66	1	730	233,843	14, 21,			Culvert 6 inflow
— Div	ersion analys	is with 1 r	ond (1)	apw	Return F	eriod: 5 Ye	 ear	Tuesday ()3 / 28 / 2017

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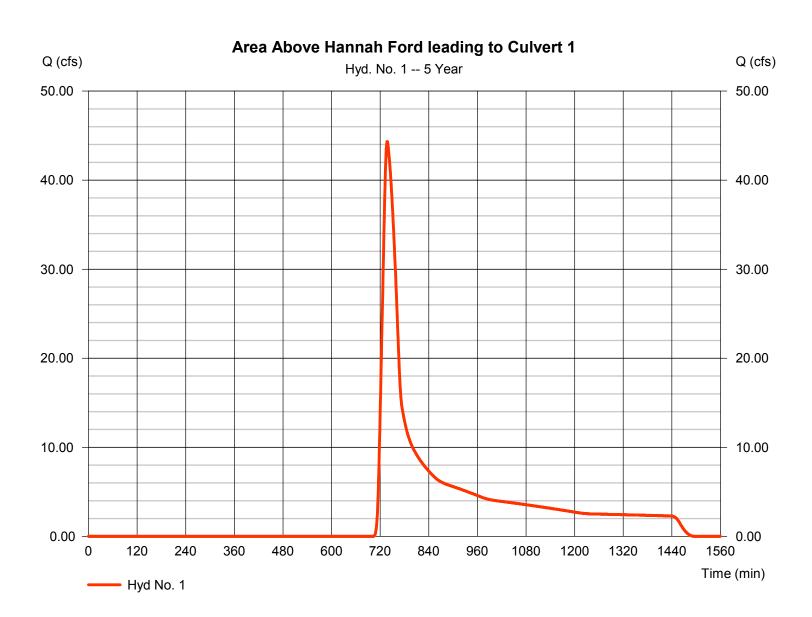
Tuesday, 03 / 28 / 2017

Hyd. No. 1

Area Above Hannah Ford leading to Culvert 1

= SCS Runoff Peak discharge = 44.33 cfsHydrograph type Storm frequency Time to peak = 737 min = 5 yrsTime interval = 1 min Hyd. volume = 273.458 cuft Curve number Drainage area = 100.000 ac= 56* Basin Slope = 0.0 %Hydraulic length = 0 ftTime of conc. (Tc) = 34.70 min Tc method = TR55 Total precip. Distribution = Type II = 4.41 inShape factor Storm duration = 484 = 24 hrs

^{*} Composite (Area/CN) = [(17.000 x 36) + (83.000 x 60)] / 100.000



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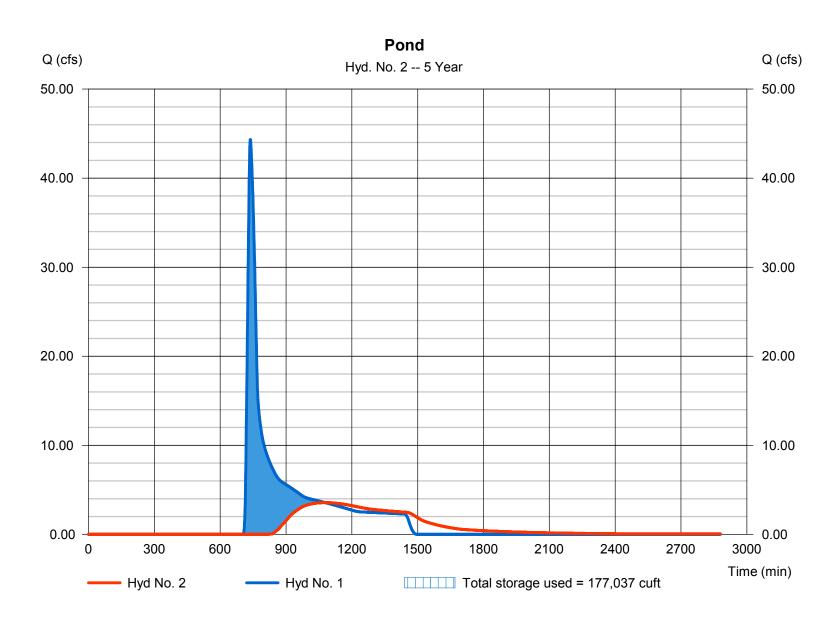
Tuesday, 03 / 28 / 2017

Hyd. No. 2

Pond

Hydrograph type Peak discharge = 3.563 cfs= Reservoir Storm frequency = 5 yrsTime to peak = 1078 min Time interval = 1 min Hyd. volume = 132.237 cuft = 1 - Area Above Hannah Ford levading tevatibrert 1 Inflow hyd. No. = 38.89 ftMax. Storage = Pond Paired with Diversion Reservoir name = 177,037 cuft

Storage Indication method used.



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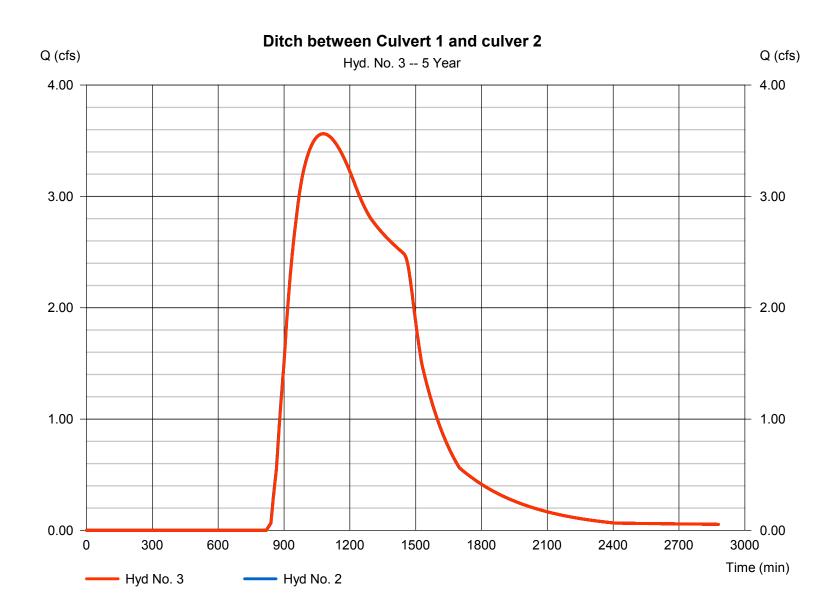
Tuesday, 03 / 28 / 2017

Hyd. No. 3

Ditch between Culvert 1 and culver 2

Hydrograph type	= Reach	Peak discharge	= 3.563 cfs
Storm frequency	= 5 yrs	Time to peak	= 1079 min
Time interval	= 1 min	Hyd. volume	= 132,234 cuft
Inflow hyd. No.	= 2 - Pond	Section type	Trapezoidal
Reach length	= 118.0 ft	Channel slope	= 1.8 %
Manning's n	= 0.030	Bottom width	= 3.0 ft
Side slope	= 3.0:1	Max. depth	= 5.0 ft
Rating curve x	= 3.202	Rating curve m	= 1.279
Ave. velocity	= 0.00 ft/s	Routing coeff.	= 1.0319

Modified Att-Kin routing method used.



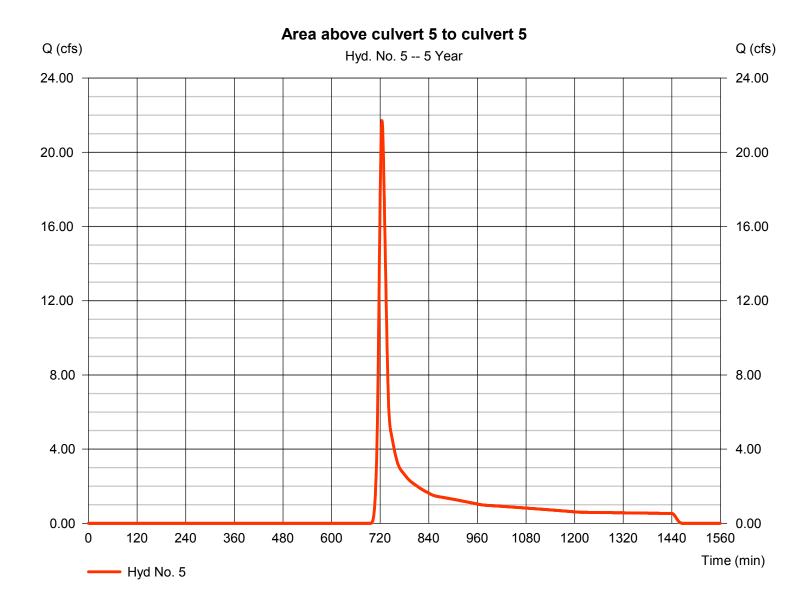
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Tuesday, 03 / 28 / 2017

Hyd. No. 5

Area above culvert 5 to culvert 5

Hydrograph type = SCS Runoff Peak discharge = 21.71 cfsStorm frequency = 5 yrsTime to peak = 724 min = 71,414 cuft Time interval = 1 min Hyd. volume Drainage area Curve number = 20.000 ac= 60 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 16.77 min = TR55 Total precip. = 4.41 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



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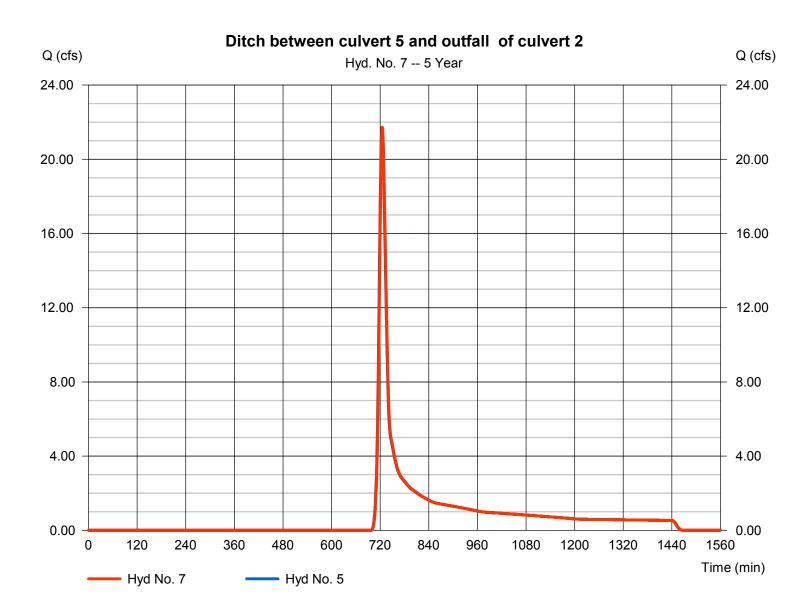
Tuesday, 03 / 28 / 2017

Hyd. No. 7

Ditch between culvert 5 and outfall of culvert 2

= Reach Peak discharge = 21.72 cfsHydrograph type Storm frequency Time to peak = 725 min = 5 yrsTime interval = 1 min Hyd. volume = 71.413 cuft Inflow hyd. No. = 5 - Area above culvert 5 to c = Trapezoidal Reach length Channel slope = 3.8 % = 174.0 ftBottom width = 3.0 ftManning's n = 0.040Side slope Max. depth = 2.0:1= 2.0 ftRating curve x Rating curve m = 1.249= 3.490Ave. velocity Routing coeff. = 0.00 ft/s= 1.0398

Modified Att-Kin routing method used.



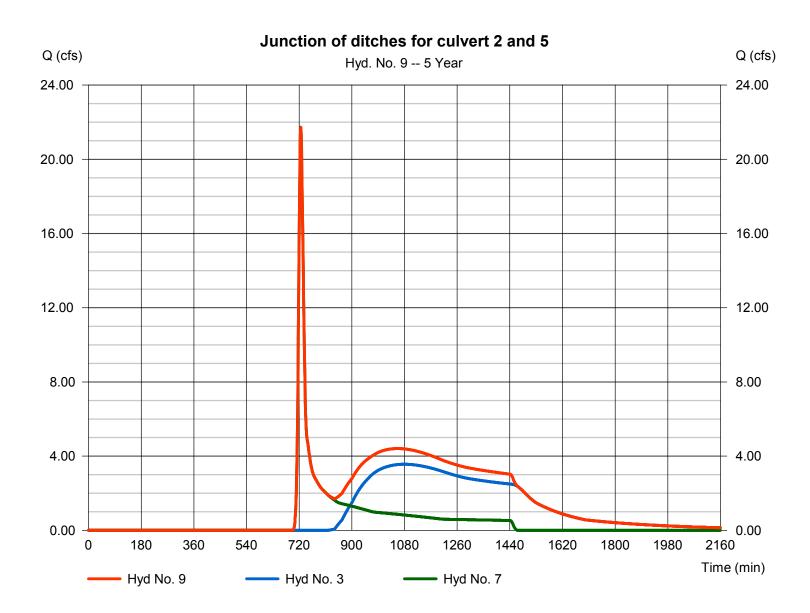
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Hyd. No. 9

Junction of ditches for culvert 2 and 5

Hydrograph type = Combine Peak discharge = 21.72 cfsStorm frequency Time to peak = 5 yrs= 725 min Time interval = 1 min Hyd. volume = 203,647 cuft Inflow hyds. = 3, 7 Contrib. drain. area = 0.000 ac



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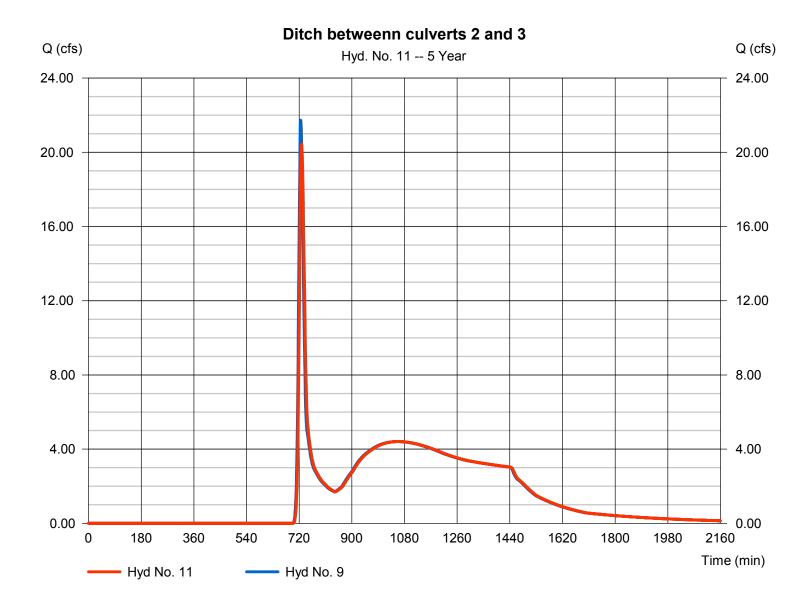
Tuesday, 03 / 28 / 2017

Hyd. No. 11

Ditch betweenn culverts 2 and 3

= Reach Peak discharge = 20.44 cfsHydrograph type Storm frequency = 5 yrsTime to peak = 729 min Time interval = 1 min Hyd. volume = 203.636 cuft = 9 - Junction of ditches for culveste2tamdtspe Inflow hyd. No. = Trapezoidal Reach length Channel slope = 2.3 % = 815.0 ftBottom width = 5.0 ftManning's n = 0.040Side slope Max. depth = 3.0:1= 5.0 ftRating curve x Rating curve m = 1.341= 1.931Ave. velocity Routing coeff. = 0.2999= 0.00 ft/s

Modified Att-Kin routing method used.



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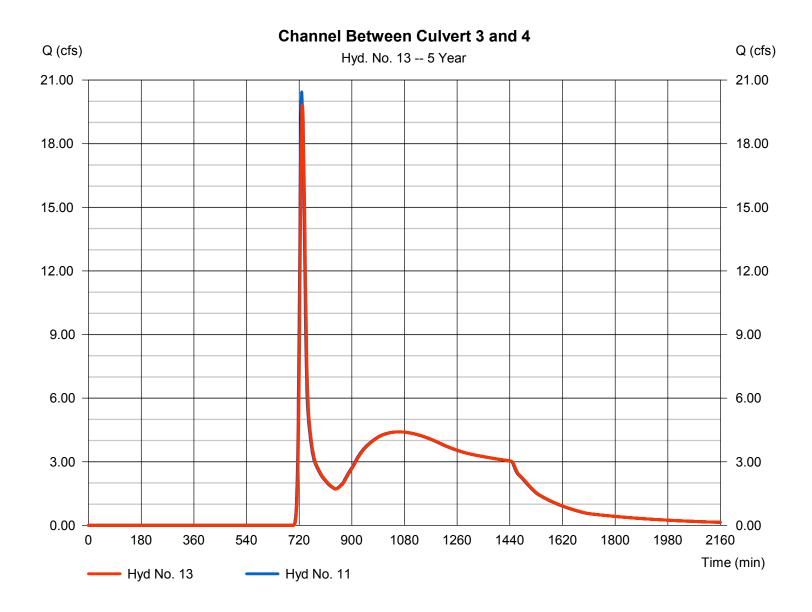
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Hyd. No. 13

Channel Between Culvert 3 and 4

Hydrograph type Peak discharge = 19.82 cfs= Reach Storm frequency = 5 yrsTime to peak = 731 min Time interval = 1 min Hyd. volume = 203.628 cuft Inflow hyd. No. = 11 - Ditch betweenn culverts 2 Spection type = Trapezoidal Channel slope = 1.2 % Reach length = 450.0 ftBottom width = 5.0 ftManning's n = 0.040Side slope Max. depth = 3.0 ft= 3.0:1Rating curve x Rating curve m = 1.395= 1.321Ave. velocity Routing coeff. = 0.3816= 0.00 ft/s

Modified Att-Kin routing method used.



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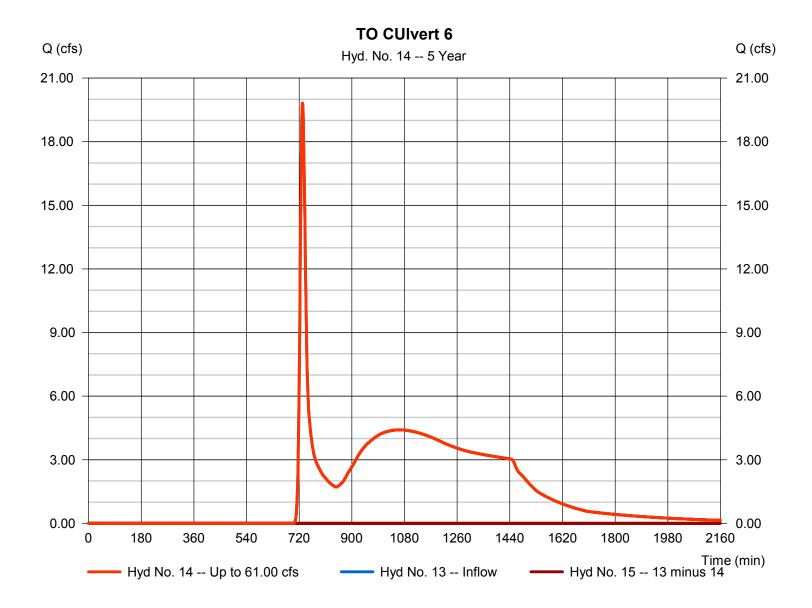
Hyd. No. 14

TO CUIvert 6

Hydrograph type= Diversion1Peak discharge= 19.82 cfsStorm frequency= 5 yrsTime to peak= 731 minTime interval= 1 minHyd. volume= 203,628 cuft

Inflow hydrograph = 13 - Channel Between Culvert 2nathdliverted hyd. = 15

Diversion method = Constant Q Constant Q = 61.00 cfs



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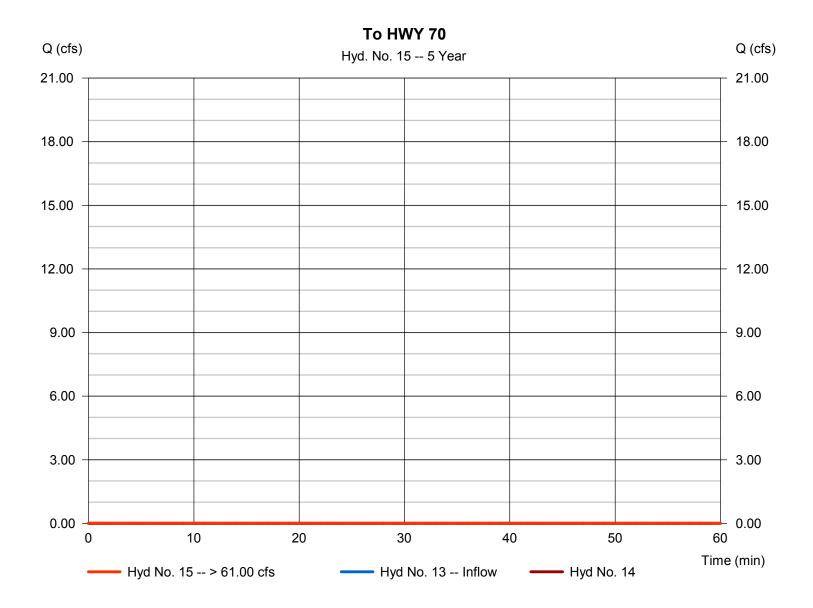
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Hyd. No. 15

To HWY 70

Hydrograph type = Diversion2 Peak discharge = 0.000 cfs
Storm frequency = 5 yrs Time to peak = n/a
Time interval = 1 min Hyd. volume = 0 cuft
Inflow hydrograph = 13 - Channel Between Culvert 2nathdisterted hyd. = 14

Diversion method = Constant Q Constant Q = 61.00 cfs



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Hyd. No. 17

Sheet flow from houses to hwy 70

Hydrograph type = SCS Runoff Peak discharge = 20.93 cfsStorm frequency = 5 yrsTime to peak = 738 min = 108,627 cuft Time interval = 1 min Hyd. volume Drainage area Curve number = 20.330 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 39.63 min = TR55 Total precip. = 4.41 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



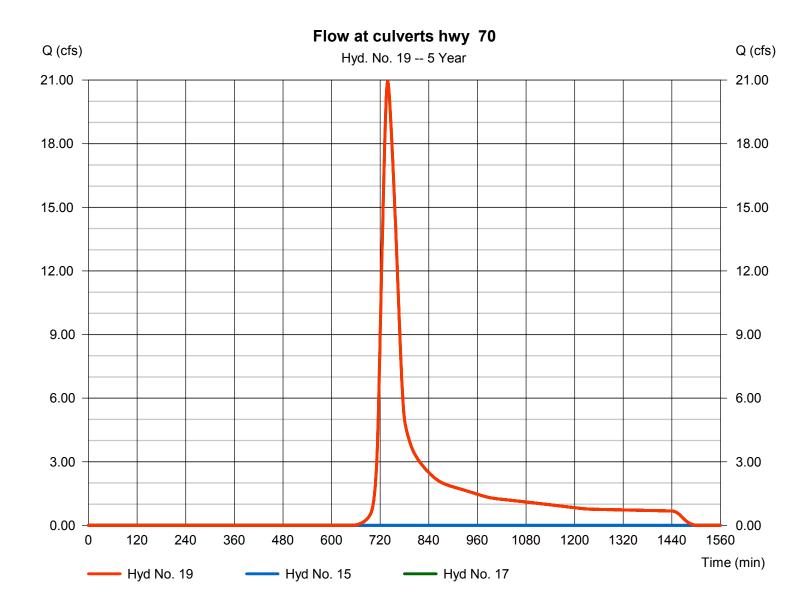
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Hyd. No. 19

Flow at culverts hwy 70

Hydrograph type = Combine Peak discharge = 20.93 cfsStorm frequency = 5 yrsTime to peak = 738 min Time interval = 1 min Hyd. volume = 108,627 cuft Inflow hyds. Contrib. drain. area = 15, 17= 20.330 ac



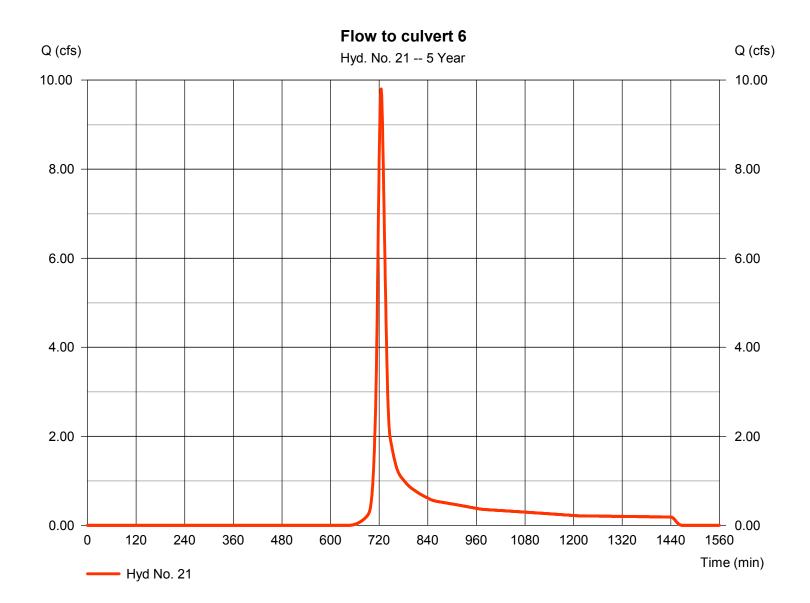
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Hyd. No. 21

Flow to culvert 6

Hydrograph type = SCS Runoff Peak discharge = 9.799 cfsStorm frequency = 5 yrsTime to peak = 725 min Time interval = 1 min Hyd. volume = 30.216 cuft Drainage area Curve number = 5.720 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 17.80 min = TR55 Total precip. = 4.41 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



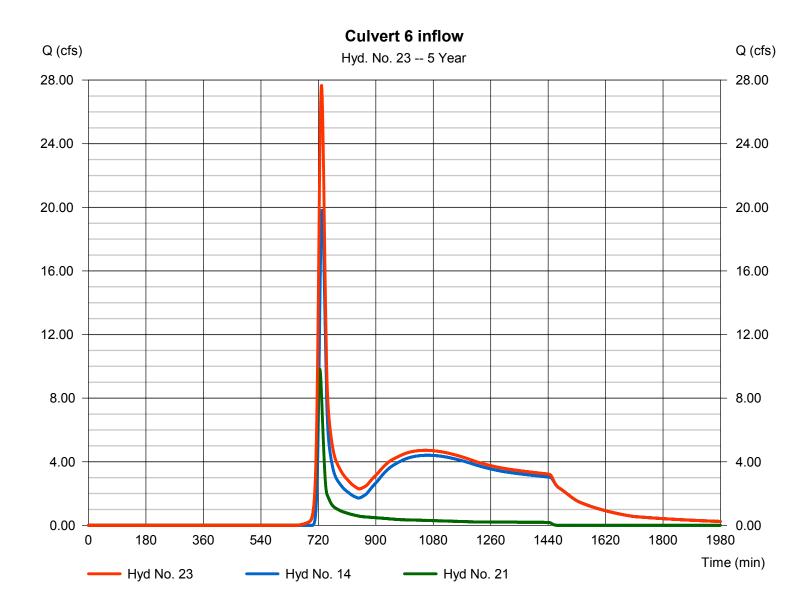
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Hyd. No. 23

Culvert 6 inflow

Hydrograph type = Combine Peak discharge = 27.66 cfsStorm frequency Time to peak = 5 yrs= 730 min Time interval = 1 min Hyd. volume = 233,843 cuft Inflow hyds. = 14, 21Contrib. drain. area = 5.720 ac



Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	69.68	1	737	385,603				Area Above Hannah Ford leading to
2	Reservoir	7.365	1	902	244,287	1	39.32	200,110	Pond
3	Reach	7.365	1	903	244,284	2			Ditch between Culvert 1 and culver 2
5	SCS Runoff	31.32	1	724	97,360				Area above culvert 5 to culvert 5
7	Reach	31.35	1	725	97,359	5			Ditch between culvert 5 and outfall of
9	Combine	31.35	1	725	341,643	3, 7,			Junction of ditches for culvert 2 and 5
11	Reach	29.78	1	728	341,633	9			Ditch betweenn culverts 2 and 3
13	Reach	28.99	1	730	341,626	11			Channel Between Culvert 3 and 4
14	Diversion1	28.99	1	730	341,626	13			TO CUIvert 6
15	Diversion2	0.000	1	n/a	0	13			To HWY 70
17	SCS Runoff	27.87	1	738	140,815				Sheet flow from houses to hwy 70
19	Combine	27.87	1	738	140,815	15, 17,			Flow at culverts hwy 70
21	SCS Runoff	12.92	1	725	39,169				Flow to culvert 6
23	Combine	39.78	1	729	380,795	14, 21,			Culvert 6 inflow
——	ersion analys	ie with 1	nond (1)	GDW/	Paturn F	Period: 10 Y	/ear	Tuesday)3 / 28 / 2017

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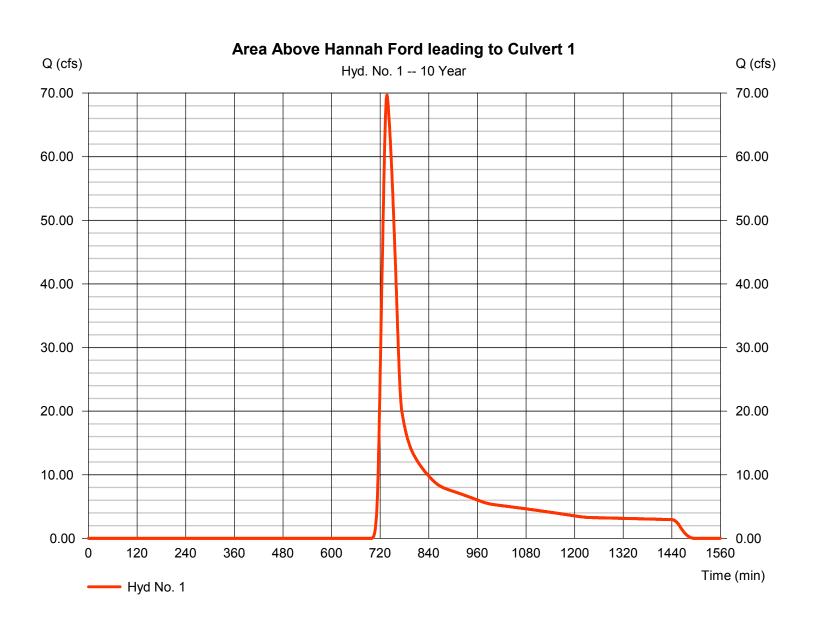
Hyd. No. 1

Area Above Hannah Ford leading to Culvert 1

= SCS Runoff Peak discharge = 69.68 cfsHydrograph type Storm frequency = 10 yrsTime to peak = 737 min Time interval = 1 min Hyd. volume = 385.603 cuft Curve number Drainage area = 100.000 ac= 56* Basin Slope = 0.0 %Hydraulic length = 0 ft

Tc method = TR55 Time of conc. (Tc) = 34.70 min
Total precip. = 5.04 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = [(17.000 x 36) + (83.000 x 60)] / 100.000



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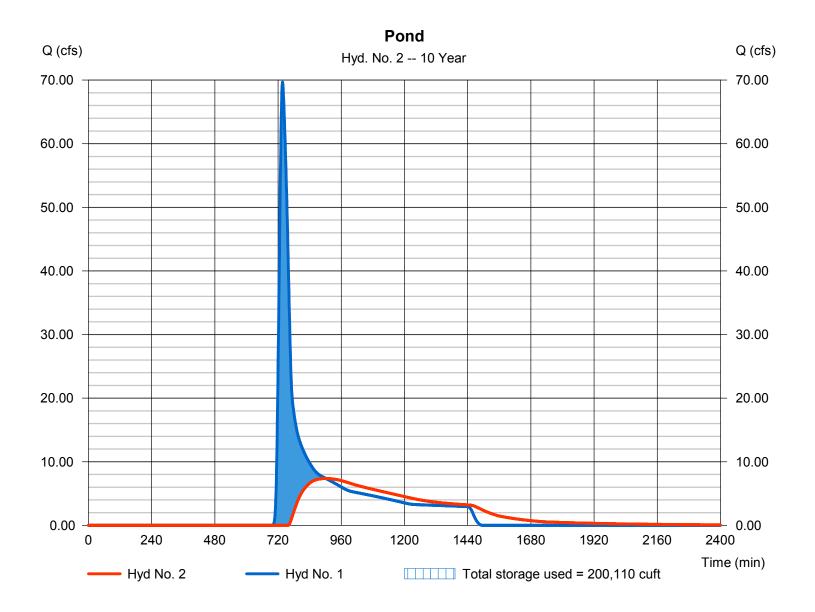
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Hyd. No. 2

Pond

Hydrograph type Peak discharge = 7.365 cfs= Reservoir Storm frequency = 10 yrsTime to peak = 902 min Time interval = 1 min Hyd. volume = 244,287 cuft Inflow hyd. No. = 1 - Area Above Hannah Ford levading tevatibrert 1 = 39.32 ftMax. Storage = Pond Paired with Diversion Reservoir name = 200,110 cuft

Storage Indication method used.



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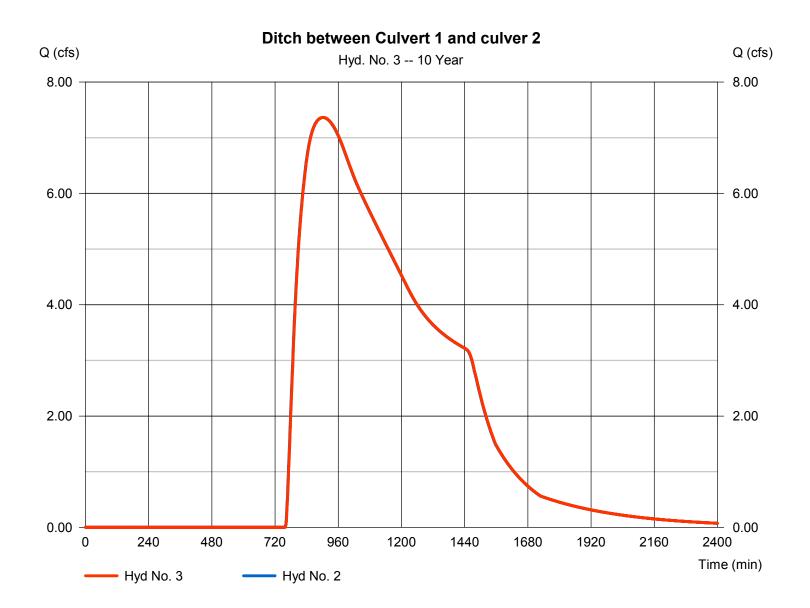
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Hyd. No. 3

Ditch between Culvert 1 and culver 2

Hydrograph type	= Reach	Peak discharge	= 7.365 cfs
Storm frequency	= 10 yrs	Time to peak	= 903 min
Time interval	= 1 min	Hyd. volume	= 244,284 cuft
Inflow hyd. No.	= 2 - Pond	Section type	Trapezoidal
Reach length	= 118.0 ft	Channel slope	= 1.8 %
Manning's n	= 0.030	Bottom width	= 3.0 ft
Side slope	= 3.0:1	Max. depth	= 5.0 ft
Rating curve x	= 3.202	Rating curve m	= 1.279
Ave. velocity	= 0.00 ft/s	Routing coeff.	= 1.1106

Modified Att-Kin routing method used.



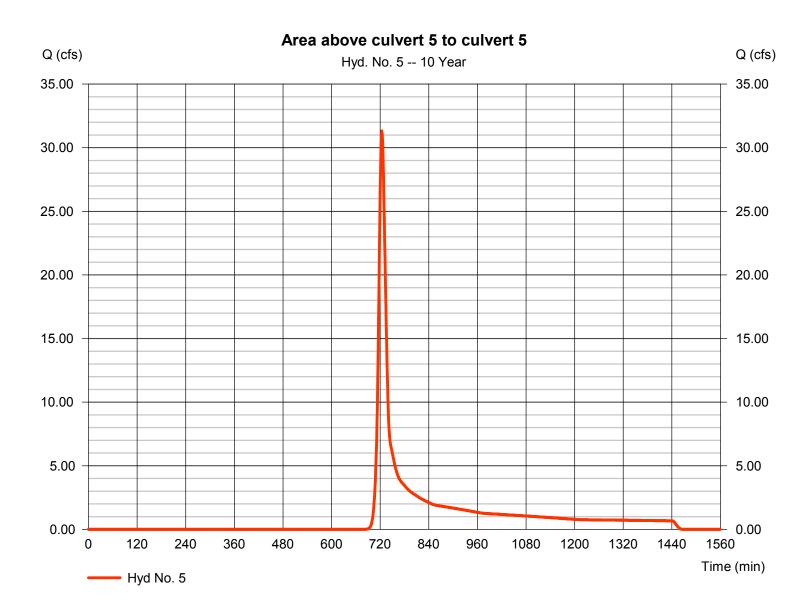
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Hyd. No. 5

Area above culvert 5 to culvert 5

Hydrograph type = SCS Runoff Peak discharge = 31.32 cfsStorm frequency = 10 yrsTime to peak = 724 min Time interval = 1 min Hyd. volume = 97,360 cuftDrainage area = 20.000 ac Curve number = 60 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 16.77 min = TR55 Total precip. = 5.04 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



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= 3.490

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= 1.249

Hyd. No. 7

Ditch between culvert 5 and outfall of culvert 2

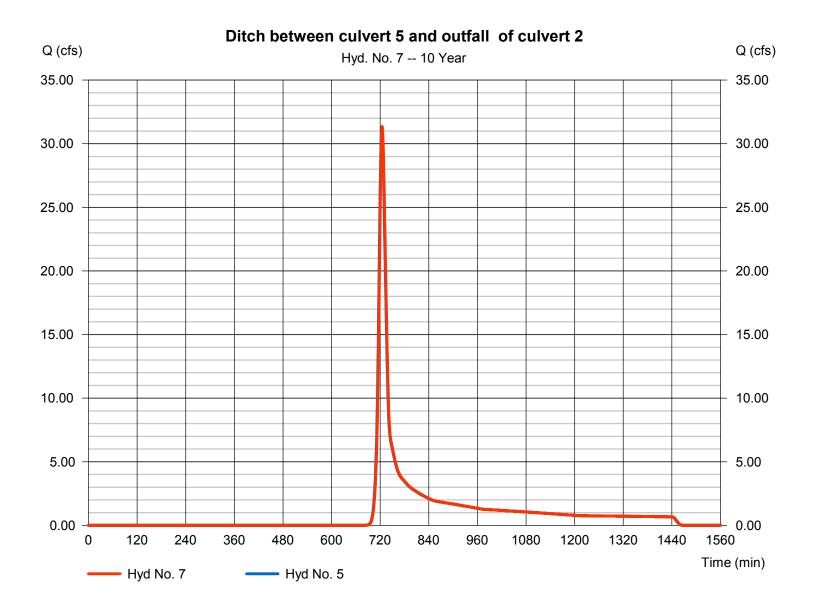
= Reach Peak discharge = 31.35 cfsHydrograph type Storm frequency = 10 yrsTime to peak = 725 min Time interval = 1 min Hyd. volume = 97.359 cuft Inflow hyd. No. = 5 - Area above culvert 5 to c = Trapezoidal Channel slope Reach length = 174.0 ft= 3.8 % Bottom width = 3.0 ftManning's n = 0.040Side slope Max. depth = 2.0 ft= 2.0:1

Ave. velocity = 0.00 ft/s Routing coeff. = 1.0762

Rating curve m

Modified Att-Kin routing method used.

Rating curve x



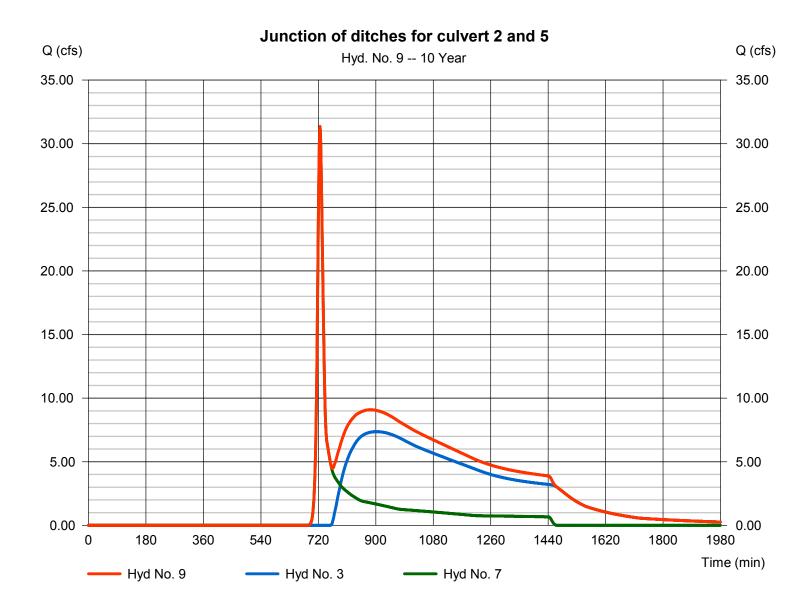
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Hyd. No. 9

Junction of ditches for culvert 2 and 5

Hydrograph type = Combine Peak discharge = 31.35 cfsStorm frequency Time to peak = 10 yrs= 725 min Time interval = 1 min Hyd. volume = 341,643 cuft Inflow hyds. = 3, 7 Contrib. drain. area = 0.000 ac



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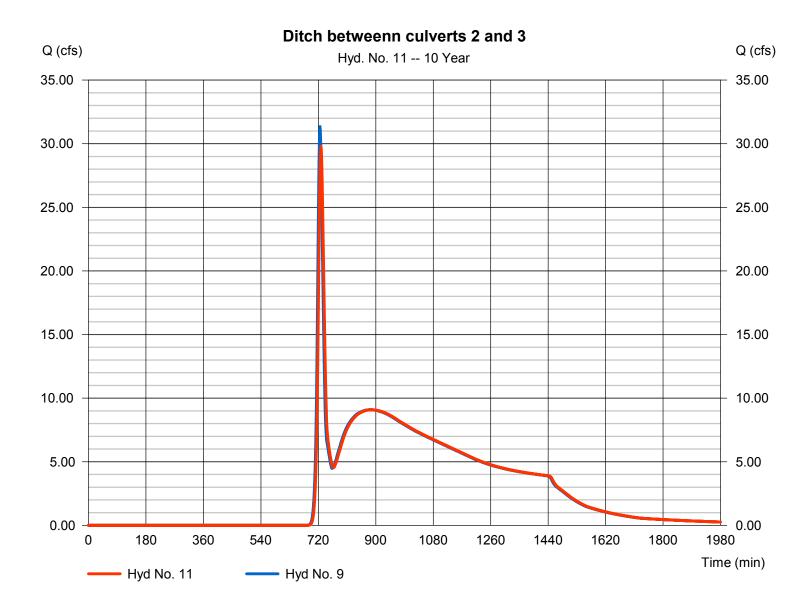
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Hyd. No. 11

Ditch betweenn culverts 2 and 3

= Reach Peak discharge = 29.78 cfsHydrograph type Storm frequency = 10 yrsTime to peak = 728 min Time interval = 1 min Hyd. volume = 341.633 cuft = 9 - Junction of ditches for culveste2tandtspe Inflow hyd. No. = Trapezoidal Reach length Channel slope = 815.0 ft= 2.3 % Bottom width = 5.0 ftManning's n = 0.040Side slope Max. depth = 3.0:1= 5.0 ftRating curve x Rating curve m = 1.341= 1.931Ave. velocity Routing coeff. = 0.3245= 0.00 ft/s

Modified Att-Kin routing method used.



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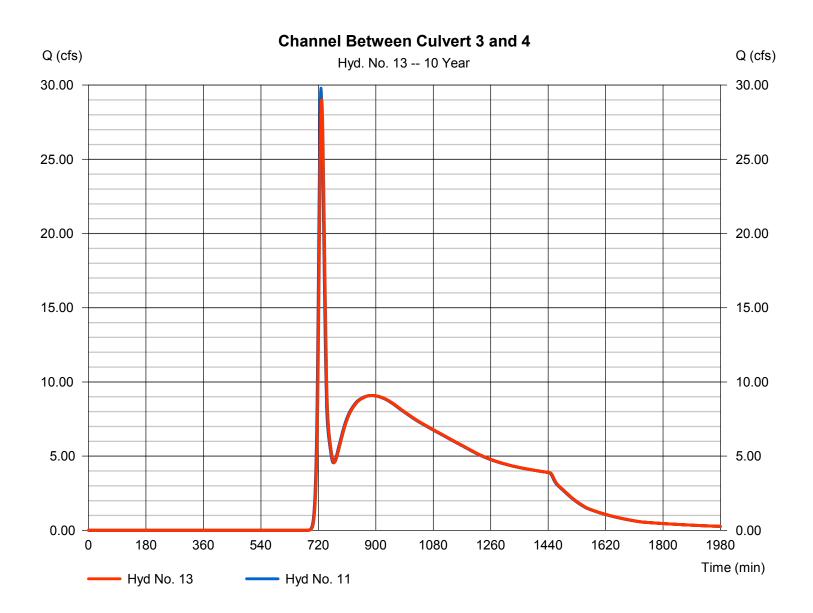
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Hyd. No. 13

Channel Between Culvert 3 and 4

Peak discharge Hydrograph type = 28.99 cfs= Reach Storm frequency = 10 yrsTime to peak = 730 min Time interval = 1 min Hyd. volume = 341,626 cuft Inflow hyd. No. = 11 - Ditch betweenn culverts 2 Spection type = Trapezoidal Reach length Channel slope = 1.2 % = 450.0 ftBottom width = 5.0 ftManning's n = 0.040Side slope Max. depth = 3.0:1= 3.0 ftRating curve x Rating curve m = 1.395= 1.321Ave. velocity Routing coeff. = 0.4106= 0.00 ft/s

Modified Att-Kin routing method used.



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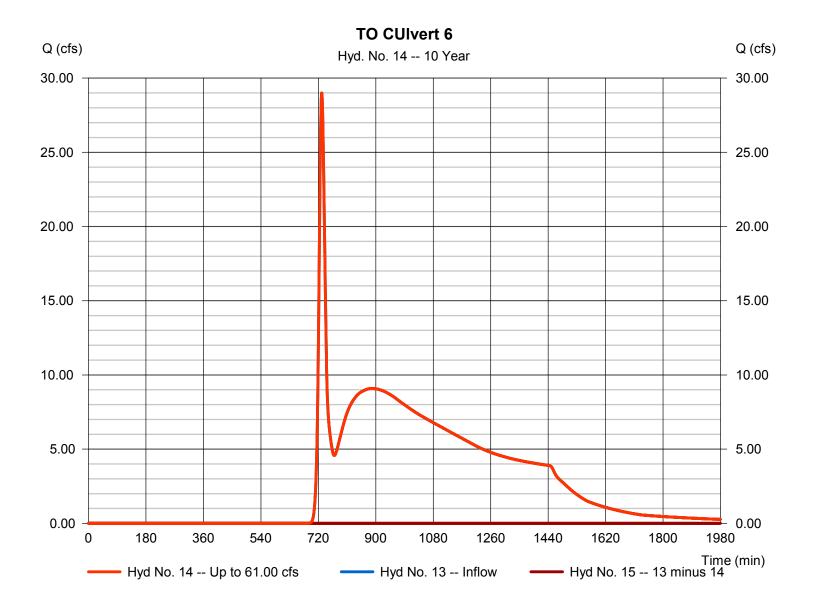
Hyd. No. 14

TO CUIvert 6

Hydrograph type= Diversion1Peak discharge= 28.99 cfsStorm frequency= 10 yrsTime to peak= 730 minTime interval= 1 minHyd. volume= 341,626 cuft

Inflow hydrograph = 13 - Channel Between Culvert 2nathdliverted hyd. = 15

Diversion method = Constant Q Constant Q = 61.00 cfs



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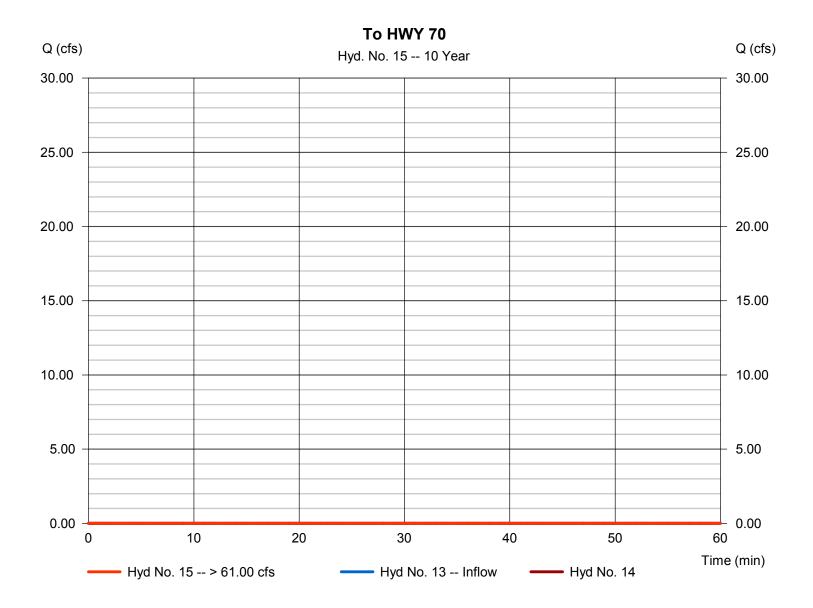
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Hyd. No. 15

To HWY 70

Hydrograph type = Diversion2 Peak discharge = 0.000 cfs
Storm frequency = 10 yrs Time to peak = n/a
Time interval = 1 min Hyd. volume = 0 cuft
Inflow hydrograph = 13 - Channel Between Culvert 2nathdiverted hyd. = 14

Diversion method = Constant Q Constant Q = 61.00 cfs



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Hyd. No. 17

Sheet flow from houses to hwy 70

Hydrograph type = SCS Runoff Peak discharge = 27.87 cfsStorm frequency = 10 yrsTime to peak = 738 min Time interval = 1 min Hyd. volume = 140,815 cuft Curve number Drainage area = 20.330 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 39.63 min = TR55 Total precip. = 5.04 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



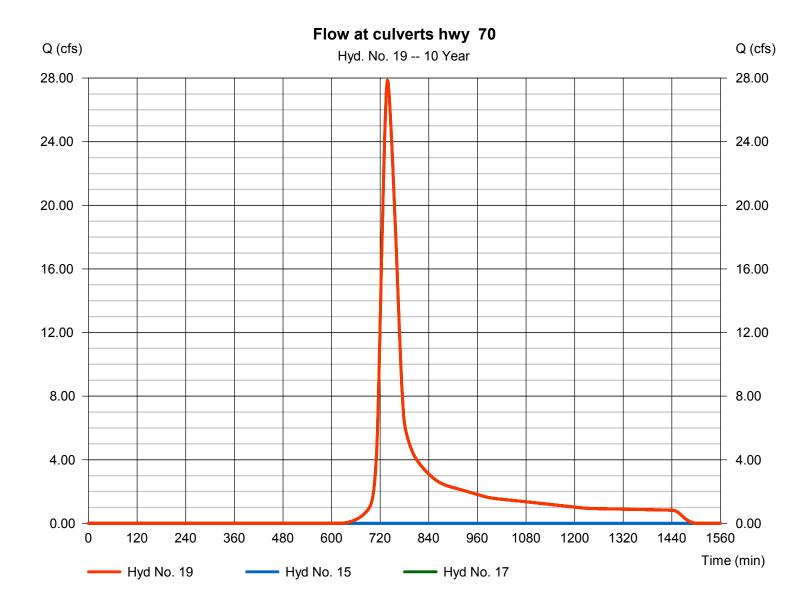
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Hyd. No. 19

Flow at culverts hwy 70

Hydrograph type = Combine Peak discharge = 27.87 cfsStorm frequency = 10 yrsTime to peak = 738 min Time interval = 1 min Hyd. volume = 140,815 cuft Inflow hyds. Contrib. drain. area = 15, 17 = 20.330 ac



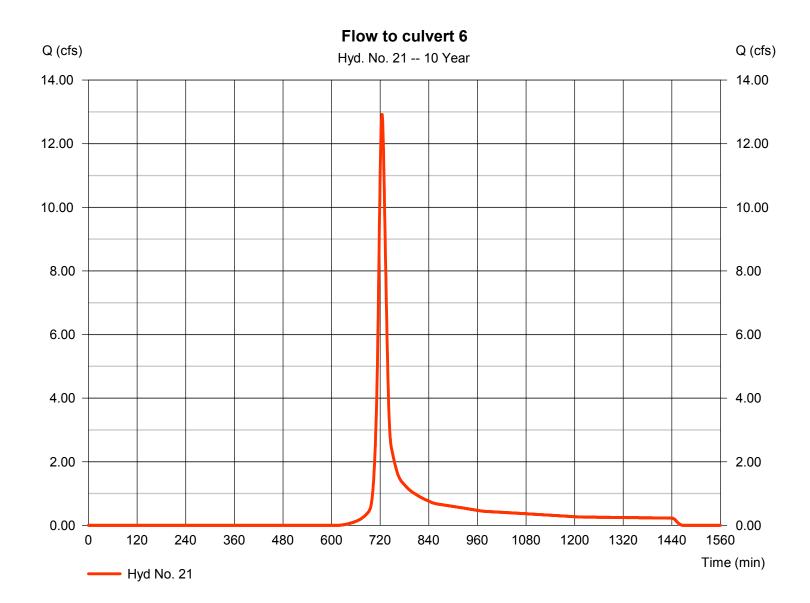
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Hyd. No. 21

Flow to culvert 6

Hydrograph type = SCS Runoff Peak discharge = 12.92 cfsStorm frequency = 10 yrsTime to peak = 725 min Time interval = 1 min Hyd. volume = 39,169 cuft Drainage area Curve number = 5.720 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 17.80 min = TR55 Total precip. = 5.04 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



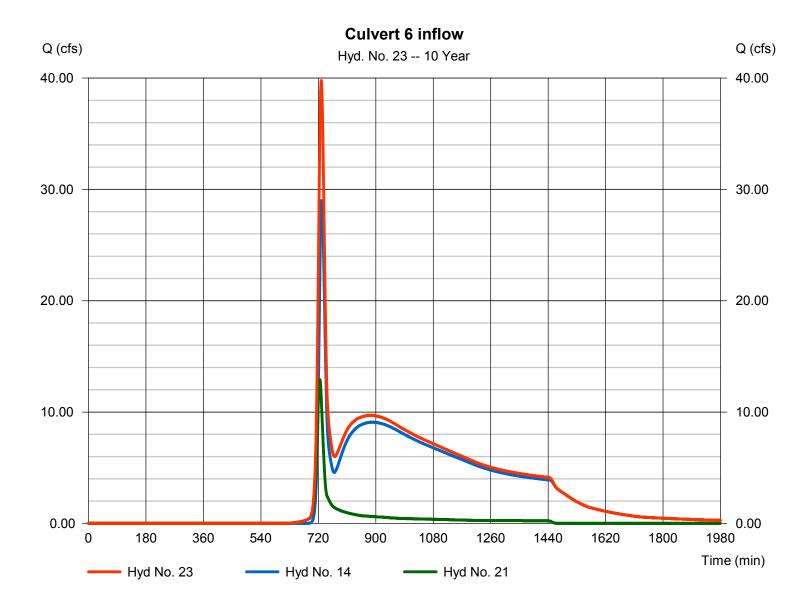
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Hyd. No. 23

Culvert 6 inflow

Hydrograph type = Combine Peak discharge = 39.78 cfsStorm frequency Time to peak = 10 yrs= 729 min Time interval = 1 min Hyd. volume = 380,795 cuft Inflow hyds. = 14, 21 Contrib. drain. area = 5.720 ac



Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

łyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	112.65	1	736	568,777				Area Above Hannah Ford leading to
2	Reservoir	16.34	1	816	427,361	1	40.32	257,068	Pond
3	Reach	16.34	1	817	427,358	2			Ditch between Culvert 1 and culver 2
5	SCS Runoff	46.54	1	724	138,852				Area above culvert 5 to culvert 5
7	Reach	46.56	1	725	138,852	5			Ditch between culvert 5 and outfall of
9	Combine	46.56	1	725	566,209	3, 7,			Junction of ditches for culvert 2 and 5
11	Reach	44.65	1	727	566,200	9			Ditch betweenn culverts 2 and 3
13	Reach	43.75	1	730	566,192	11			Channel Between Culvert 3 and 4
14	Diversion1	43.75	1	730	566,192	13			TO CUlvert 6
15	Diversion2	0.000	1	n/a	0	13			To HWY 70
17	SCS Runoff	38.53	1	738	190,584				Sheet flow from houses to hwy 70
19	Combine	38.53	1	738	190,584	15, 17,			Flow at culverts hwy 70
21	SCS Runoff	17.74	1	724	53,013				Flow to culvert 6
23	Combine	58.95	1	728	619,204	14, 21,			Culvert 6 inflow
	ersion analys	is with 1 p	oond (1).	gpw	Return F	Period: 25 \	⊥ ∕ear	Tuesday, (03 / 28 / 2017

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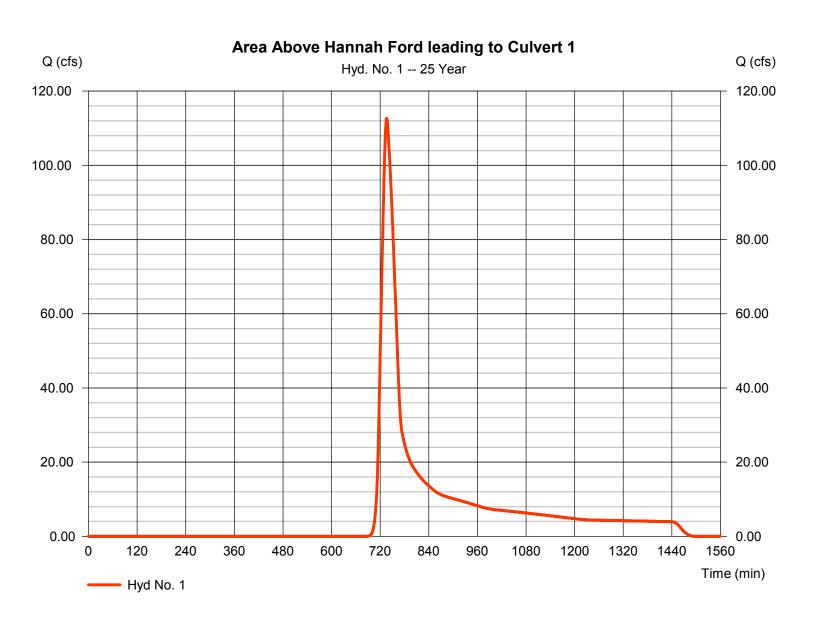
Tuesday, 03 / 28 / 2017

Hyd. No. 1

Area Above Hannah Ford leading to Culvert 1

= SCS Runoff Peak discharge = 112.65 cfsHydrograph type Storm frequency = 25 yrsTime to peak = 736 min Time interval = 1 min Hyd. volume = 568,777 cuft Curve number Drainage area = 100.000 ac= 56* Basin Slope = 0.0 %Hydraulic length = 0 ftTime of conc. (Tc) Tc method = TR55 $= 34.70 \, \text{min}$ Total precip. Distribution = Type II = 5.95 inStorm duration Shape factor = 484 = 24 hrs

^{*} Composite (Area/CN) = [(17.000 x 36) + (83.000 x 60)] / 100.000



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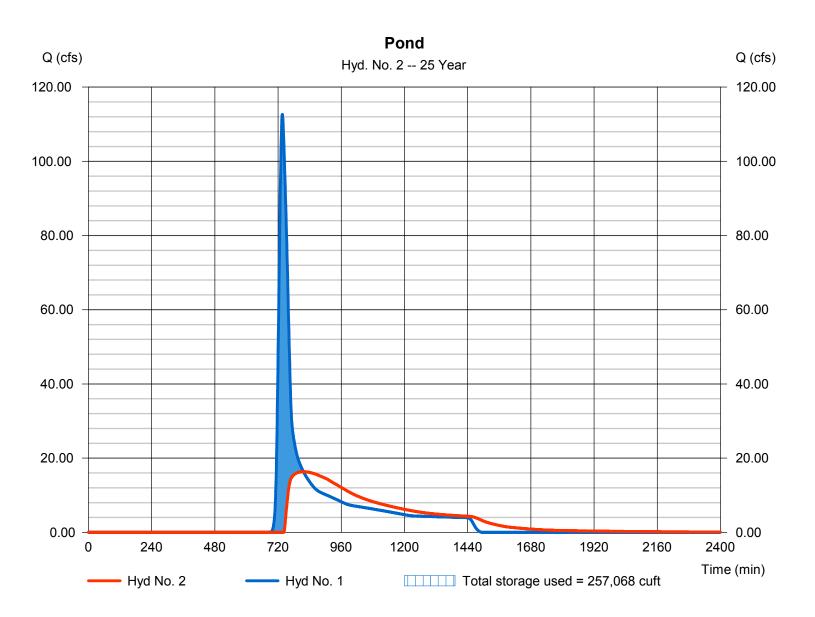
Tuesday, 03 / 28 / 2017

Hyd. No. 2

Pond

Hydrograph type Peak discharge = 16.34 cfs= Reservoir Storm frequency = 25 yrsTime to peak = 816 min Time interval = 1 min Hyd. volume = 427,361 cuft = 1 - Area Above Hannah Ford levading tevatibrert 1 Inflow hyd. No. = 40.32 ftMax. Storage = Pond Paired with Diversion Reservoir name = 257,068 cuft

Storage Indication method used.



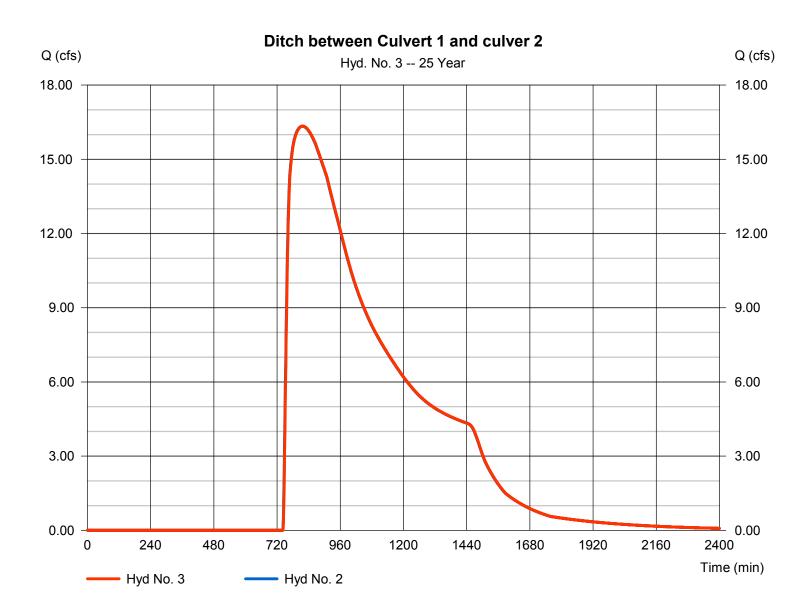
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Tuesday, 03 / 28 / 2017

Hyd. No. 3

Ditch between Culvert 1 and culver 2

Hydrograph type Storm frequency Time interval Inflow hyd. No. Reach length Manning's n Side slope	= Reach = 25 yrs = 1 min = 2 - Pond = 118.0 ft = 0.030 = 3.0:1	Peak discharge Time to peak Hyd. volume Section type Channel slope Bottom width Max. depth	= 16.34 cfs = 817 min = 427,358 cuft = Trapezoidal = 1.8 % = 3.0 ft = 5.0 ft
Side slope Rating curve x Ave. velocity	= 3.0:1 = 3.202 = 0.00 ft/s	Max. depth Rating curve m Routing coeff.	= 5.0 ft = 1.279 = 1.1954



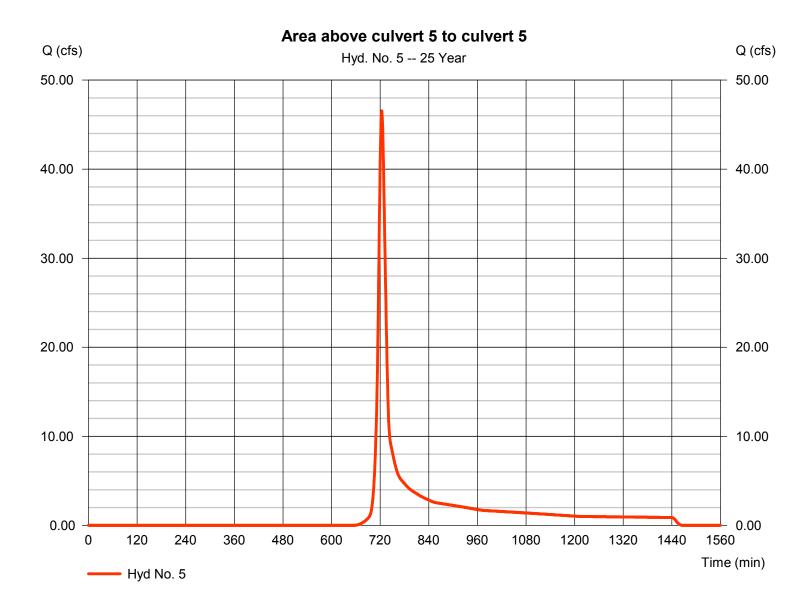
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Tuesday, 03 / 28 / 2017

Hyd. No. 5

Area above culvert 5 to culvert 5

Hydrograph type = SCS Runoff Peak discharge = 46.54 cfsStorm frequency = 25 yrs Time to peak = 724 min Time interval = 1 min Hyd. volume = 138,852 cuft Drainage area Curve number = 20.000 ac= 60 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 16.77 min = TR55 Total precip. = 5.95 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



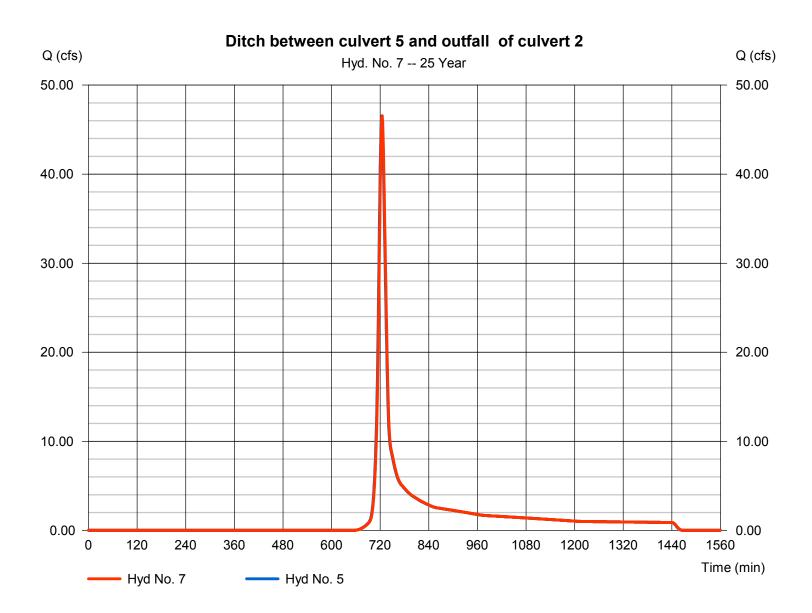
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Tuesday, 03 / 28 / 2017

Hyd. No. 7

Ditch between culvert 5 and outfall of culvert 2

= Reach Peak discharge = 46.56 cfsHydrograph type Storm frequency = 25 yrsTime to peak = 725 min Time interval = 1 min Hyd. volume = 138.852 cuft Inflow hyd. No. = 5 - Area above culvert 5 to c = Trapezoidal Reach length Channel slope = 3.8 % = 174.0 ftBottom width = 3.0 ftManning's n = 0.040Side slope Max. depth = 2.0 ft= 2.0:1Rating curve x Rating curve m = 1.249= 3.490Ave. velocity Routing coeff. = 1.1154= 0.00 ft/s



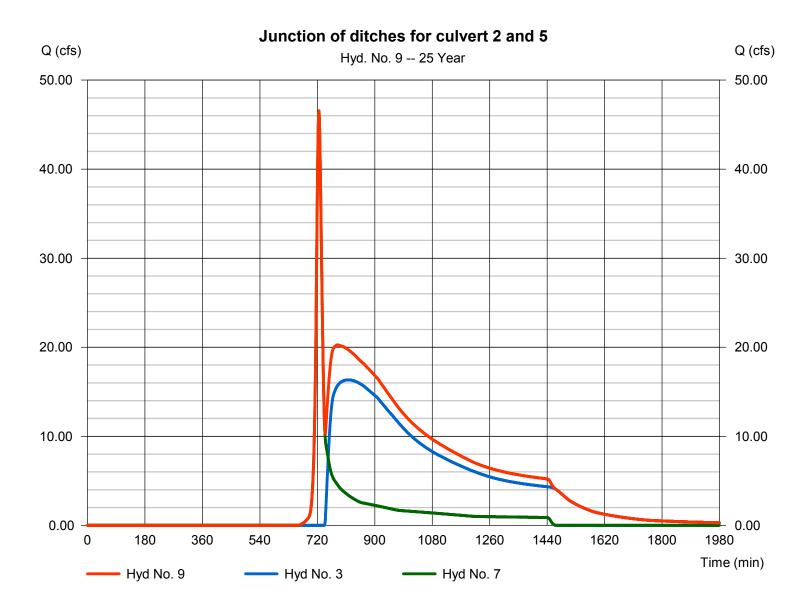
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Tuesday, 03 / 28 / 2017

Hyd. No. 9

Junction of ditches for culvert 2 and 5

Hydrograph type = Combine Peak discharge = 46.56 cfsStorm frequency Time to peak = 25 yrs= 725 min Time interval = 1 min Hyd. volume = 566,209 cuft Inflow hyds. = 3, 7 Contrib. drain. area = 0.000 ac



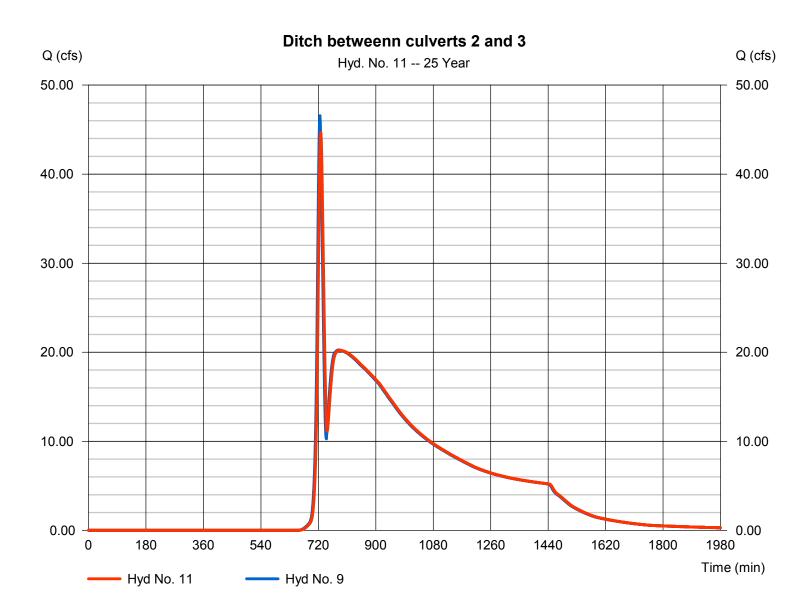
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Tuesday, 03 / 28 / 2017

Hyd. No. 11

Ditch betweenn culverts 2 and 3

Peak discharge = Reach = 44.65 cfsHydrograph type Storm frequency = 25 yrsTime to peak = 727 min Time interval = 1 min Hyd. volume = 566.200 cuft = 9 - Junction of ditches for culveste2tamdtspe Inflow hyd. No. = Trapezoidal Reach length = 815.0 ftChannel slope = 2.3 % = 5.0 ftManning's n = 0.040Bottom width Side slope Max. depth = 3.0:1= 5.0 ftRating curve x Rating curve m = 1.931= 1.341Ave. velocity Routing coeff. = 0.00 ft/s= 0.3528



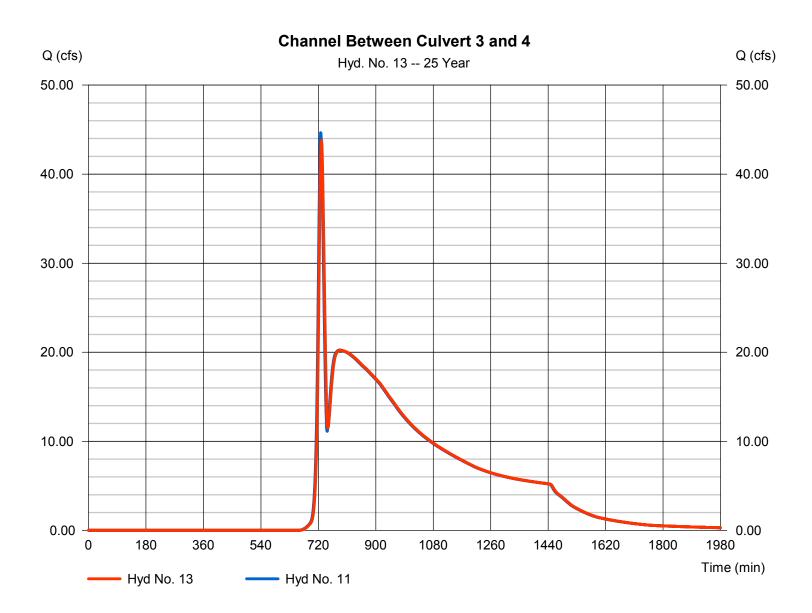
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Tuesday, 03 / 28 / 2017

Hyd. No. 13

Channel Between Culvert 3 and 4

Peak discharge = 43.75 cfsHydrograph type = Reach Storm frequency = 25 yrsTime to peak = 730 min Time interval = 1 min Hyd. volume = 566,192 cuft Inflow hyd. No. = 11 - Ditch betweenn culverts 2 Spection type = Trapezoidal Reach length Channel slope = 1.2 % = 450.0 ftBottom width = 5.0 ftManning's n = 0.040Side slope Max. depth = 3.0:1= 3.0 ftRating curve x Rating curve m = 1.395= 1.321Ave. velocity Routing coeff. = 0.4436= 0.00 ft/s



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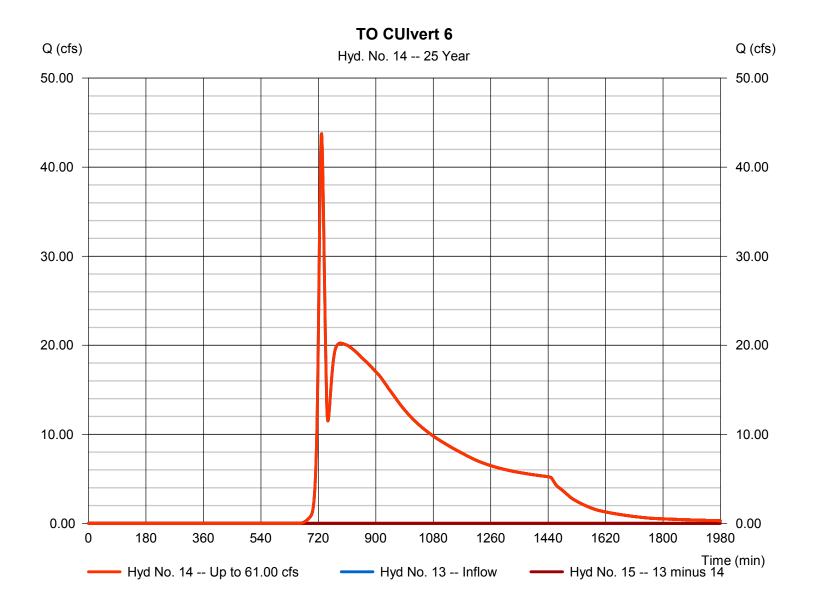
Hyd. No. 14

TO CUIvert 6

Hydrograph type= Diversion1Peak discharge= 43.75 cfsStorm frequency= 25 yrsTime to peak= 730 minTime interval= 1 minHyd. volume= 566,192 cuft

Inflow hydrograph = 13 - Channel Between Culvert 2nathdliverted hyd. = 15

Diversion method = Constant Q Constant Q = 61.00 cfs



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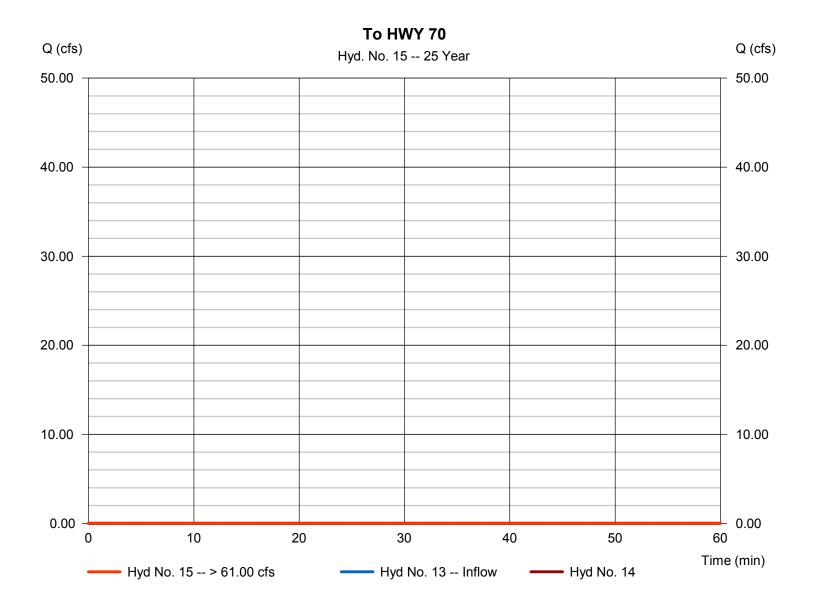
Tuesday, 03 / 28 / 2017

Hyd. No. 15

To HWY 70

Hydrograph type = Diversion2 Peak discharge = 0.000 cfs
Storm frequency = 25 yrs Time to peak = n/a
Time interval = 1 min Hyd. volume = 0 cuft
Inflow hydrograph = 13 - Channel Between Culvert 2nathdiverted hyd. = 14

Diversion method = Constant Q Constant Q = 61.00 cfs



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Hyd. No. 17

Sheet flow from houses to hwy 70

Hydrograph type = SCS Runoff Peak discharge = 38.53 cfsStorm frequency = 25 yrs Time to peak = 738 min Time interval = 1 min Hyd. volume = 190,584 cuft Drainage area Curve number = 20.330 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 39.63 min = TR55 Total precip. = 5.95 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



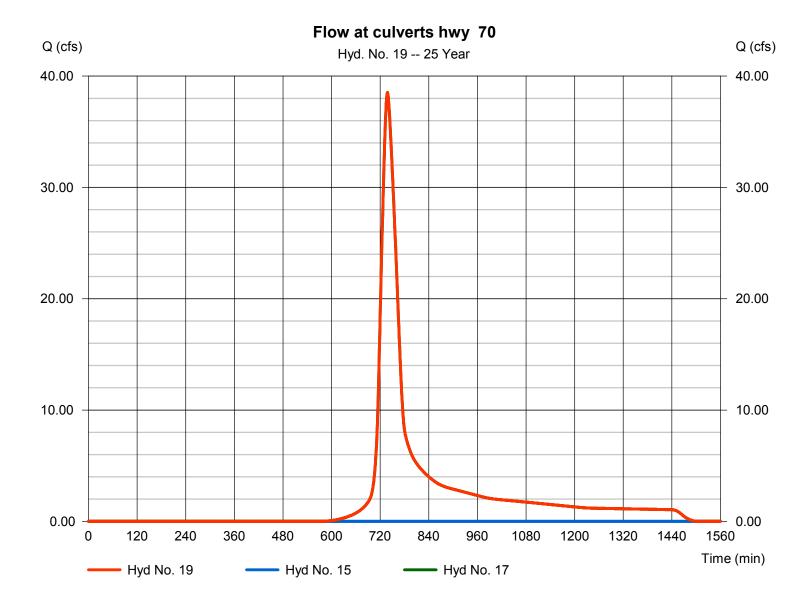
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Tuesday, 03 / 28 / 2017

Hyd. No. 19

Flow at culverts hwy 70

Hydrograph type = Combine Peak discharge = 38.53 cfsStorm frequency = 25 yrsTime to peak = 738 min Time interval = 1 min Hyd. volume = 190,584 cuft Inflow hyds. = 15, 17Contrib. drain. area = 20.330 ac



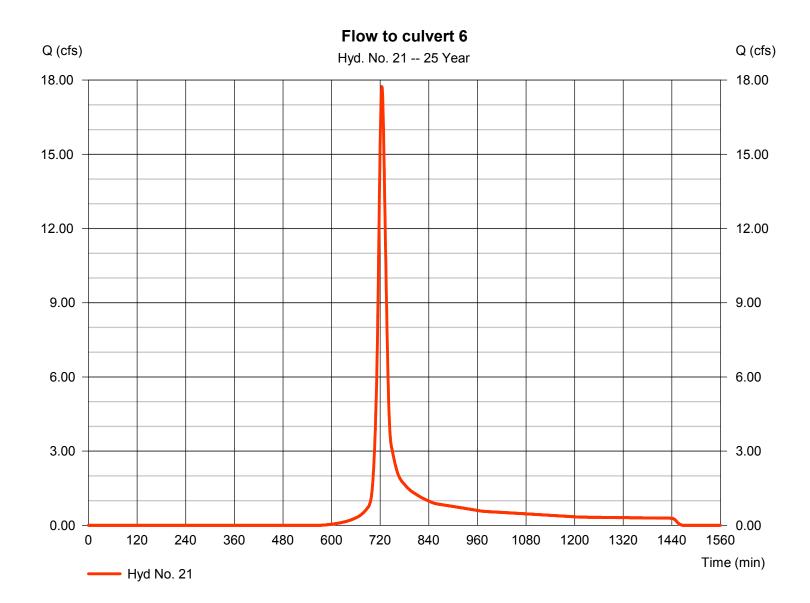
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Hyd. No. 21

Flow to culvert 6

Hydrograph type = SCS Runoff Peak discharge = 17.74 cfsStorm frequency = 25 yrs Time to peak = 724 min Time interval = 1 min Hyd. volume = 53,013 cuftDrainage area Curve number = 5.720 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 17.80 min = TR55 Total precip. = 5.95 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



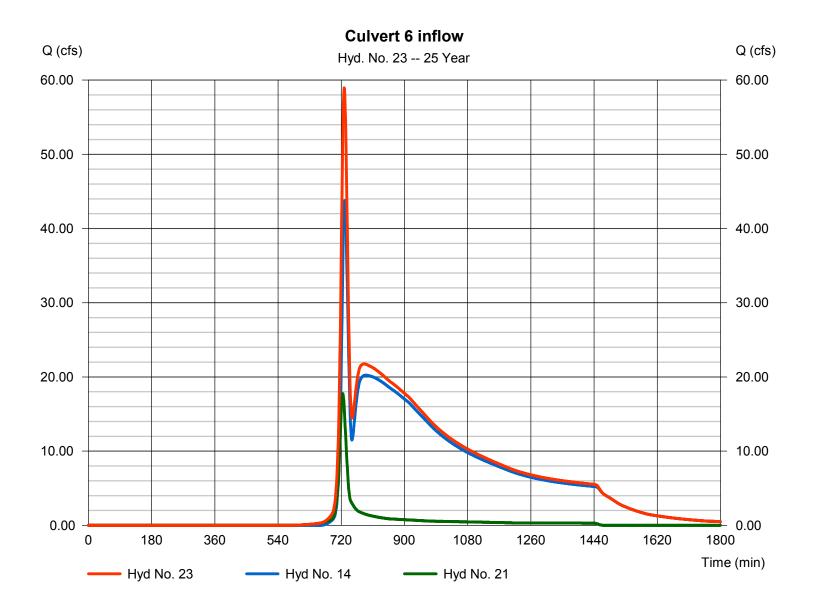
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Tuesday, 03 / 28 / 2017

Hyd. No. 23

Culvert 6 inflow

Hydrograph type = Combine Peak discharge = 58.95 cfsStorm frequency Time to peak = 25 yrs= 728 min Time interval = 1 min Hyd. volume = 619,204 cuft Inflow hyds. = 14, 21Contrib. drain. area = 5.720 ac



Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

lyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	150.27	1	736	728,353				Area Above Hannah Ford leading to
2	Reservoir	22.21	1	805	586,869	1	41.53	329,191	Pond
3	Reach	22.21	1	806	586,867	2			Ditch between Culvert 1 and culver 2
5	SCS Runoff	59.46	1	724	174,409				Area above culvert 5 to culvert 5
7	Reach	59.47	1	725	174,409	5			Ditch between culvert 5 and outfall of
9	Combine	59.47	1	725	761,276	3, 7,			Junction of ditches for culvert 2 and 5
11	Reach	57.47	1	727	761,268	9			Ditch betweenn culverts 2 and 3
13	Reach	56.42	1	729	761,260	11			Channel Between Culvert 3 and 4
14	Diversion1	56.42	1	729	761,260	13			TO CUIvert 6
15	Diversion2	0.000	1	n/a	0	13			To HWY 70
17	SCS Runoff	47.37	1	738	232,111				Sheet flow from houses to hwy 70
19	Combine	47.37	1	738	232,111	15, 17,			Flow at culverts hwy 70
21	SCS Runoff	21.73	1	724	64,564				Flow to culvert 6
23	Combine	75.35	1	728	825,823	14, 21,			Culvert 6 inflow
	ersion analys	:	(4)		Data = 5	Period: 50 Y		 	03 / 28 / 2017

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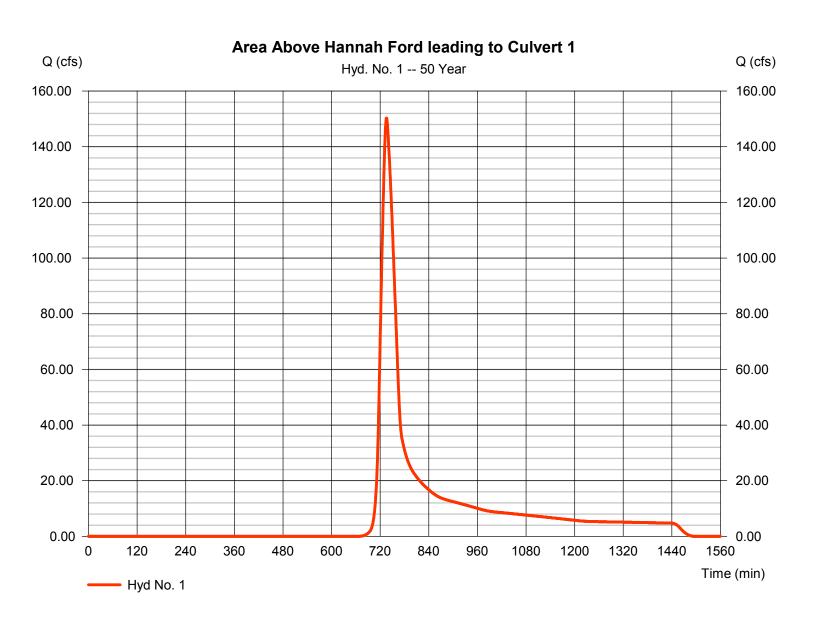
Tuesday, 03 / 28 / 2017

Hyd. No. 1

Area Above Hannah Ford leading to Culvert 1

= SCS Runoff Peak discharge = 150.27 cfsHydrograph type Storm frequency = 50 yrsTime to peak = 736 min Time interval = 1 min Hyd. volume = 728.353 cuft Curve number Drainage area = 100.000 ac= 56* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 34.70 min = TR55 Total precip. Distribution = Type II = 6.67 inStorm duration Shape factor = 484 = 24 hrs

^{*} Composite (Area/CN) = [(17.000 x 36) + (83.000 x 60)] / 100.000



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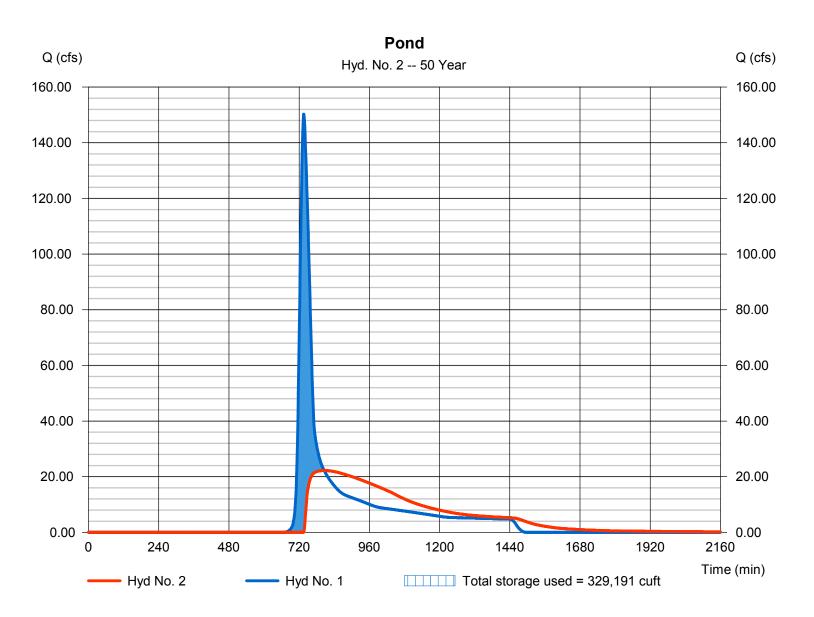
Tuesday, 03 / 28 / 2017

Hyd. No. 2

Pond

Hydrograph type Peak discharge = 22.21 cfs= Reservoir Storm frequency = 50 yrsTime to peak = 805 min Time interval = 1 min Hyd. volume = 586,869 cuft Inflow hyd. No. = 1 - Area Above Hannah Ford levading tevatibrert 1 = 41.53 ftMax. Storage = Pond Paired with Diversion Reservoir name = 329,191 cuft

Storage Indication method used.



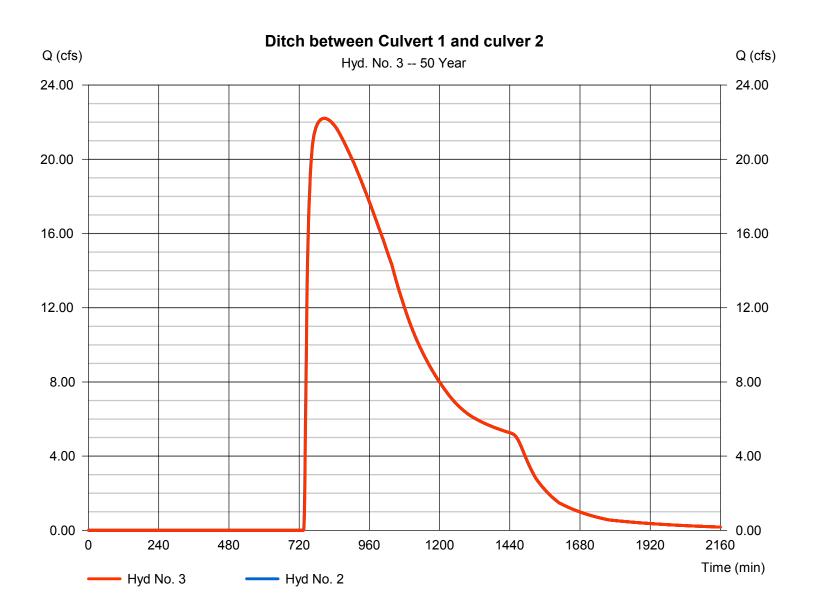
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Hyd. No. 3

Ditch between Culvert 1 and culver 2

Hydrograph type	= Reach	Peak discharge	= 22.21 cfs
Storm frequency	= 50 yrs	Time to peak	= 806 min
Time interval	= 1 min	Hyd. volume	= 586,867 cuft
Inflow hyd. No.	= 2 - Pond	Section type	Trapezoidal
Reach length	= 118.0 ft	Channel slope	= 1.8 %
Manning's n	= 0.030	Bottom width	= 3.0 ft
Side slope	= 3.0:1	Max. depth	= 5.0 ft
Rating curve x	= 3.202	Rating curve m	= 1.279
Ave. velocity	= 0.00 ft/s	Routing coeff.	= 1.2274



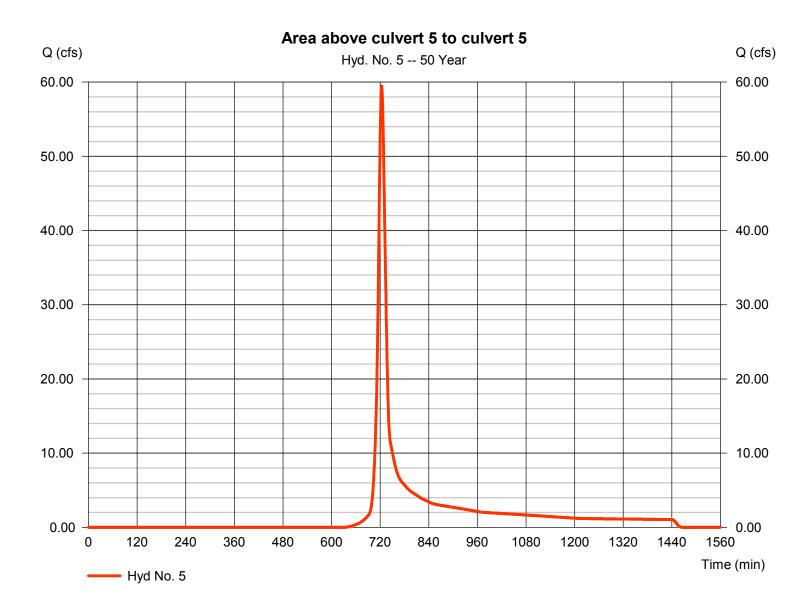
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Hyd. No. 5

Area above culvert 5 to culvert 5

Hydrograph type = SCS Runoff Peak discharge = 59.46 cfsStorm frequency = 50 yrsTime to peak = 724 min Time interval = 1 min Hyd. volume = 174,409 cuftDrainage area Curve number = 20.000 ac= 60 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 16.77 min = TR55 Total precip. = 6.67 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



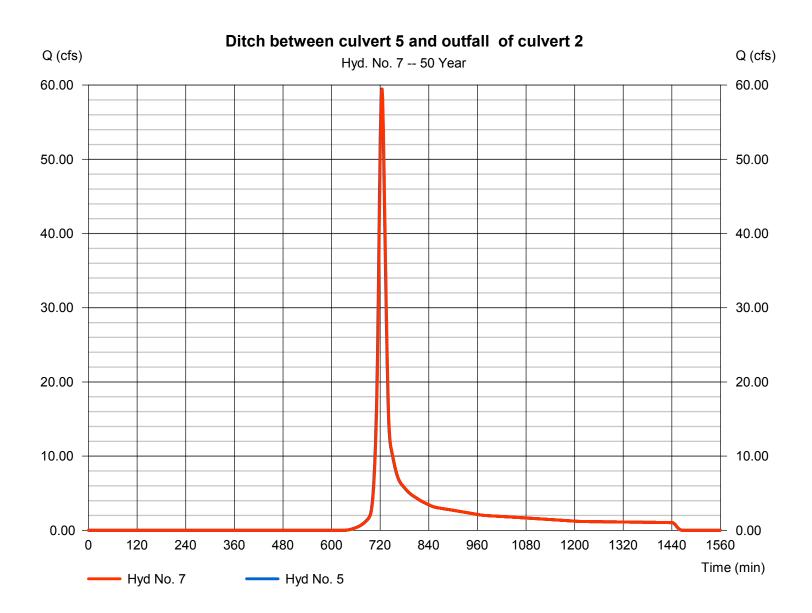
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Hyd. No. 7

Ditch between culvert 5 and outfall of culvert 2

= Reach Peak discharge = 59.47 cfsHydrograph type Storm frequency = 50 yrsTime to peak = 725 min Time interval = 1 min Hyd. volume = 174.409 cuft Inflow hyd. No. = 5 - Area above culvert 5 to c = Trapezoidal Reach length = 174.0 ftChannel slope = 3.8 % Bottom width = 3.0 ftManning's n = 0.040Side slope Max. depth = 2.0 ft= 2.0:1Rating curve x Rating curve m = 1.249= 3.490Ave. velocity Routing coeff. = 0.00 ft/s= 1.1395



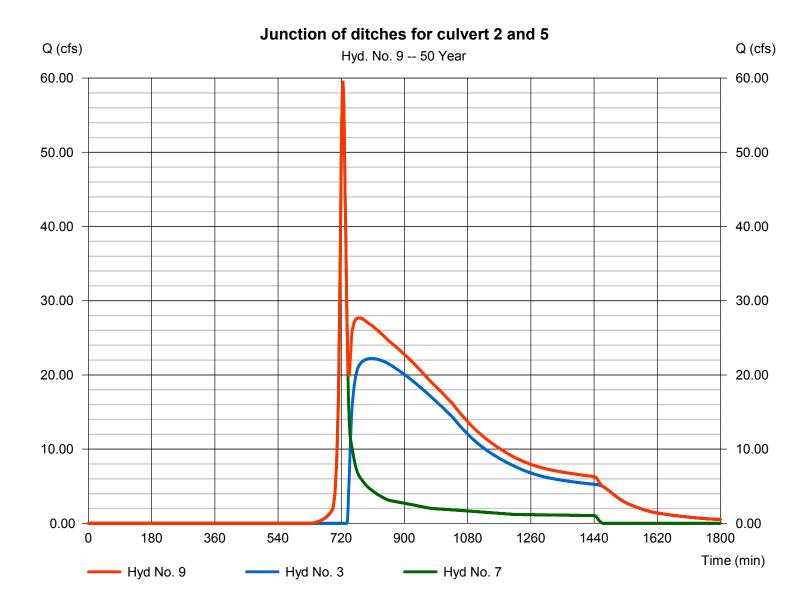
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Hyd. No. 9

Junction of ditches for culvert 2 and 5

Hydrograph type = Combine Peak discharge = 59.47 cfsStorm frequency Time to peak = 50 yrs= 725 min Time interval = 1 min Hyd. volume = 761,276 cuft Inflow hyds. = 3, 7 Contrib. drain. area = 0.000 ac



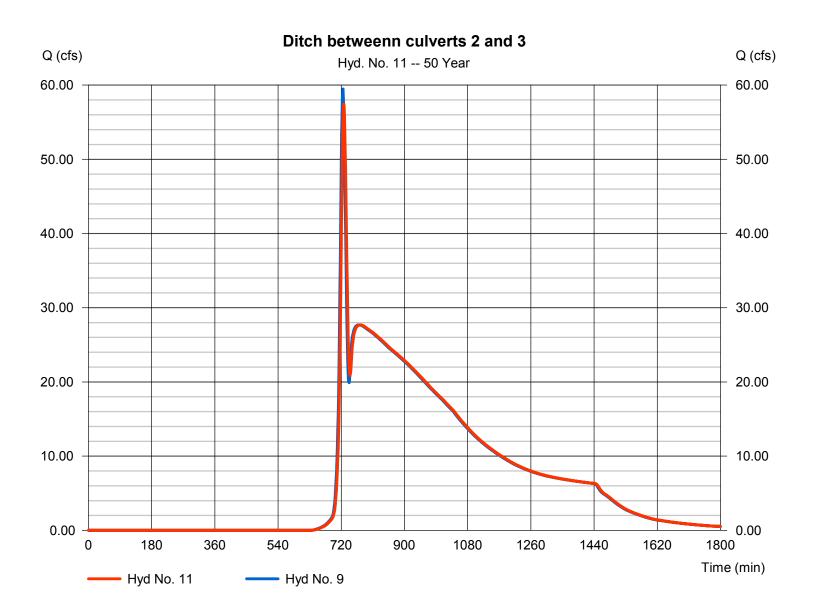
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Hyd. No. 11

Ditch betweenn culverts 2 and 3

Peak discharge = Reach = 57.47 cfsHydrograph type Storm frequency = 50 yrsTime to peak = 727 min Time interval = 1 min Hyd. volume = 761.268 cuft = 9 - Junction of ditches for culveste2tandtspe Inflow hyd. No. = Trapezoidal Reach length Channel slope = 815.0 ft= 2.3 % Bottom width = 5.0 ftManning's n = 0.040Side slope Max. depth = 3.0:1= 5.0 ftRating curve x Rating curve m = 1.341= 1.931Ave. velocity Routing coeff. = 0.3713= 0.00 ft/s



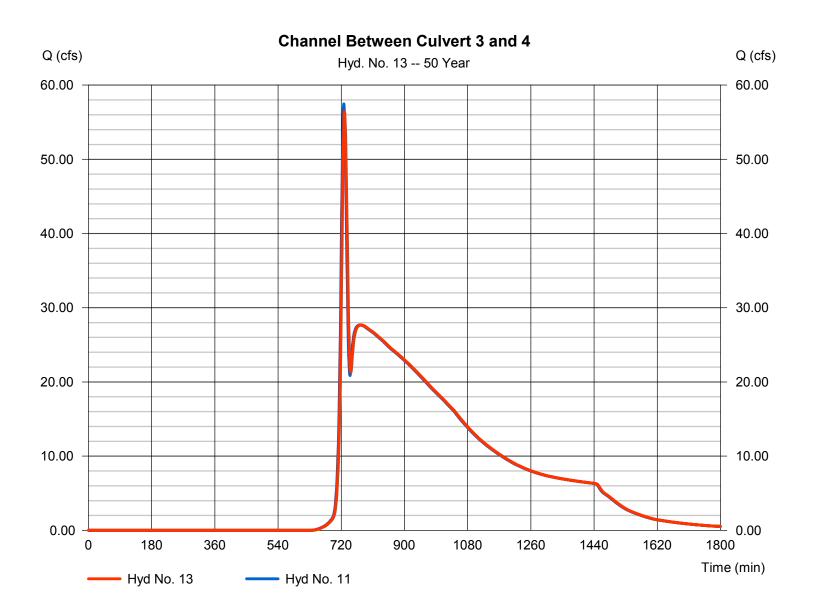
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Hyd. No. 13

Channel Between Culvert 3 and 4

Peak discharge Hydrograph type = 56.42 cfs= Reach Storm frequency = 50 yrsTime to peak = 729 min Time interval = 1 min Hyd. volume = 761.260 cuft Inflow hyd. No. = 11 - Ditch betweenn culverts 2 Spection type = Trapezoidal Channel slope = 1.2 % Reach length = 450.0 ftBottom width = 5.0 ftManning's n = 0.040Side slope Max. depth = 3.0:1= 3.0 ftRating curve x Rating curve m = 1.395= 1.321Ave. velocity Routing coeff. = 0.00 ft/s= 0.4652



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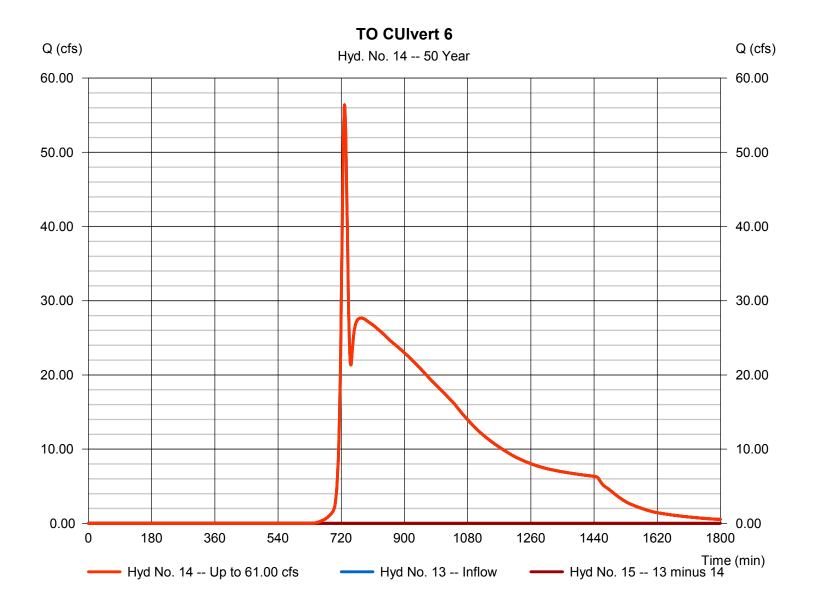
Hyd. No. 14

TO CUIvert 6

Hydrograph type= Diversion1Peak discharge= 56.42 cfsStorm frequency= 50 yrsTime to peak= 729 minTime interval= 1 minHyd. volume= 761,260 cuft

Inflow hydrograph = 13 - Channel Between Culvert 2 mathdli 4 erted hyd. = 15

Diversion method = Constant Q Constant Q = 61.00 cfs



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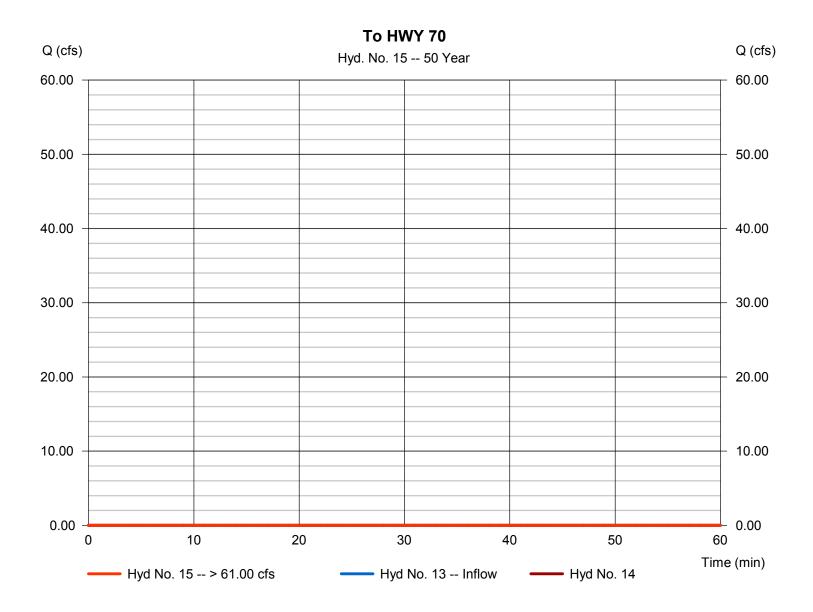
Tuesday, 03 / 28 / 2017

Hyd. No. 15

To HWY 70

Hydrograph type = Diversion2 Peak discharge = 0.000 cfs
Storm frequency = 50 yrs Time to peak = n/a
Time interval = 1 min Hyd. volume = 0 cuft
Inflow hydrograph = 13 - Channel Between Culvert 2nathdiserted hyd. = 14

Diversion method = Constant Q Constant Q = 61.00 cfs



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Hyd. No. 17

Sheet flow from houses to hwy 70

Hydrograph type = SCS Runoff Peak discharge = 47.37 cfsStorm frequency = 50 yrsTime to peak = 738 min Time interval = 1 min Hyd. volume = 232.111 cuft Curve number Drainage area = 20.330 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 39.63 min = TR55 Total precip. = 6.67 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



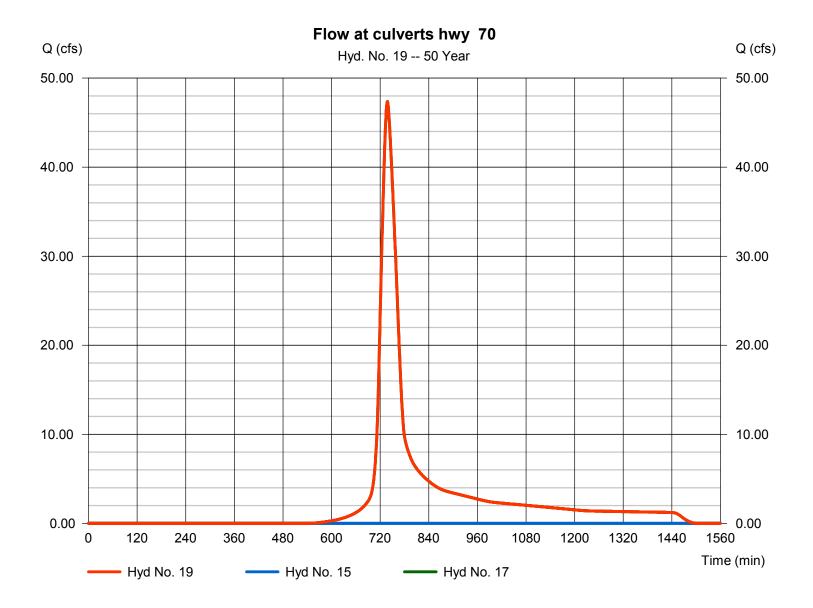
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Tuesday, 03 / 28 / 2017

Hyd. No. 19

Flow at culverts hwy 70

Hydrograph type = Combine Peak discharge = 47.37 cfsStorm frequency = 50 yrsTime to peak = 738 min Time interval = 1 min Hyd. volume = 232,111 cuft Inflow hyds. Contrib. drain. area = 20.330 ac= 15, 17



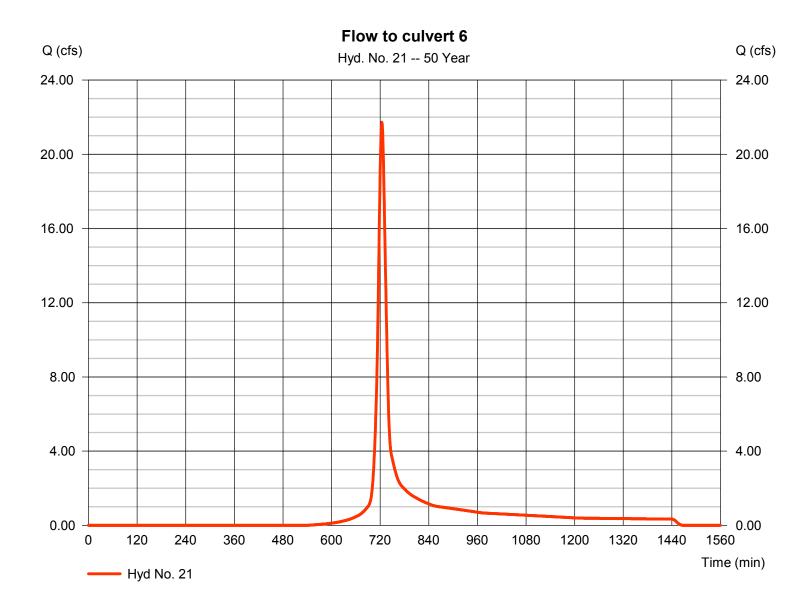
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Hyd. No. 21

Flow to culvert 6

Hydrograph type = SCS Runoff Peak discharge = 21.73 cfsStorm frequency = 50 yrsTime to peak = 724 min Time interval = 1 min Hyd. volume = 64,564 cuft Drainage area Curve number = 5.720 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 17.80 min = TR55 Total precip. = 6.67 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



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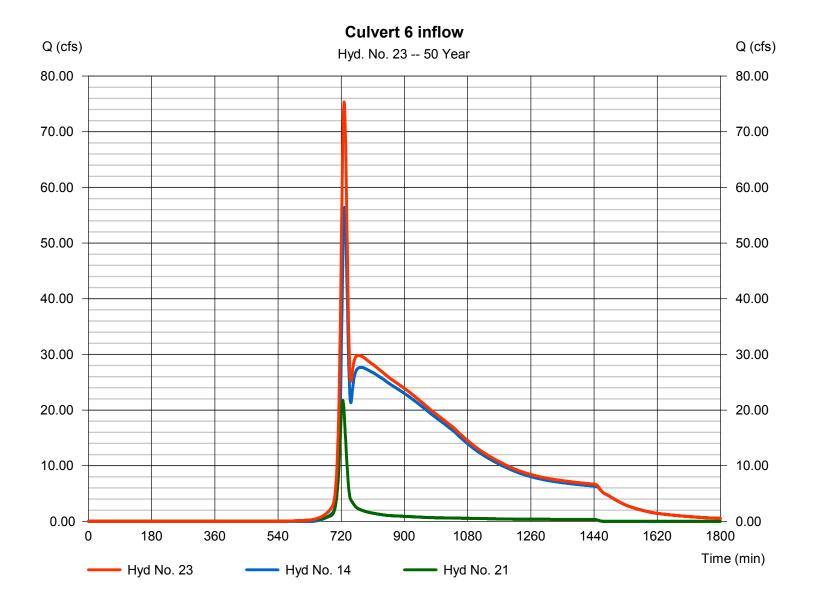
Tuesday, 03 / 28 / 2017

Hyd. No. 23

Culvert 6 inflow

Hydrograph type = Combine
Storm frequency = 50 yrs
Time interval = 1 min
Inflow hyds. = 14, 21

Peak discharge = 75.35 cfs
Time to peak = 728 min
Hyd. volume = 825,823 cuft
Contrib. drain. area = 5.720 ac



Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	192.30	1	735	905,950				Area Above Hannah Ford leading to
2	Reservoir	33.89	1	786	764,408	1	42.76	407,688	Pond
3	Reach	33.89	1	787	764,404	2			Ditch between Culvert 1 and culver 2
5	SCS Runoff	73.57	1	724	213,534				Area above culvert 5 to culvert 5
7	Reach	73.68	1	724	213,534	5			Ditch between culvert 5 and outfall of
9	Combine	73.68	1	724	977,938	3, 7,			Junction of ditches for culvert 2 and 5
11	Reach	71.45	1	727	977,931	9			Ditch betweenn culverts 2 and 3
13	Reach	70.31	1	729	977,924	11			Channel Between Culvert 3 and 4
14	Diversion1	61.00	1	725	974,637	13			TO CUlvert 6
15	Diversion2	9.307	1	729	3,287	13			To HWY 70
17	SCS Runoff	56.85	1	738	276,957				Sheet flow from houses to hwy 70
19	Combine	57.64	1	731	280,027	15, 17,			Flow at culverts hwy 70
21	SCS Runoff	26.00	1	724	77,038				Flow to culvert 6
23	Combine	87.24	1	725	1,051,892	14, 21,			Culvert 6 inflow
Div	ersion analys	is with 1 p	oond (1).	gpw	Return P	eriod: 100	Year	Tuesday, 0	03 / 28 / 2017

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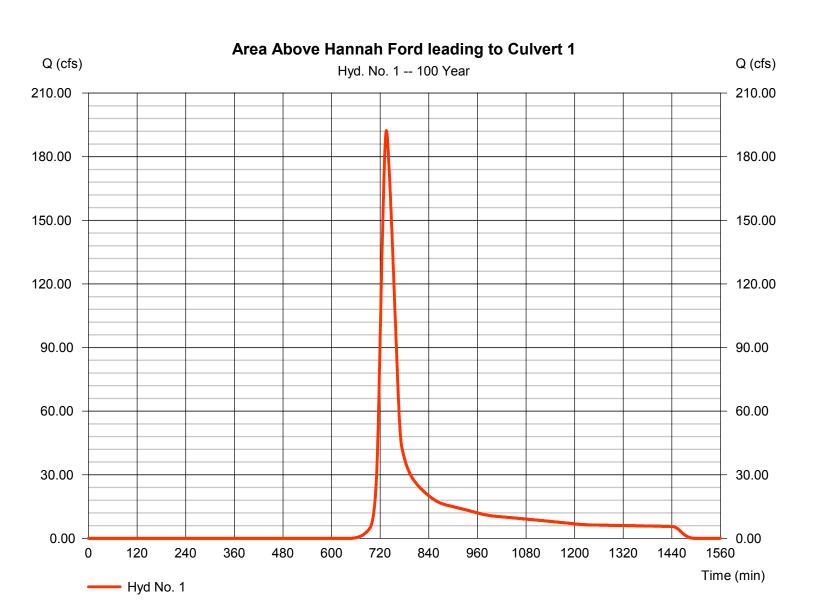
Tuesday, 03 / 28 / 2017

Hyd. No. 1

Area Above Hannah Ford leading to Culvert 1

= SCS Runoff Peak discharge = 192.30 cfsHydrograph type Storm frequency = 100 yrsTime to peak = 735 min Time interval = 1 min Hyd. volume = 905.950 cuft Curve number Drainage area = 100.000 ac= 56* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 34.70 min = TR55 Total precip. Distribution = Type II = 7.42 inStorm duration = 24 hrs Shape factor = 484

^{*} Composite (Area/CN) = [(17.000 x 36) + (83.000 x 60)] / 100.000



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

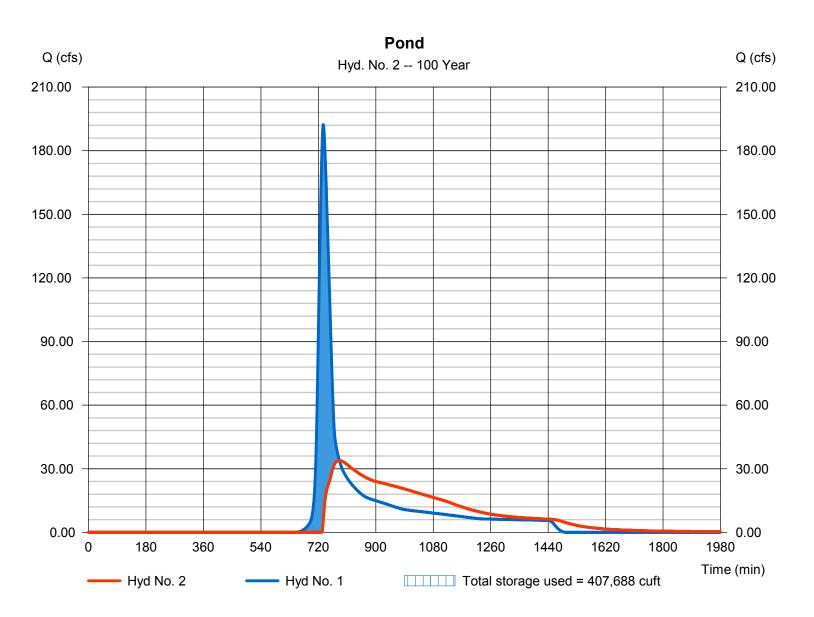
Tuesday, 03 / 28 / 2017

Hyd. No. 2

Pond

Hydrograph type Peak discharge = 33.89 cfs= Reservoir Storm frequency = 100 yrsTime to peak = 786 min Time interval = 1 min Hyd. volume = 764,408 cuft = 1 - Area Above Hannah Ford levading tevatibrert 1 = 42.76 ftInflow hyd. No. Max. Storage Reservoir name = Pond Paired with Diversion = 407,688 cuft

Storage Indication method used.



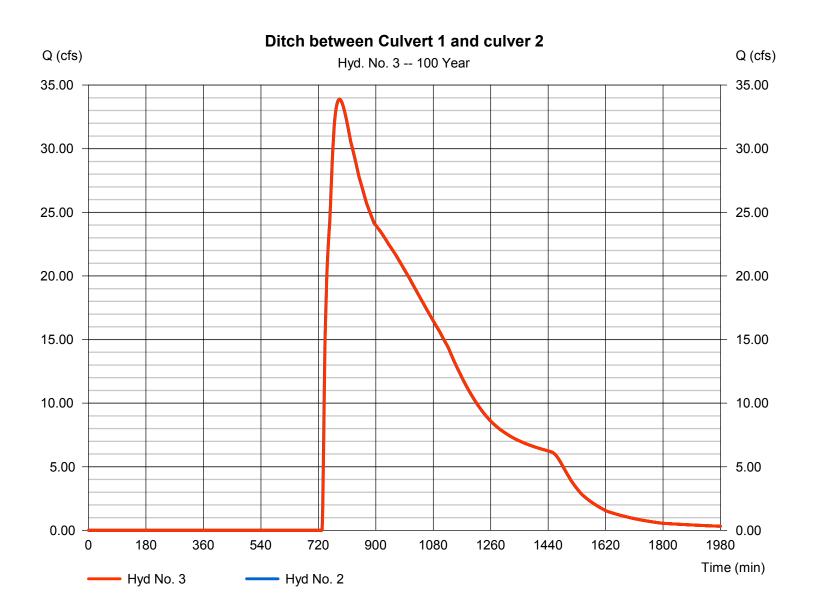
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

Tuesday, 03 / 28 / 2017

Hyd. No. 3

Ditch between Culvert 1 and culver 2

Hydrograph type	= Reach	Peak discharge	= 33.89 cfs
Storm frequency	= 100 yrs	Time to peak	= 787 min
Time interval	= 1 min	Hyd. volume	= 764,404 cuft
Inflow hyd. No.	= 2 - Pond	Section type	Trapezoidal
Reach length	= 118.0 ft	Channel slope	= 1.8 %
Manning's n	= 0.030	Bottom width	= 3.0 ft
Side slope	= 3.0:1	Max. depth	= 5.0 ft
Rating curve x	= 3.202	Rating curve m	= 1.279
Ave. velocity	= 0.00 ft/s	Routing coeff.	= 1.2706



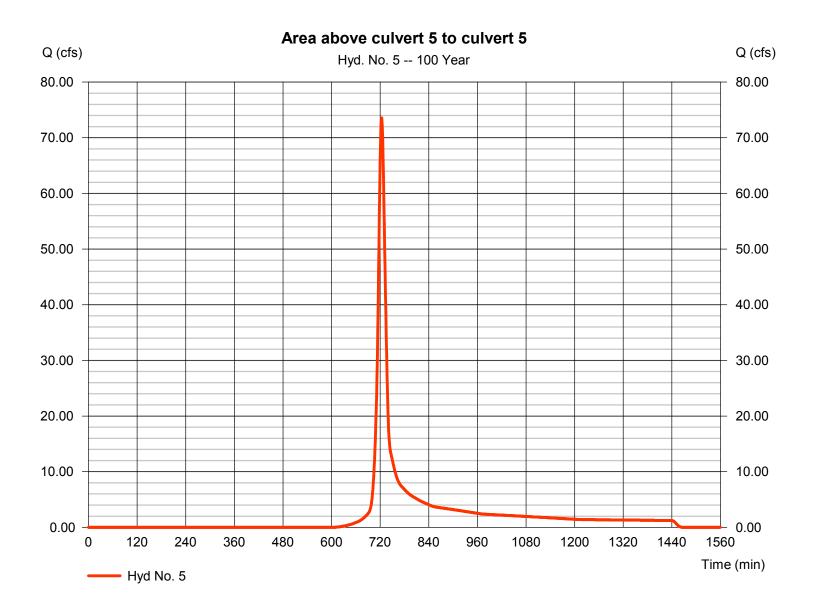
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

Tuesday, 03 / 28 / 2017

Hyd. No. 5

Area above culvert 5 to culvert 5

Hydrograph type = SCS Runoff Peak discharge = 73.57 cfsStorm frequency = 100 yrsTime to peak = 724 min Time interval = 1 min Hyd. volume = 213,534 cuft Drainage area Curve number = 20.000 ac= 60 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 16.77 min = TR55 Total precip. = 7.42 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



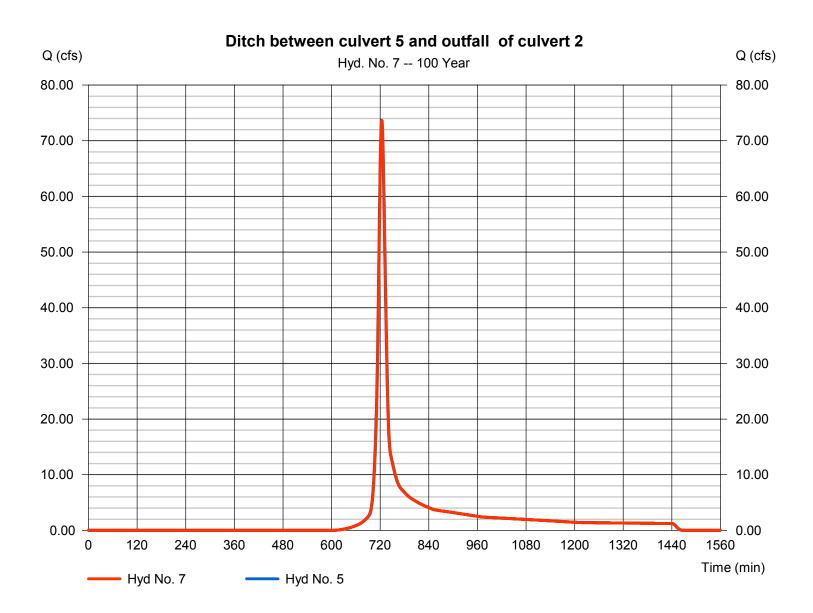
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

Tuesday, 03 / 28 / 2017

Hyd. No. 7

Ditch between culvert 5 and outfall of culvert 2

= Reach Peak discharge = 73.68 cfsHydrograph type Storm frequency = 100 yrsTime to peak = 724 min Time interval = 1 min Hyd. volume = 213.534 cuft Inflow hyd. No. = 5 - Area above culvert 5 to c = Trapezoidal Channel slope Reach length = 174.0 ft= 3.8 % Bottom width = 3.0 ftManning's n = 0.040Side slope Max. depth = 2.0 ft= 2.0:1Rating curve x = 3.490Rating curve m = 1.249Ave. velocity Routing coeff. = 1.1603= 0.00 ft/s



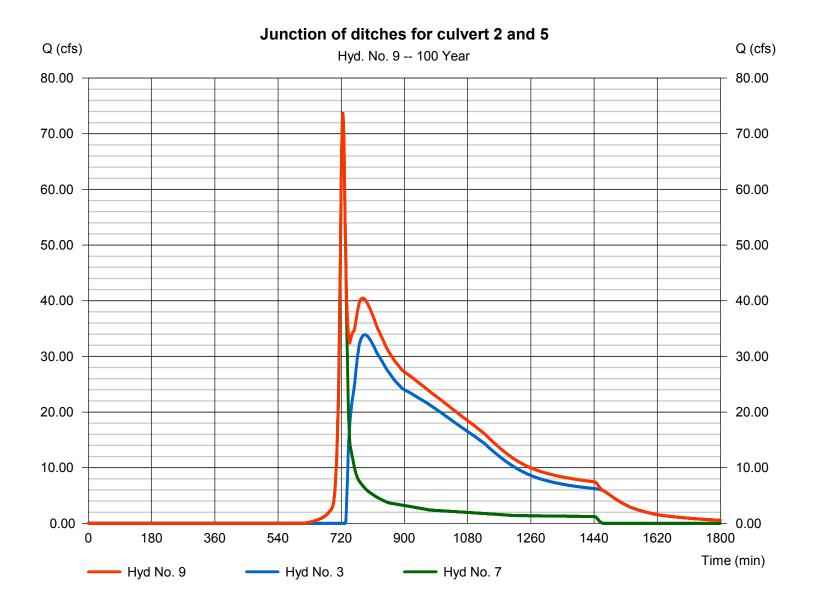
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

Tuesday, 03 / 28 / 2017

Hyd. No. 9

Junction of ditches for culvert 2 and 5

Hydrograph type = Combine Peak discharge = 73.68 cfsStorm frequency Time to peak = 100 yrs= 724 min Time interval = 1 min Hyd. volume = 977,938 cuft Inflow hyds. = 3, 7 Contrib. drain. area = 0.000 ac



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

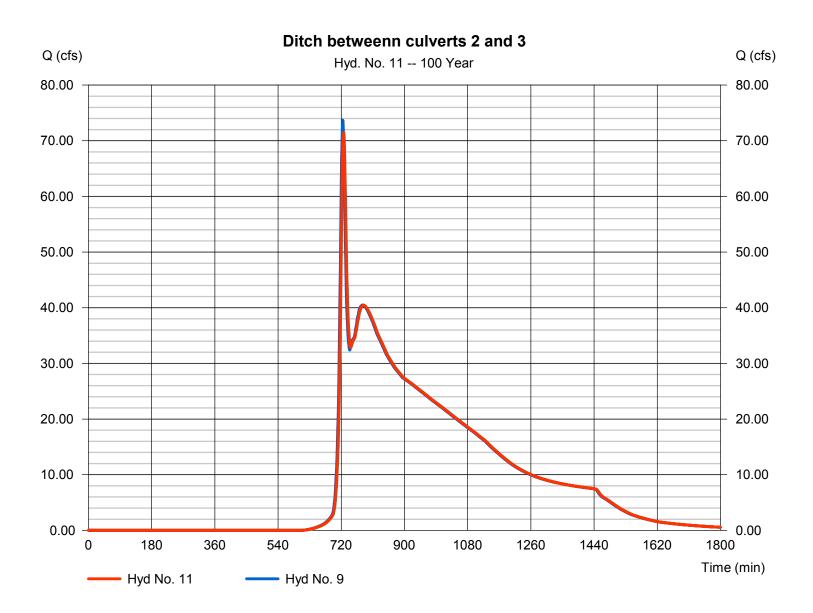
Tuesday, 03 / 28 / 2017

Hyd. No. 11

Ditch betweenn culverts 2 and 3

Peak discharge = Reach = 71.45 cfsHydrograph type Storm frequency = 100 yrsTime to peak = 727 min Time interval = 1 min Hyd. volume = 977,931 cuft = 9 - Junction of ditches for culveste2tandtspe Inflow hyd. No. = Trapezoidal Reach length Channel slope = 2.3 % = 815.0 ftBottom width = 5.0 ftManning's n = 0.040Side slope Max. depth = 3.0:1= 5.0 ftRating curve x Rating curve m = 1.341= 1.931Ave. velocity Routing coeff. = 0.3880= 0.00 ft/s

Modified Att-Kin routing method used.



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

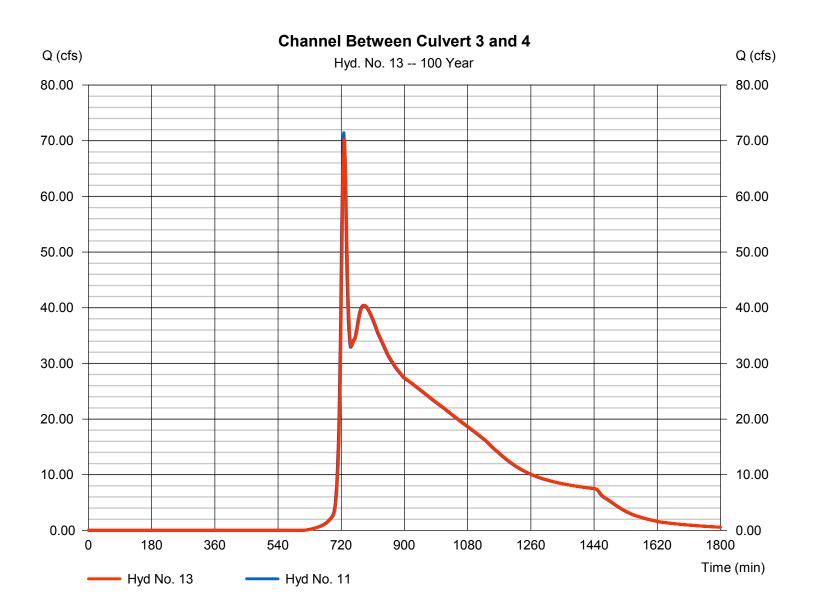
Tuesday, 03 / 28 / 2017

Hyd. No. 13

Channel Between Culvert 3 and 4

Peak discharge = 70.31 cfsHydrograph type = Reach Storm frequency = 100 yrsTime to peak = 729 min Time interval = 1 min Hyd. volume = 977,924 cuft Inflow hyd. No. = 11 - Ditch betweenn culverts 2 Spection type = Trapezoidal Channel slope = 1.2 % Reach length = 450.0 ftBottom width = 5.0 ftManning's n = 0.040Side slope Max. depth = 3.0:1= 3.0 ftRating curve x Rating curve m = 1.395= 1.321Ave. velocity Routing coeff. = 0.00 ft/s= 0.4843

Modified Att-Kin routing method used.



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

Tuesday, 03 / 28 / 2017

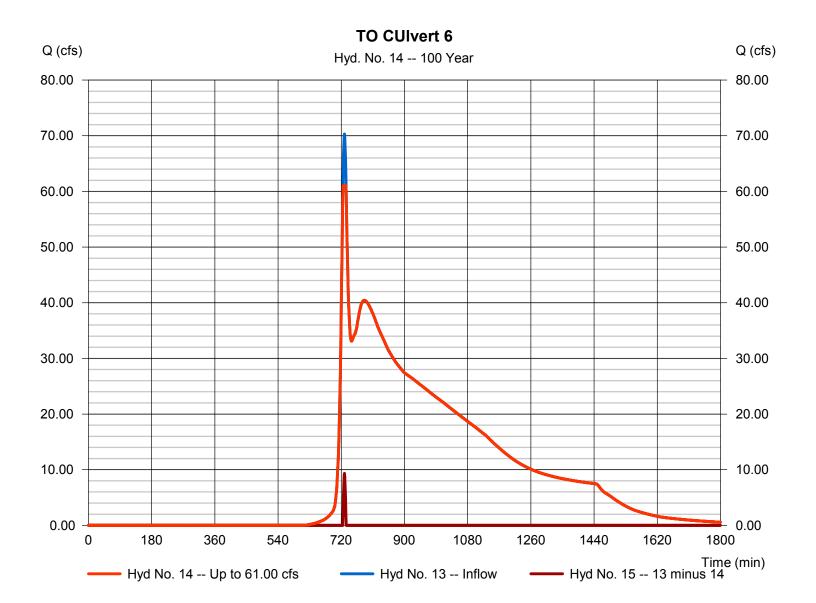
Hyd. No. 14

TO CUIvert 6

Hydrograph type= Diversion1Peak discharge= 61.00 cfsStorm frequency= 100 yrsTime to peak= 725 minTime interval= 1 minHyd. volume= 974,637 cuft

Inflow hydrograph = 13 - Channel Between Culvert 2nathdliverted hyd. = 15

Diversion method = Constant Q Constant Q = 61.00 cfs



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

Tuesday, 03 / 28 / 2017

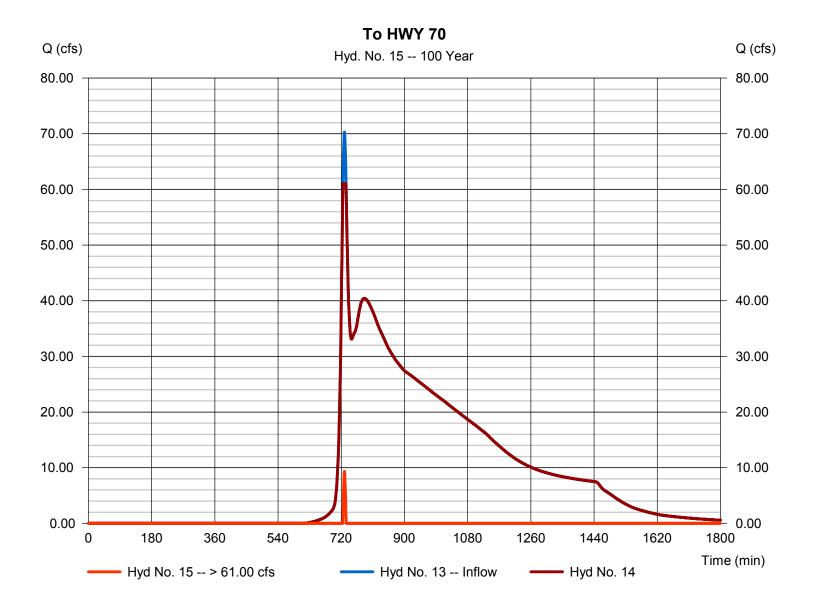
Hyd. No. 15

To HWY 70

Hydrograph type= Diversion2Peak discharge= 9.307 cfsStorm frequency= 100 yrsTime to peak= 729 minTime interval= 1 minHyd. volume= 3,287 cuft

Inflow hydrograph = 13 - Channel Between Culvert 2nathdliverted hyd. = 14

Diversion method = Constant Q Constant Q = 61.00 cfs



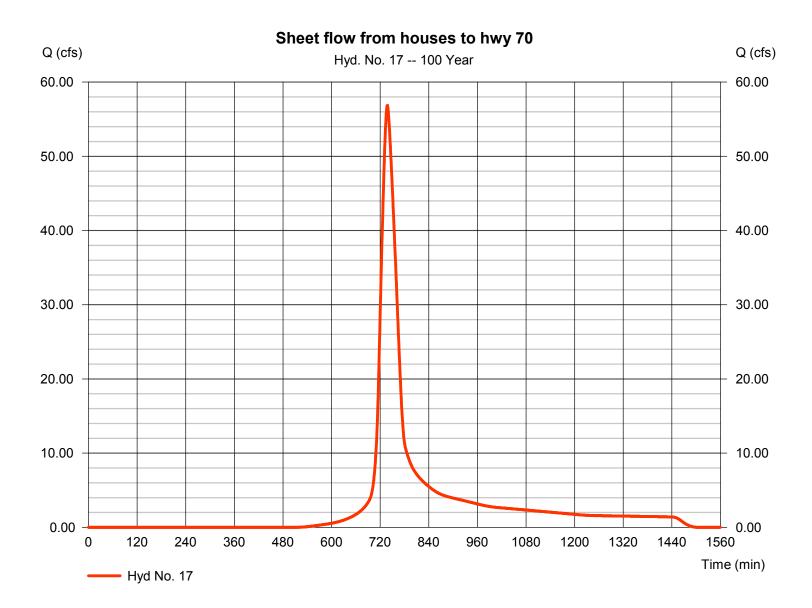
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

Tuesday, 03 / 28 / 2017

Hyd. No. 17

Sheet flow from houses to hwy 70

Hydrograph type = SCS Runoff Peak discharge = 56.85 cfsStorm frequency = 100 yrsTime to peak = 738 min Time interval = 1 min Hyd. volume = 276,957 cuft Curve number Drainage area = 20.330 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 39.63 min = TR55 Total precip. = 7.42 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



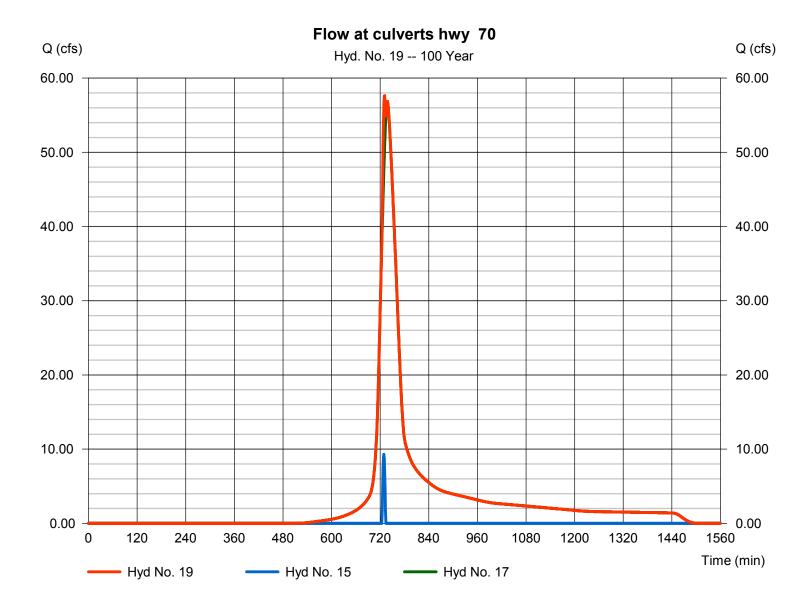
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

Tuesday, 03 / 28 / 2017

Hyd. No. 19

Flow at culverts hwy 70

Hydrograph type = Combine Peak discharge = 57.64 cfsStorm frequency = 100 yrsTime to peak = 731 min Time interval = 1 min Hyd. volume = 280,027 cuft Contrib. drain. area Inflow hyds. = 15, 17 = 20.330 ac



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

= 24 hrs

Tuesday, 03 / 28 / 2017

= 484

Hyd. No. 21

Flow to culvert 6

Storm duration

Hydrograph type = SCS Runoff Peak discharge = 26.00 cfsStorm frequency = 100 yrsTime to peak = 724 min Time interval = 1 min Hyd. volume = 77,038 cuft Drainage area Curve number = 5.720 ac= 68 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 17.80 min = TR55 Total precip. = 7.42 inDistribution = Type II

Shape factor

Flow to culvert 6 Q (cfs) Q (cfs) Hyd. No. 21 -- 100 Year 28.00 28.00 24.00 24.00 20.00 20.00 16.00 16.00 12.00 12.00 8.00 8.00 4.00 4.00 0.00 0.00 120 240 360 480 600 720 840 960 1080 1200 1320 1440 1560 Time (min) Hyd No. 21

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2016 by Autodesk, Inc. v11

Tuesday, 03 / 28 / 2017

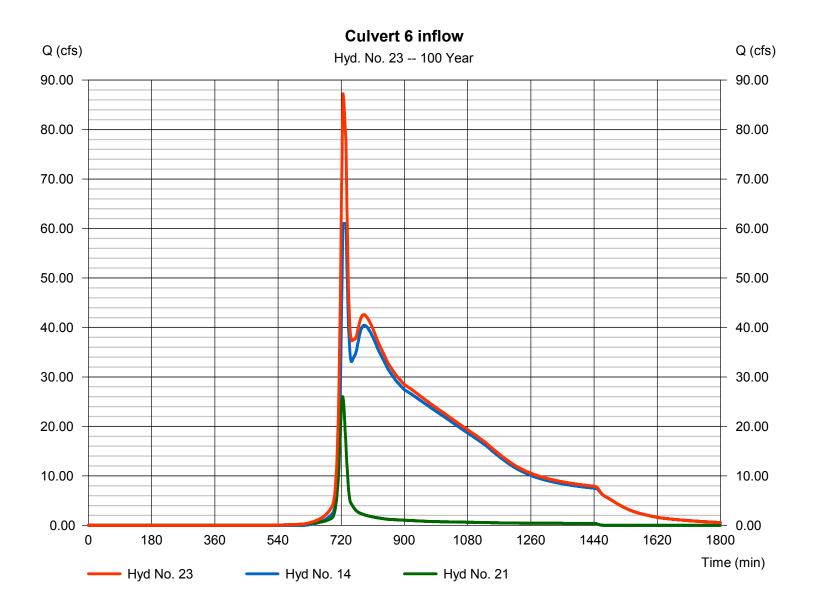
Hyd. No. 23

Culvert 6 inflow

Hydrograph type = Combine Peak discharge = 87.24 cfs
Storm frequency = 100 yrs Time to peak = 725 min

Time interval = 1 min Hyd. volume = 1,051,892 cuft

Inflow hyds. = 14, 21 Contrib. drain. area = 5.720 ac





ENCLOSURE (C)

CULVERT / CHANNEL REPORTS

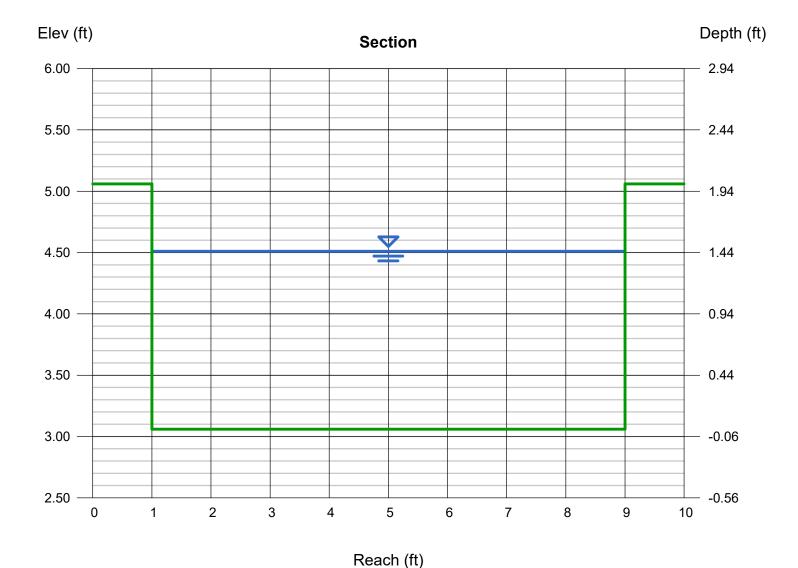
Channel Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Sunday, Mar 5 2017

Concrete Diversion Ditch

Rectangular		Highlighted	
Bottom Width (ft)	= 8.00	Depth (ft)	= 1.45
Total Depth (ft)	= 2.00	Q (cfs)	= 75.00
		Area (sqft)	= 11.60
Invert Elev (ft)	= 3.06	Velocity (ft/s)	= 6.47
Slope (%)	= 0.40	Wetted Perim (ft)	= 10.90
N-Value	= 0.015	Crit Depth, Yc (ft)	= 1.40
		Top Width (ft)	= 8.00
Calculations		EGL (ft)	= 2.10
Compute by:	Known Q		
Known Q (cfs)	= 75.00		

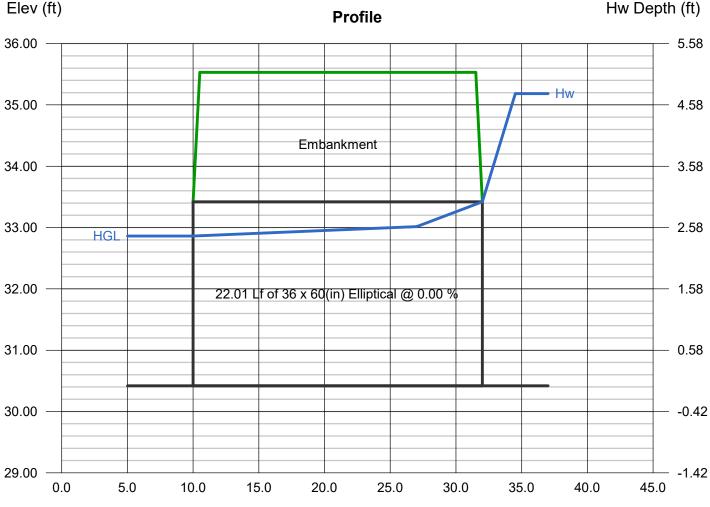


Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Monday, Mar 6 2017

Culvert 1 50yr

Invert Elev Dn (ft)	= 30.42	Calculations	
Pipe Length (ft)	= 22.01	Qmin (cfs)	= 98.00
Slope (%)	= 0.00	Qmax (cfs)	= 150.27
Invert Elev Up (ft)	= 30.42	Tailwater Élev (ft)	= Normal
Rise (in)	= 36.0	. ,	
Shape	= Elliptical	Highlighted	
Span (in)	= 60.0	Qtotal (cfs)	= 98.00
No. Barrels	= 1	Qpipe (cfs)	= 98.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	 Horizontal Ellipse Concrete 	Veloc Dn (ft/s)	= 9.19
Culvert Entrance	Square edge w/headwall (H)	Veloc Up (ft/s)	= 8.90
Coeff. K,M,c,Y,k	= 0.01, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 32.86
		HGL Up (ft)	= 33.06
Embankment		Hw Elev (ft)	= 35.18
Top Elevation (ft)	= 35.53	Hw/D (ft)	= 1.59
Top Width (ft)	= 21.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 300.00		
Elev (ft)	Profile		Hw Depth (ft)



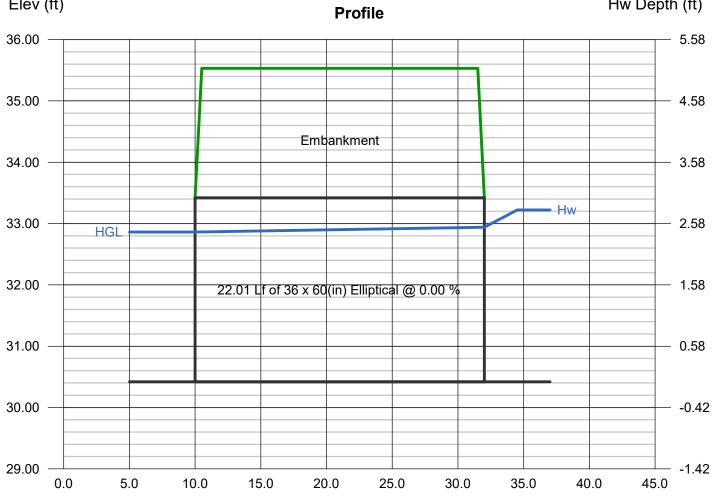
Reach (ft)

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Monday, Mar 6 2017

Culvert 1 50yr with Pond

Invert Elev Dn (ft)	= 30.42	Calculations	
Pipe Length (ft)	= 22.01	Qmin (cfs)	= 0.00
Slope (%)	= 0.00	Qmax (cfs)	= 37.95
Invert Elev Up (ft)	= 30.42	Tailwater Élev (ft)	= Normal
Rise (in)	= 36.0	,	
Shape	= Elliptical	Highlighted	
Span (in)	= 60.0	Qtotal (cfs)	= 37.00
No. Barrels	= 1	Qpipe (cfs)	= 37.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	 Horizontal Ellipse Concrete 	Veloc Dn (ft/s)	= 3.47
Culvert Entrance	Square edge w/headwall (H)	Veloc Up (ft/s)	= 3.47
Coeff. K,M,c,Y,k	= 0.01, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 32.86
		HGL Up (ft)	= 32.94
Embankment		Hw Elev (ft)	= 33.22
Top Elevation (ft)	= 35.53	Hw/D (ft)	= 0.93
Top Width (ft)	= 21.00	Flow Regime	= Outlet Control
Crest Width (ft)	= 300.00		
Flev (ft)	_		Hw Denth (ft)

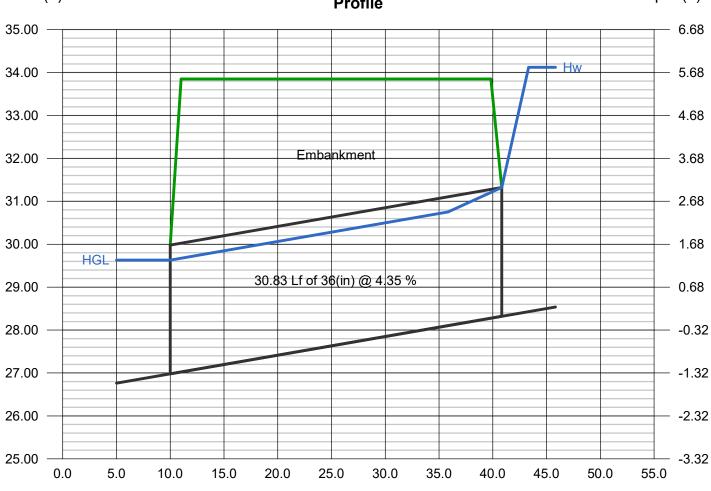


Reach (ft)

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Culvert 2 50 yr Existing Conditions

Cuiveit 2 30 yi Lx	isting Conditions		
Invert Elev Dn (ft)	= 26.98	Calculations	
Pipe Length (ft)	= 30.83	Qmin (cfs)	= 13.00
Slope (%)	= 4.35	Qmax (cfs)	= 112.00
Invert Elev Up (ft)	= 28.32	Tailwater Élev (ft)	= Normal
Rise (in)	= 36.0	. ,	
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 112.00
No. Barrels	= 1	Qpipe (cfs)	= 69.57
n-Value	= 0.013	Qovertop (cfs)	= 42.43
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 10.53
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 10.53
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 29.63
		HGL Up (ft)	= 30.97
Embankment		Hw Elev (ft)	= 34.12
Top Elevation (ft)	= 33.85	Hw/D (ft)	= 1.93
Top Width (ft)	= 28.80	Flow Regime	= Inlet Control
Crest Width (ft)	= 100.00		
Elev (ft)	Profile		Hw Depth (ft)
35.00			6.68
34.00			1w 5.68
			0.00



Reach (ft)

28.00 -

27.00 -

26.00 -

25.00 -

0.0

5.0

10.0

15.0

20.0

-0.32

- -1.32

- -2.32

- -3.32

55.0

 $\label{thm:local_equation} \mbox{Hydraflow Express Extension for Autodesk@ AutoCAD@ Civil 3D@ by Autodesk, Inc.}$

Culvert 2 100 vr Existing Conditions

Culvert 2 100 yr Ex	Culvert 2 100 yr Existing Conditions				
Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 26.98 = 30.83 = 4.35 = 28.32 = 36.0	Calculations Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 150.00 = 192.00 = Normal		
Shape Span (in) No. Barrels n-Value Culvert Type Culvert Entrance Coeff. K,M,c,Y,k	= Circular = 36.0 = 1 = 0.013 = Circular Concrete = Square edge w/headwall (C) = 0.0098, 2, 0.0398, 0.67, 0.5	Highlighted Qtotal (cfs) Qpipe (cfs) Qovertop (cfs) Veloc Dn (ft/s) Veloc Up (ft/s) HGL Dn (ft) HGL Up (ft)	= 192.00 = 71.85 = 120.15 = 10.78 = 10.78 = 29.66 = 31.00		
Embankment Top Elevation (ft) Top Width (ft) Crest Width (ft)	= 33.85 = 28.80 = 100.00	Hw Elev (ft) Hw/D (ft) Flow Regime	= 34.38 = 2.02 = Inlet Control		
Elev (ft)	Profile		Hw Depth (ft) 6.68		
34.00			Hw 5.68		
33.00			4.68		
32.00	Embankment		3.68		
31.00			2.68		
30.00			1.68		
HGL					

Reach (ft)

30.0

35.0

40.0

45.0

50.0

25.0

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Culvert 2 50 yr with Diversion and Pond

Pipe Le Slope (lev Up (= 26. = 30. = 4.3 = 28. = 36.	83 5 32				Calculatio Qmin (cfs Qmax (cfs Tailwater) s)	:	= 13.00 = 37.95 = Norm	5
Shape Span (ii No. Bar n-Value Culvert Culvert	n) rels		= Cir = 36. = 1 = 0.0 = Cir = Sq	cular 0	je w/hea	•	C) 5	Highlight Qtotal (cfs Qpipe (cfs Qovertop Veloc Dn Veloc Up HGL Dn (the control of the control of the cfs	s) (cfs) (ft/s) (ft/s) ft)	: : :	= 37.00 = 37.00 = 0.00 = 12.55 = 7.49 = 28.28 = 30.30) 5 3
Top Wid	evation (dth (ft) /idth (ft)	,	= 33. = 28. = 100	80				Hw Elev (i Hw/D (ft) Flow Regi	ft)	:	= 31.37 = 1.02 = Inlet	Control
Elev (ft))					Profile					пw D	epth (ft)
34.00 —												5.68
33.00 —												4.68
32.00 —					Emba	nkment						3.68
31.00 —										Hw		2.68
30.00 —												1.68
29.00 —				30.8	3 Lf of 3	6(in) @ 4	35 %					0.68
28.00 —	HGL											-0.32
27.00 —			_									-1.32
26.00 —												-2.32
25.00 —	0.0 5	.0 10	0.0 1	5.0 20	0.0 25	5.0 30	0.0	35.0 40	0.0 45	5.0 5	0.0 5	-3.32

Reach (ft)

 $\label{thm:condition} \mbox{Hydraflow Express Extension for Autodesk@ AutoCAD@ Civil 3D@ by Autodesk, Inc.}$

Culvert 2 100 yr with Diversion and Pond

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 26.98 = 30.83 = 4.35 = 28.32 = 36.0	Calculations Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 30.00 = 77.00 = Normal
Shape Span (in) No. Barrels n-Value Culvert Type Culvert Entrance Coeff. K,M,c,Y,k	= Circular = 36.0 = 1 = 0.013 = Circular Concrete = Square edge w/headwall (C) = 0.0098, 2, 0.0398, 0.67, 0.5	Highlighted Qtotal (cfs) Qpipe (cfs) Qovertop (cfs) Veloc Dn (ft/s) Veloc Up (ft/s) HGL Dn (ft) HGL Up (ft)	= 77.00 = 68.02 = 8.98 = 10.36 = 10.36 = 29.61 = 30.95
Embankment Top Elevation (ft)	= 33.85	Hw Elev (ft) Hw/D (ft)	= 33.95 = 1.88
Top Width (ft) Crest Width (ft)	= 28.80 = 100.00	Flow Regime	= Inlet Control
Elev (ft)			Hw Depth (ft)
34.00	Profile		w 5.68
34.00			N 3.08
33.00			4.68
32.00	Embankment		3.68
31.00			2.68
30.00 HGL			1.68
29.00	30.83 Lf of 36(in) @ 4.35	%	0.68
28.00			-0.32
27.00			-1.32
26.00			-2.32
25.00 0.0 5.0 1	0.0 15.0 20.0 25.0 30.0	35.0 40.0 45.0	50.0 55.0 -3.32

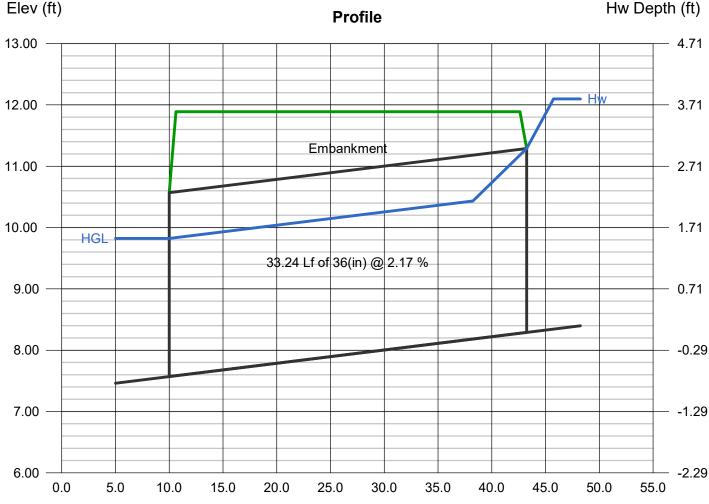
Reach (ft)

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Monday, Feb 13 2017

Culvert 3 50yr Existing Conditions

Invert Elev Dn (ft)	= 7.57	Calculations	
Pipe Length (ft) ´	= 33.24	Qmin (cfs)	= 82.00
Slope (%)	= 2.17	Qmax (cfs)	= 181.23
Invert Elev Up (ft)	= 8.29	Tailwater Élev (ft)	= Normal
Rise (in)	= 36.0		
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 172.00
No. Barrels	= 3	Qpipe (cfs)	= 143.82
n-Value	= 0.013	Qovertop (cfs)	= 28.18
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 8.42
Culvert Entrance	Square edge w/headwall (C)	Veloc Up (ft/s)	= 8.42
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 9.82
		HGL Up (ft)	= 10.54
Embankment		Hw Elev (ft)	= 12.10
Top Elevation (ft)	= 11.89	Hw/D (ft)	= 1.27
Top Width (ft)	= 32.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 100.00		
Elev (ft)	Profile		Hw Depth (ft)



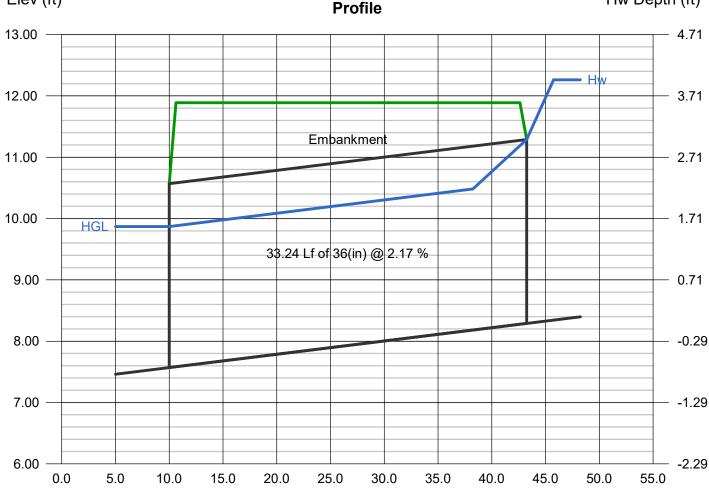
Reach (ft)

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Monday, Mar 6 2017

Culvert 3 100yr Existing Conditions

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 7.57 = 33.24 = 2.17 = 8.29 = 36.0	Calculations Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 82.00 = 230.00 = Normal
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 222.00
No. Barrels	= 3	Qpipe (cfs)	= 150.17
n-Value	= 0.013	Qovertop (cfs)	= 71.83
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 8.60
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 8.60
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 9.87
		HGL Up (ft)	= 10.59
Embankment		Hw Elev (ft)	= 12.26
Top Elevation (ft)	= 11.89	Hw/D (ft)	= 1.32
Top Width (ft)	= 32.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 100.00		
Elev (ft)	Profile		Hw Depth (ft)

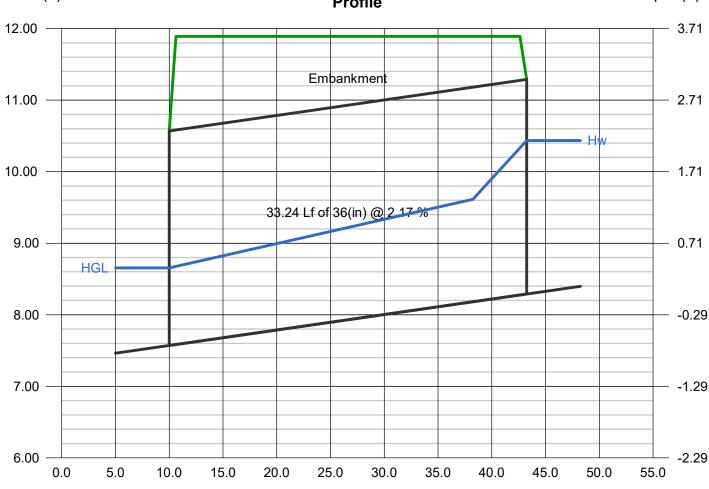


Reach (ft)

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Culvert 3 50yr With Diversion and Pond

•			
Invert Elev Dn (ft)	= 7.57	Calculations	
Pipe Length (ft)	= 33.24	Qmin (cfs)	= 20.00
Slope (%)	= 2.17	Qmax (cfs)	= 65.83
Invert Èlev Up (ft)	= 8.29	Tailwater Élev (ft)	= Normal
Rise (in)	= 36.0	()	
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 65.00
No. Barrels	= 3	Qpipe (cfs)	= 65.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 9.41
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 6.16
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 8.65
		HGL Up (ft)	= 9.79
Embankment		Hw Elev (ft)	= 10.43
Top Elevation (ft)	= 11.89	Hw/D (ft)	= 0.71
Top Width (ft)	= 32.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 100.00	· ·	
Elev (ft)	- au		Hw Depth (ft)
()	Profile		()
12.00			3.71

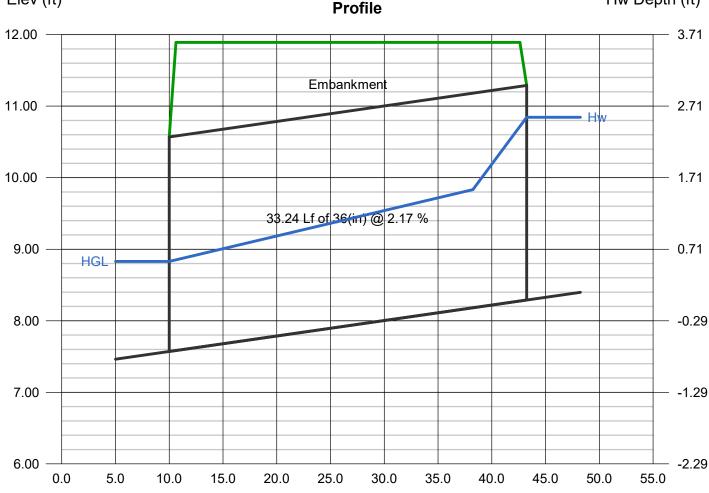


Reach (ft)

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Culvert 3 100yr With Diversion and Pond

Invert Elev Dn (ft) Pipe Length (ft) Slope (%)	= 7.57 = 33.24 = 2.17	Calculations Qmin (cfs) Qmax (cfs)	= 80.00 = 85.00
Invert Elev Up (ft)	= 8.29	Tailwater Elev (ft)	= Normal
Rise (in)	= 36.0		
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 85.00
No. Barrels	= 3	Qpipe (cfs)	= 85.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Concrete	Veloc Dn (ft/s)	= 10.06
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 6.76
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 8.83
		HGL Up (ft)	= 10.01
Embankment		Hw Elev (ft)	= 10.85
Top Elevation (ft)	= 11.89	Hw/D (ft)	= 0.85
Top Width (ft)	= 32.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 100.00		
Elev (ft)	Profile		Hw Depth (ft)



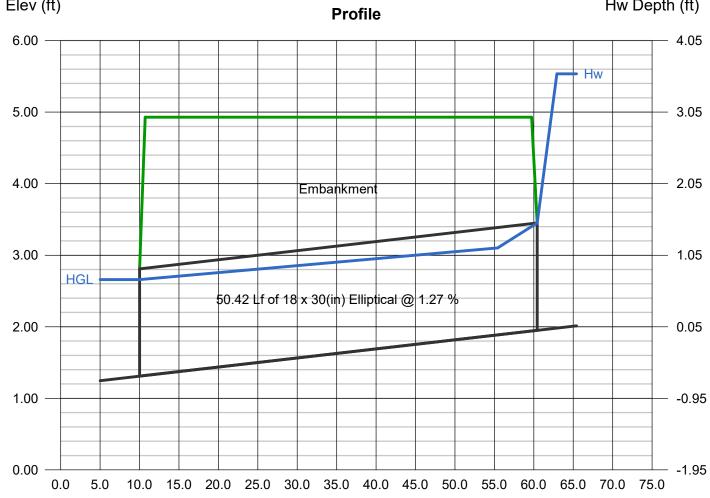
Reach (ft)

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Wednesday, Apr 5 2017

Culvert 4 50yr Existing Conditions

Invert Elev Dn (ft)	= 1.31	Calculations	
Pipe Length (ft) ´	= 50.42	Qmin (cfs)	= 0.00
Slope (%)	= 1.27	Qmax (cfs)	= 228.03
Invert Elev Up (ft)	= 1.95	Tailwater Élev (ft)	= (dc+D)/2
Rise (in)	= 18.0		
Shape	= Elliptical	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 220.00
No. Barrels	= 3	Qpipe (cfs)	= 71.29
n-Value	= 0.013	Qovertop (cfs)	= 148.71
Culvert Type	 Horizontal Ellipse Concrete 	Veloc Dn (ft/s)	= 8.40
Culvert Entrance	Square edge w/headwall (H)	Veloc Up (ft/s)	= 9.27
Coeff. K,M,c,Y,k	= 0.01, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 2.66
		HGL Up (ft)	= 3.15
Embankment		Hw Elev (ft)	= 5.54
Top Elevation (ft)	= 4.93	Hw/D (ft)	= 2.39
Top Width (ft)	= 49.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 100.00		
Elev (ft)	—		Hw Depth (ft)

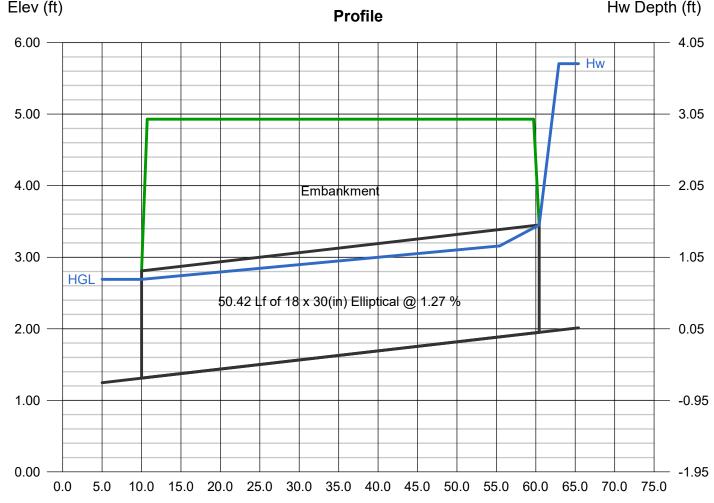


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Wednesday, Apr 5 2017

Culvert 4 100yr Existing Conditions

Invert Elev Dn (ft)	= 1.31	Calculations	
Pipe Length (ft)	= 50.42	Qmin (cfs)	= 200.00
Slope (%)	= 1.27	Qmax (cfs)	= 287.00
Invert Elev Up (ft)	= 1.95	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 18.0	, ,	, ,
Shape	= Elliptical	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 287.00
No. Barrels	= 3	Qpipe (cfs)	= 73.57
n-Value	= 0.013	Qovertop (cfs)	= 213.43
Culvert Type	 Horizontal Ellipse Concrete 	Veloc Dn (ft/s)	= 8.45
Culvert Entrance	= Square edge w/headwall (H)	Veloc Up (ft/s)	= 9.20
Coeff. K,M,c,Y,k	= 0.01, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 2.69
		HGL Up (ft)	= 3.21
Embankment		Hw Elev (ft)	= 5.70
Top Elevation (ft)	= 4.93	Hw/D (ft)	= 2.50
Top Width (ft)	= 49.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 100.00	-	
Fley (ft)			Hw Denth (ft)

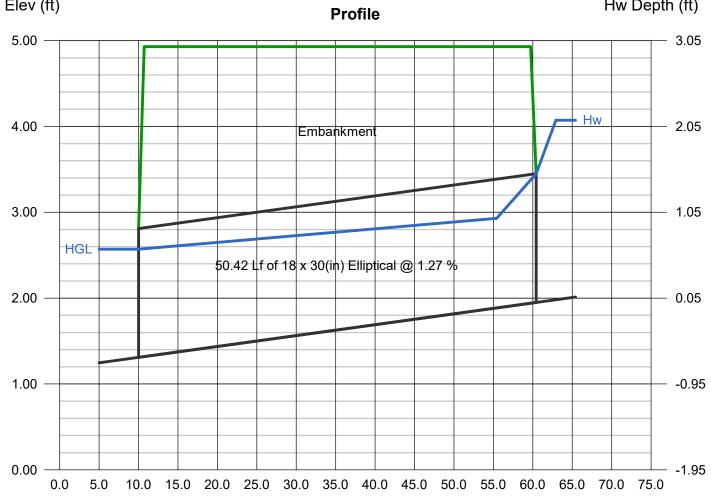


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Wednesday, Apr 5 2017

Culvert 4 50yr With Diversion and Pond

Invert Elev Dn (ft)	= 1.31	Calculations	
Pipe Length (ft)	= 50.42	Qmin (cfs)	= 35.00
Slope (%)	= 1.27	Qmax (cfs)	= 47.37
Invert Elev Up (ft)	= 1.95	Tailwater Élev (ft)	= (dc+D)/2
Rise (in)	= 18.0	,	, ,
Shape	= Elliptical	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 47.00
No. Barrels	= 3	Qpipe (cfs)	= 47.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	 Horizontal Ellipse Concrete 	Veloc Dn (ft/s)	= 5.88
Culvert Entrance	= Square edge w/headwall (H)	Veloc Up (ft/s)	= 7.09
Coeff. K,M,c,Y,k	= 0.01, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 2.57
		HGL Up (ft)	= 2.97
Embankment		Hw Elev (ft)	= 4.07
Top Elevation (ft)	= 4.93	Hw/D (ft)	= 1.41
Top Width (ft)	= 49.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 100.00	-	
Fley (ft)			Hw Denth (ft)



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Wednesday, Apr 5 2017

Culvert 4 100yr With Diversion and Pond

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 1.31 = 50.42 = 1.27 = 1.95 = 18.0	Calculations Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 35.00 = 56.85 = (dc+D)/2
Shape	= Elliptical	Highlighted	
Span (in)	= 30.0	Qtotal (cfs)	= 56.00
No. Barrels	= 3	Qpipe (cfs)	= 56.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	 Horizontal Ellipse Concrete 	Veloc Dn (ft/s)	= 6.78
Culvert Entrance	Square edge w/headwall (H)	Veloc Up (ft/s)	= 7.97
Coeff. K,M,c,Y,k	= 0.01, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 2.60
		HGL Up (ft)	= 3.03
Embankment		Hw Elev (ft)	= 4.54
Top Elevation (ft)	= 4.93	Hw/D (ft)	= 1.73
Top Width (ft)	= 49.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 100.00		
Elev (ft)	Profile		Hw Depth (ft)

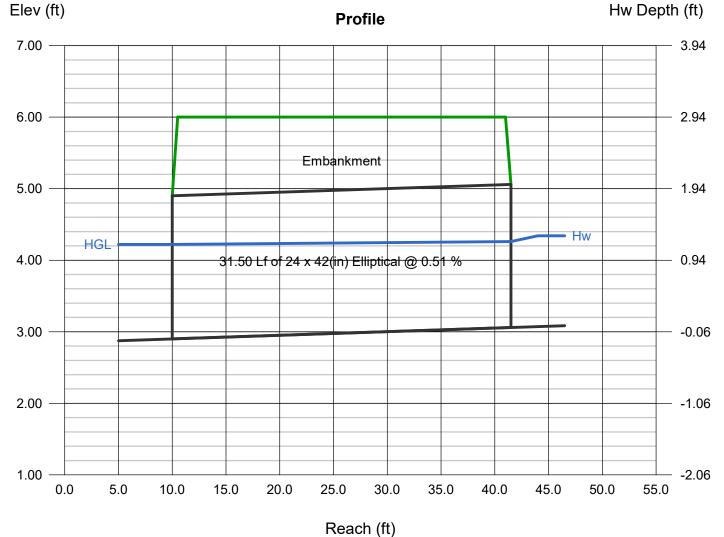
Elev (ft) **Profile** 5.00 -- 3.05 Hw 4.00 -- 2.05 Embankment 3.00 -— 1.05 HGL 50.42 Lf of 18 x 30(in) Elliptical @ 1.27 % 2.00 -**-** 0.05 1.00 -**-**0.95 0.00 -- -1.95 0.0 5.0 $10.0 \quad 15.0 \quad 20.0 \quad 25.0 \quad 30.0 \quad 35.0 \quad 40.0 \quad 45.0 \quad 50.0 \quad 55.0 \quad 60.0 \quad 65.0 \quad 70.0 \quad 75.0$

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Sunday, Mar 5 2017

Culvert 6, 50yr

Invert Elev Dn (ft)	= 2.90	Calculations	
· ,			- 0.00
Pipe Length (ft)	= 31.50	Qmin (cfs)	= 0.00
Slope (%)	= 0.51	Qmax (cfs)	= 20.75
Invert Elev Up (ft)	= 3.06	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 24.0		
Shape	= Elliptical	Highlighted	
Span (in)	= 42.0	Qtotal (cfs)	= 20.00
No. Barrels	= 3	Qpipe (cfs)	= 20.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	 Horizontal Ellipse Concrete 	Veloc Dn (ft/s)	= 1.62
Culvert Entrance	= Square edge w/headwall (H)	Veloc Up (ft/s)	= 1.88
Coeff. K,M,c,Y,k	= 0.01, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 4.22
		HGL Up (ft)	= 4.26
Embankment		Hw Elev (ft)	= 4.34
Top Elevation (ft)	= 6.00	Hw/D (ft)	= 0.64
Top Width (ft)	= 30.50	Flow Regime	= Outlet Control
Crest Width (ft)	= 100.00	Ŭ	
□ (/4)			Llux Danth (ft)

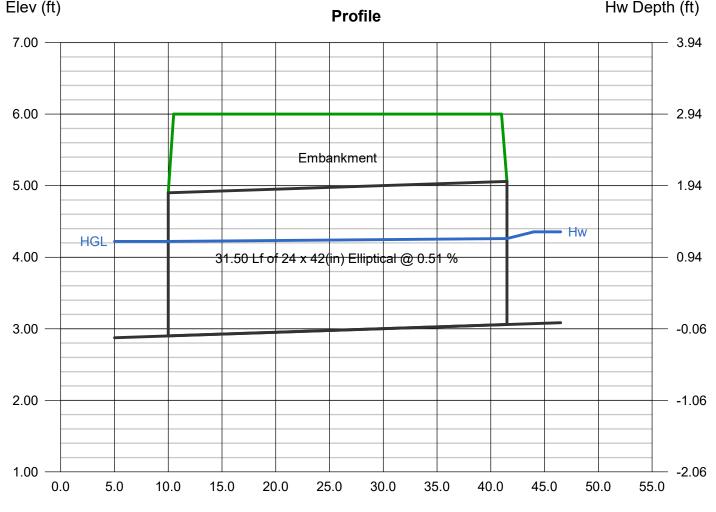


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Monday, Mar 6 2017

Culvert 6, 100yr

Invert Elev Dn (ft)	= 2.90	Calculations	
Pipe Length (ft)	= 31.50	Qmin (cfs)	= 0.00
Slope (%)	= 0.51	Qmax (cfs)	= 24.00
Invert Elev Up (ft)	= 3.06	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 24.0	, ,	,
Shape	= Elliptical	Highlighted	
Span (in)	= 42.0	Qtotal (cfs)	= 24.00
No. Barrels	= 3	Qpipe (cfs)	= 24.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	 Horizontal Ellipse Concrete 	Veloc Dn (ft/s)	= 1.94
Culvert Entrance	= Groove end w/headwll (H)	Veloc Up (ft/s)	= 2.26
Coeff. K,M,c,Y,k	= 0.0018, 2.5, 0.0292, 0.74, 0.2	HGL Dn (ft)	= 4.22
		HGL Up (ft)	= 4.26
Embankment		Hw Elev (ft)	= 4.35
Top Elevation (ft)	= 6.00	Hw/D (ft)	= 0.65
Top Width (ft)	= 30.50	Flow Regime	= Outlet Control
Crest Width (ft)	= 100.00	-	
Fley (ft)			Hw Denth (ft)

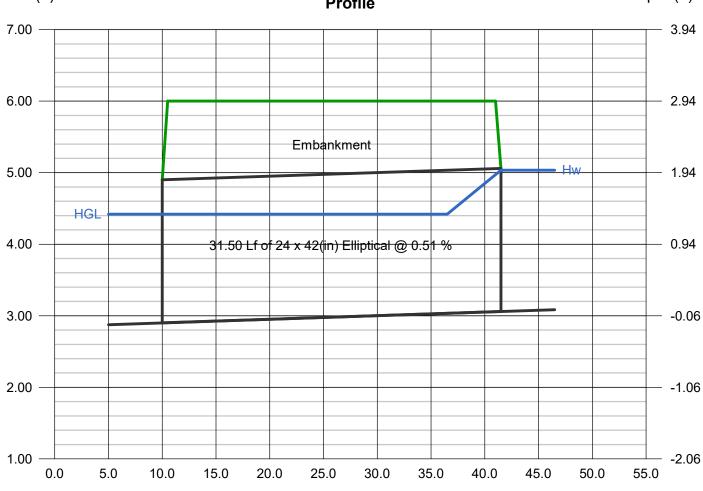


Reach (ft)

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Culvert 6, 50yr w Diversion & Pond

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 2.90 = 31.50 = 0.51 = 3.06 = 24.0	Calculations Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 0.00 = 65.00 = (dc+D)/2
Shape	= Elliptical	Highlighted	
Span (in)	= 42.0	Qtotal (cfs)	= 65.00
No. Barrels	= 3	Qpipe (cfs)	= 65.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	 Horizontal Ellipse Concrete 	Veloc Dn (ft/s)	= 4.72
Culvert Entrance	= Groove end w/headwll (H)	Veloc Up (ft/s)	= 5.25
Coeff. K,M,c,Y,k	= 0.0018, 2.5, 0.0292, 0.74, 0.2	HGL Dn (ft)	= 4.42
		HGL Up (ft)	= 4.42
Embankment		Hw Elev (ft)	= 5.03
Top Elevation (ft)	= 6.00	Hw/D (ft)	= 0.99
Top Width (ft)	= 30.50	Flow Regime	= Inlet Control
Crest Width (ft)	= 100.00		
Elev (ft)	Profile		Hw Depth (ft)

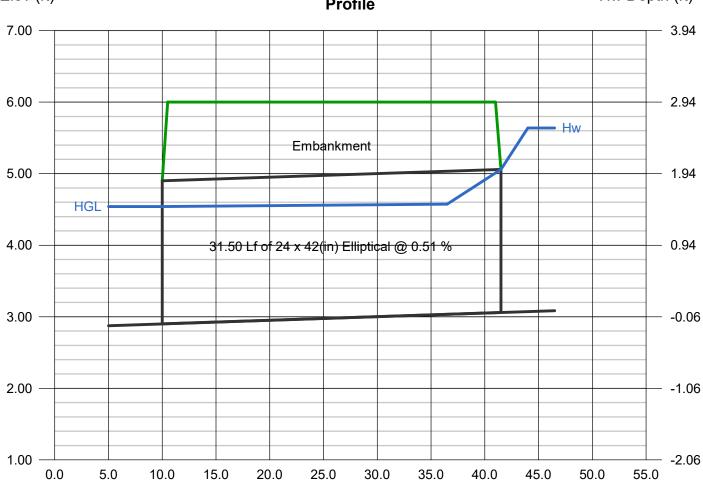


Reach (ft)

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Culvert 6, 100yr w Diversion & Pond

Invert Elev Dn (ft) Pipe Length (ft)	= 2.90 = 31.50	Calculations Qmin (cfs)	= 0.00
Slope (%)	= 0.51	Qmax (cfs)	= 100.00
Invert Elev Up (ft)	= 3.06	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 24.0		
Shape	= Elliptical	Highlighted	
Span (in)	= 42.0	Qtotal (cfs)	= 100.00
No. Barrels	= 3	Qpipe (cfs)	= 100.00
n-Value	= 0.013	Qovertop (cfs)	= 0.00
Culvert Type	 Horizontal Ellipse Concrete 	Veloc Dn (ft/s)	= 6.70
Culvert Entrance	= Groove end w/headwll (H)	Veloc Up (ft/s)	= 7.26
Coeff. K,M,c,Y,k	= 0.0018, 2.5, 0.0292, 0.74, 0.2	HGL Dn (ft)	= 4.54
		HGL Up (ft)	= 4.58
Embankment		Hw Elev (ft)	= 5.64
Top Elevation (ft)	= 6.00	Hw/D (ft)	= 1.29
Top Width (ft)	= 30.50	Flow Regime	= Inlet Control
Crest Width (ft)	= 100.00	_	
Elev (ft)	Profile		Hw Depth (ft)



Reach (ft)



ENCLOSURE (D)

CONSTRUCTION COST ESTIMATE

Construction Cost Estimate

Pond Cost Estimate							
Item	Pond Value Unit Unit Price Total Cos					al Cost	
Grading w/o Haul off	1426	CY	\$	8	\$	11,407	
Reseed	1.5	acre	\$	1,200	\$	1,800	
Finishing	2511	SY	\$	1	\$	2,511	
Replace Topsoil	2511	SY	\$	6	\$	15,067	
Construction Entrance	1	unit	\$	1,200	\$	1,200	
Fill for Dam	1070	CY	\$	15.00	\$	16,050	
Total					\$	48,035	

Pond Values					
1.5 acres					
67801	ft^2 (Pond Area)				
2511	SY (Pond Area)				

Ditch Repair (South of Culvert 2)				
~100 yards	\$	5,000		

Concrete Channel Estimate							
Item Dimension Unit Price Unit Total Co							
Base	196	\$	700	су	\$	137,407	
Walls	79	\$	700	су	\$	54,963	
				Total	\$	192,370	

Note: Channel features a base of 8ft, walls of 2ft and concrete depth of 1ft. **Note:** Concrete estimate includes cost of concrete + excavation + refill

Concrete Structure Cost Estimate							
Item Unit Price Unit Total Cost							
Concrete	\$	750.00	су	\$ 14,666.67			
Total				\$ 14,666.67			

Concrete Values		
528	cf	
19.56	су	

Note: Concrete estimate includes cost of concrete + excavation + refill

Note: Estimations were calculated from numbers received from lead estimator at Jones Bros. Contractors



ENCLOSURE (E)

MAINTENANCE AGREEMENT

City of Pegram Maintenance Agreement

A consistent maintenance program is the best way to ensure that your detention basin will continue to perform its water quality and flood control functions. Refer to your copy of the detention basin plan from the Pegram Senior Design Team for any questions as to how the detention basin is designed to function.

In general, a maintenance program should contain the following components:

- regular inspections
- review by a licensed Professional Civil Engineer
- vegetation management
- embankment and outlet stabilization
- debris and litter control
- sediment/pollution removal

The storm sewer system includes pipes, catch basins and the outlet structures that enter and exit the detention basin. It is important to regularly inspect the structural elements (inlet/outlet pipes) of your detention basin in order to ensure that storm water is flowing in and out of the pond as originally designed. Debris and sediment commonly clog detention basins and reduce the pond's overall effectiveness.

The following maintenance and inspection tasks should be included for the structural basin components: (also see Detention Basin Inspection and Maintenance Record located at the end of this Guide.

- 1. Inspect the inlet pipes and outlet pipes for structural integrity. (Annually) Check inlet/ outlet pipes for structural integrity to ensure they aren't crumbling or broken.
- 2. Inspect riprap at the inlet pipes. (Annually) Replace when the riprap is clogged with sediment and debris.

- 3. Conduct routine inspections for trash or other debris that may be blocking the inlet or outlet pipes or emergency spillway. (Monthly and after rain events)
- Remove all trash and debris from the basin. Improperly maintained ponds can harbor breeding area for mosquitos and reduce the storage volume of the pond.
- 4. Inspect and clean the storm sewer system and catch basins upstream from the detention basin. (Every 5 years or as needed)
- 5. Inspect for sediment accumulation at the inlet pipes. (Semiannually and after rain events) It's important to clean out sediment that might be restricting water flow. Remove accumulated sediment with a shovel and wheelbarrow if it is blocking water flow. Small amounts of removed sediment can be spread evenly on upland areas and seeded with natural vegetation.
- 6. Inspect the stone around the riser/standpipe (outlet pipe). (Semiannually and after rain events) If stone has accumulated sediment, vegetation and/or debris to an extent that water is not flowing through the stone and out of the pond as originally designed, then the stone should be replaced with clean 3" diameter stone choked with clean 6A stone.
- 7. Inspect for excess sediment accumulation in the pond (Annually) Remove every 5-10 years or when the sediment accumulation is more than 6-12".
- 8. Have a Professional Civil Engineer inspect the pond to ensure it is functioning properly. (Annually) Compare existing conditions to asbuilt engineering plans

Property Management:

In addition to these tasks, local homeowners should be educated to the Property management refers to specific activities that they can do to enhance the detention basin and minimize long-term maintenance. A number of these activities are described as follows:

- 1. Do not use pesticides, herbicides, or fertilizers in the ponds. These products will leach from the pond and pollute the water-decreasing the overall quality of groundwater
- 2. Do not place yard waste such as leaves, grass clippings or brush in the detention pond or in the storm drains located in the streets. These materials release excess nutrients as they decompose and will lead to more algae growth in the pond.
- 3. Do not dump any materials in the storm sewer system. Improperly disposed of materials will pollute the basin.
- 4. If you must use fertilizers, only use low-phosphorus, slow-release varieties. Keep fertilizers on the lawn and not on paved areas.
- 5. Pick up and dispose of pet waste with your weekly garbage.
- 6. Provide educational updates to the property owners. Discuss your maintenance plan at regular meetings, provide information in newsletters, and host annual clean-up days

Thank you in advance for your cooperation in maintaining the integrity and quality of your detention pond in efforts to improve water quality and overall performance.

City of Pegram Inspection and Maintenance Record

Task	Inspection Frequency	Year		
		Engineer	Cost	Notes

Inspect inlet pipes and outlet pipe for structural integrity	Annually		
Inspect riprap at inlet pipes	Annually		
Conduct routine inspections for trash or other debis that may be blocking the inlet or outlet pipes	Monthy/ After Rainfall Events		
Inspect and clean catch basins upstream	Every 5 years		
Inspect for sediment and trash accumulation at the inlet pipes	Semiannually/ After Rainfall Events		
Inspect for excess sediment accumulation in the pond	Annually		
Remove accumulated sediment at basin inlet	Semiannually/ After Rainfall Events		
Have a Professional Civil Engineer inspect the pond	Annually		
Inspect side slopes, berms and spillways for erosion	Annually/ After Rainfall Events		
Re-establish natural vegetation on eroded slopes	Annually		
Inspect basin for signs of chemicals. Remove/dispose of properly	Monthly		
Review Maintenance Plan	Annually		



Enclosure (F): Man Hour Log & Timesheets

Category	Estimated Hours	Hours To Date			
Project Management					
Management	192	195			
Phase 1: Site Investigation					
Investigation	8	13			
Phase 2: Survey					
Survey	93	115			
Preliminary Design					
Hydraulic Analysis	62	15			
Preliminary Solutions	72	41			
Final Design					
Design Work	240	200			
Totals	667	579			



Enclosure (G):Meeting Minutes

From: Abigail Queen queenaj@mail.lipscomb.edu

Subject: September 13, 2016 Minutes

Date: September 13, 2016 at 9:27 AM

To: nrcurtis@mail.lipscomb.edu, cjreid@mail.lipscomb.edu, David Lowery loweryda@mail.lipscomb.edu, Cody Glenn

caglenn@mail.lipscomb.edu, Chris Gwaltney cagwaltney@lipscomb.edu

Civil Engineering Senior Capstone Sequence

At 8:00 a.m. on Tuesday, September 13, 2016, four members of the Pegram Flood Control Project called a meeting in Hughes Engineering Center at Lipscomb University.

The following members of team were present:

Christian Reid

Nathan Curtis

DA Lowery

Abby Queen

In addition to the team members present, Cody Glenn is also a member of the PFC Team but was not in attendance. Professor Chris Gwaltney was also in attendance.

Report:

Pegram Team spoke about the alterations and enhancements of tasks- specifically the Project management. Also added man hours and some subtasks. First order of business will be to research historical data. Abby will take CSX and Socioeconomic historical data. Christian will take rainfall and flood data. Nathan will take geological data. Cody will take TDOT data. DA will begin research on the technicalities of working with Primavera and will furthermore be handling conversation between technical advisors. DA will also be contacting the EPA contact to establish a hopeful working relationship. All historical date will tentatively be completed by October 1. Surveying was discussed- a tentative date will be for early november, with a short PFC Team presentation to the Survey Class beforehand. Concrete dates have not been established.

Action: Prof Gwaltney set up DA with Primavera by September 13

Prof gwaltney will give team contact info for mayor, city planner and EPA contact

DA will. speak with technical advisors about client meeting ASAP and Sean Moynahan (EPA contact)



Minutes from Civil Senior Design Team: Pegram

Date: 09/20/2016

Group Members: Abby Queen, D.A. Lowry, Nathan Curtis, Cody Glenn, Christian Reid

All members in attendance

- Key goals of the meeting
 - Find times to meet with town officials
 - o Build WBS
 - Set up technical advisor meeting

Update of last week's minutes

Abby- Has gathered socio-economic data and has a CSX contact info. Has reached out to her contact at CSX with little response. Is continuing to try and find a reliable contact.

Cody- Has found two contacts at TDOT. Has reached out via email and is awaiting response.

D.A. - in coordination with EPA rep. about possibly joining the meeting with Pegram Town Officials. D.A. is also coordinating a meeting with the advisement team to take place soon.

Christian- Gathered 6 years of weather record for Pegram. Is currently looking for FEMA flood data and watershed information.

Current action steps

Abby- Talking to CSX contact about data availability (completion of Oct. 1)

Nathan- Gather geo data to include maps and soil data (completion of Oct. 1)

Cody- Gathering TDOT data through contacts or online (by Oct. 1)

- D.A.- Will coordinate meeting with town official, EPA rep and advisors, Awaiting Gwaltney to provide Primavera Software (by Sept. 27)
- Will offer available meeting time as Any Tuesday or Thursday by 7 am with a need to be back in Nashville by 2:30 pm. Anticipated meeting time is 2 hrs.
- Technical advisor meeting by next Thursday

Christian- Will try and determine flood depths using FEMA, cull data on weather for applications (By Oct. 1)

Group Action: finished initial WBS with tasks and man hours. Action Step: work with advisors to fill in any gaps in initial WBS. Completed by Oct. 1

Action Step: Gwaltney to give D.A. Primavera by Oct. 4

September 29, 2016
Hughes Engineering Center 5:30
the following members of the team were present:
Abby Queen
Christian Reid
Cody Glenn
DA Lowery
Nathan Curtis

The following technical advisors were present: Peter Chimera Matt Lackey

Note for team: ACME mapper topo view is helpful for aerial site view

Members informed advisors of the details of the project

Peter has been informed by local residents that there is a large gasline located between the highway and the railroad

Abby explained that shes been having difficulty contacting and gathering info from CSX. Peter may have a contact with a local

Mr. Lackey advises

gather data about the problem (ie: culvert sizes, watershed, and rainfall data) Find where the water is going will be key

gather data for contributing area from a topo map and export to CAD explore other possible solutions (detention ponds or tanks OR just improve flooding ditches if the problem is manageable)

2. Prepare preliminary cost estimates of possible solutions

For PSD, prelim proposal should include: delineate drainage basins, exclude survey, analyze culverts, find initial flows going into the culverts. Work to find the project scope through these work tasks look for improvements in the flooding ditches

- 3. Prepare a real deliverable: Find storm data and what year storm we want to design include tdot requirements for culvert sizes for railroad crossings)
 Inform the city of Pegram that the culverts are only passing the 2 year storm when they should be passing the 10 or 25 year storm
- 4. Research the requirements for utilities, TDOT, CSX. Make sure there are no other utilities that our project will be concerned with. Include right of way from TDOT regualtions

Peter advises similarly, to

Go look at the problem and talk to the surrounding property owners. Ask Pegram Mayor what the project budget actually is

Prepare cost estimates including our hours for design and project management Include survey hours as part of cost estimate

Both advisors say its a bit backwards in that we should do the design in phases, where we need to do a bit of design and gather information before putting the final price before the client

ACTION:

talk to mayors office about the project scope, practicalities of working with private entities Peter Chimera to Abby Queen concerning CSX contact All members need to go look at project area during a hard rainfall DA to follow up with Mr. Lackeys contact for easement data Christian to look up historical storm data from NOAH

Minutes

Members Present:

DA Lowery Cody Glenn Abby Queen Christian Reid Nathan Curtis Chris Gwaltney

Also Present: Mayor Morehead

Mayor: The Parking lot surrounding the culver looks like a lake

3-4 times a year. The water doesn't top Highway 70 very often though. Most of the complaints are from Small businesses. The water travels west along 70 from the gas station on the North side of the highway towards the 3 culverts that run under the highway.

DA: We should survey the whole parking lot (in front of

Citgo)

Mayor: The ditch runs back into the hills (north) and catches a

lot of water from there.

Mayor: Barriers along the ditch need to be fixed however the

state says they don't have money and there is dispute among the residents as to whether the land belongs to the government or is private property. There is also a problem at the westward culvert (in front of Parts City) however the water

does not get up to Parts City.

DA: We need to Survey from the Cash Express east to Janette Relators.

Mayor: We haven't found the sink hole and it may have been filled. There are a lot of

sinkholes in Pegram, I ran into one in my backyard 20 years ago at my House

when I was mowing. My house is at the bottom of the hills.

DA: Will TDOT pay any money towards fixing this problem?

Christian: We will prove that this culvert does not meet TDOT's standards.

Mayor: The drainage ditch does go through private property and runs from miles into

the hills. It will be hard to get onto people's land to mess with the ditch.

Christian: The solution should be near highway 70/

Gwaltney: Who have you talked to at TDOT?

Mayor: We talked to the head of district from Clarksville. He doesn't think the water is

coming from the natural reserve that sits back in the hills. The property owners

want the flooding to be fixed and may even allow you to alter their land.

Christian: We plan to come up with 3 or 4 plans and let you choose.



Culverts that run under Highway 70

Mayor: We lose businesses to flooding. TDOT cuts the grass in the ditch maybe one a

year. There is no property tax in Pegram so we can't get a grant. I am planning to bring up a property tax at the next city meeting. There are 3500 people and 1300 of them are voters. They are mostly older and retired and don't want to spend

money.

Christian: What is the cost of flood damage to a building?

Mayor: I'm not sure, but I think quite a bit. It costs several thousand dollars at least.

DA: If we prove to TDOT that we have a solution who would pay for it?

Mayor: TDOT would pay and do the work.

DA: So grant money won't help?

Mayor: TDOT could allow Pegram to do it. Christian: Could we get land from the hills?

Mayor: There are people up there who would probably be

willing to donate some land.

DA: One solution may be a detention pond in the hills.

Mayor: There may be one up there.

Gwaltney: Should we go through you to get to the land owners.

Mayor: I don't care.

Mayor: Brad Evans is the City Engineer.

DA: What are the chances on making a detention pond? Mayor: We need to talk to the lady at 4448 or 4449 (Hannah

Ford?)

DA: The Pond may be back in the trees.

Gwaltney: It sounds like they took a problem and worked in the

middle but not at the ends (referring to culvert that

runs under Hannah Ford Rd)

Could we do ditch improvements?



Possible Place for detention pond along Hannah Ford Road

The ditch was not this big when I moved Mayor:

here.

RESIDENT: There was not ditch when I moved here.

The water doesn't get above the wood wall my husband built. There was a kid who almost drowned here. It wasn't a problem until the houses were built in the north.



Ditch that runs along the edge of the RESIDENT'S property. Was not there when RESIDENT moved in.

Christian: There are some big rocks that get washed down here.

DA: We will be doing a survey in early November.



Looking toward culvert that runs under Hannah Ford Road (causing ditch).





Ditch that runs south Under Hannah Ford Road

Meeting Minutes

10/18/2016

Members in attendance: Christian, Nathan, Abby, Cody, DA

Advisors in attendance: Prof. Gwaltney

We discussed the new layout for the shared drive folder to include locations of all files. Group members all now have OneDrive on computer for ease of access to files.

We reviewed the work breakdown structure, tasks and hours were agreed upon by all members. **Action Item: DA will finish schedule in Primavera P6, due 10/25/2016.**

Action item sections for proposal due from all member 10/25/2016 for review by group. Submittal of final proposal due 11/1/2016.

Action item survey boundary and presentation for survey class completed by Cody 10/25/2016

Action item the group will make a site visit to establish benchmark prior to surveying trip, which is on 11/5/2016. DA will coordinate with Mayor Moorehead to get permission for access to survey area. Group will provide a list to professor 4- 5 days prior to benchmark establishment trip. Date TBD based on coordination with mayor.

technical advisor meeting minutes
February 28, 2017
5:00 PM
all members of Pegram Senior Design present
Professor Chris Gwaltney present
Technical Advisors:
Matt Lackey
Justin
Peter Chimera

need drainage maps: delineation of large culvert and watershed of each area USGS Topo

osas jobo

show land use to explain curve numbers

list assumptions for estimated capacity of culverts

which controls? manning (outlet control) or inlet control

true flow is larger than estimated based on low curve numbers- needs to be at least a curve number of 60

label ditch improvement on proposal
Matt recommendation: create diversion ditch in analysis
What is the capacity of the southern culvert, when it will overtop
and who will diversion impact
give maintenance plan for designed structures

make outlet structure only able to send max amount of capacity to the culverts split outlet structure

redefine scope as it has unfolded

may have to assume things, just state an assumption- "dont chase the rabbit down the hole"

give mayor information on existing condition analysis for Pegram to give to TDOT for \$\$ also schematic design options for senior design project:

Construction drawings for ditch and pond structures

prove everything in calculations: include addition of culverts and curve number(soil types)

break everything down into components and show work matt and DA got in a fistfight matt will bill DA for ripped shirt come up with a plan to design



Enclosure (H):Presentation Slides



Enclosure (I): Reference Material

Welcome to the Town of Pegram, Tennessee

Main No. 615-646-0773 / FAX 615-646-6869 Town Hall Hours: Monday - Friday, 8 AM-12 PM & 1-4 PM Sewer Emergency After Hours: 533-2637

"Community Leaders"

Please be advised that e-mail you send to and/or receive from any Town official or staff member may be a public record subject to the Tennessee Public Records Law, T.C.A. §10-7-503.

Pegram Charter - Click Here.

Pegram Codes (Verify with City Hall for any updates) - Click Here.

Charles Morehead	Mayor, Purchasing Agent, Personnel Supervisor	mrcourier@att.net	615-426-3275
Bill Herbert	Vice Mayor	wm358@bellsouth.net	615-646-6994
Bob Sanders	Alderman	rsand21@aol.com	615-403-7475
Aubrey Chambers	Alderman	slctoo@bellsouth.net	615-646-1627
Warren Miller	Alderman	warrenwsm27@aol.com	615-662-0119
Jamie Mrzena	Town Recorder - Court Clerk/Accounting Department Head	recorder@negram net	615-646-0773
Jennie Peters	Town Clerk - Front Desk Management	cityhall@pegram.net	615-646-0773
James Parks	Building / Codes Enforcer	, and the second	615-646-0773
Jim Stinnett	Sewer Operator		615-646-0773
Larry Martin	Public Works- Maintenance Department Head	publicworks@pegram.net	615-646-0773
Brad Bivens	Engineer - Town Consultant		615-646-0773
			615-646-0773
Martha Brooke Perry	Attorney - Town Consultant		615-646-0773
Brent Stuart	PFD Fire Chief (Volunteer Part-Time)		615-646-6800
Nathan Stanley	PFD Asst. Chief (Volunteer Part-Time)		615-646-6800
Lou Chambers	Planning Commission	slctoo@bellsouth.net	615-646-1627
Charles W. Edens	Planning Commission		615-662-9903
Gene Hannah	Planning Commission, Chairman		615-646-6616
Bob Sanders	Planning Commission		615-673-7609
Melissa McWright	Planning Commission		615-646-3114
T I IZ:ub	Doord of Zoning Anneals Chairman		615-673-7205
T.J. Kirby	Board of Zoning Appeals, Chairman		015-0/3-/205
David Becker	Board of Zoning Appeals		
Donnie Dunn	Board of Zoning Appeals		
Gary Jackson	Board of Zoning Appeals		
Rick Roarke	Board of Zoning Appeals		

Lou Chambers	Emergency Management Board - Director	slctoo@bellsouth.net	615-646-1627
Kevin Stewart	Emergency Management Board - Assistant Director		615-646-5098
Brent Stuart	Emergency Management Board - Fire Department Representative		615-646-0773
Aubrey Chambers	Emergency Management Board - Governing Body Representative		615-646-1627
Stoney Greenlee	Emergency Management Board		615-662-0831
Wanda Kelley	Emergency Management Board		615-977-9871
Cindy Beirnes	Emergency Management Board		615-646-3022
Kathy Cundall	Emergency Management Board		615-662-8567
Mark Beirnes	Emergency Management Board		615-646-3022
Barry Mangrum	Emergency Management Board		615-533-9636

Sheriff's Office: 792-4341 (Enforcement for Town of Pegram)

Pegram Sewer Emergency After Hours: 533-2637 or 533-2461

Animal Control: 792-3647 / Landfill & Recyling Center: 792-7538

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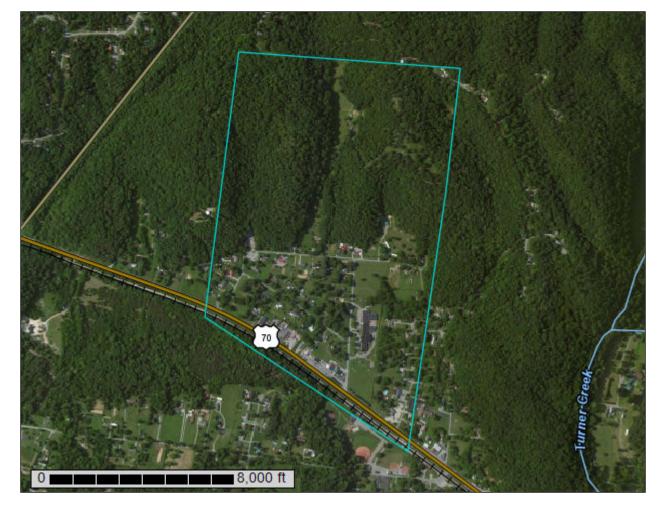
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Last update: 10/01/2010



Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Cheatham County, Tennessee



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Unit Polygons

-

Soil Map Unit Lines

Soil Map Unit Points

Special Point Features

ဖ

Blowout

 \boxtimes

Borrow Pit

Ж

Clay Spot

Closed Depression

Gravel Pit

۰

Gravelly Spot

0

Landfill Lava Flow

٨.

Marsh or swamp

尕

Mine or Quarry

0

Miscellaneous Water
Perennial Water

0

Rock Outcrop

+

Saline Spot

...

Sandy Spot

Severely Eroded Spot

Λ

Sinkhole

d

Sodic Spot

Slide or Slip

8

Spoil Area



Stony Spot



Very Stony Spot



Wet Spot Other



Special Line Features

Water Features

_

Streams and Canals

Transportation

ransp

Rails

~

Interstate Highways

~

US Routes

 \sim

Major Roads

 \sim

Local Roads

Background

1

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Cheatham County, Tennessee Survey Area Data: Version 10, Sep 11, 2015

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Mar 17, 2011—May 30, 2011

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Cheatham County, Tennessee (TN021)					
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI		
AmB2	Armour silt loam, 2 to 5 percent slopes	23.8	10.5%		
AmC2	Armour silt loam, 5 to 12 percent slopes	0.0	0.0%		
ВуВ2	Byler silt loam, 2 to 5 percent slopes, eroded	53.3	23.4%		
En	Ennis gravelly silt loam, occasionally flooded	12.8	5.6%		
HaC	Hawthorne gravelly silt loam, 5 to 12 percent slopes	17.7	7.8%		
HaD	Hawthorne gravelly silt loam, 12 to 20 percent slopes	16.7	7.3%		
HsF	Hawthorne-Sulphura association, steep	68.1	29.9%		
HuB	Humphreys gravelly silt loam, 2 to 5 percent slopes	12.6	5.5%		
MnD2	Minvale gravelly silt loam, 12 to 20 percent slopes, eroded	22.7	10.0%		
Totals for Area of Interest		227.6	100.0%		

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They

generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Cheatham County, Tennessee

AmB2—Armour silt loam, 2 to 5 percent slopes

Map Unit Setting

National map unit symbol: 2td31 Elevation: 500 to 850 feet

Mean annual precipitation: 48 to 58 inches
Mean annual air temperature: 57 to 61 degrees F

Frost-free period: 190 to 230 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Armour and similar soils: 90 percent Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Armour

Setting

Landform: Stream terraces

Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave, convex Across-slope shape: Linear, convex

Parent material: Silty alluvium over clayey residuum weathered from phosphatic

limestone

Typical profile

A - 0 to 19 inches: silt loam

Bt - 19 to 58 inches: silty clay loam

BC - 58 to 79 inches: clay

Properties and qualities

Slope: 2 to 5 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20

to 0.60 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Available water storage in profile: High (about 11.6 inches)

Interpretive groups

Land capability classification (irrigated): 2e Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: B Hydric soil rating: No

Minor Components

Byler

Percent of map unit: 4 percent Landform: Stream terraces

Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave, convex Across-slope shape: Linear, convex

Hydric soil rating: No

Arrington

Percent of map unit: 4 percent

Landform: Flood plains

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope

Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

Mimosa

Percent of map unit: 2 percent Landform: Escarpments

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave, convex Across-slope shape: Linear, convex

Hydric soil rating: No

AmC2—Armour silt loam, 5 to 12 percent slopes

Map Unit Setting

National map unit symbol: 2td32

Elevation: 500 to 850 feet

Mean annual precipitation: 48 to 58 inches Mean annual air temperature: 57 to 61 degrees F

Frost-free period: 190 to 230 days

Farmland classification: Not prime farmland

Map Unit Composition

Armour and similar soils: 90 percent Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Armour

Setting

Landform: Stream terraces

Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave, convex Across-slope shape: Linear, convex

Parent material: Silty alluvium over clayey residuum weathered from phosphatic

limestone

Typical profile

A - 0 to 19 inches: silt loam

Bt - 19 to 58 inches: silty clay loam

BC - 58 to 79 inches: clay

Properties and qualities

Slope: 5 to 12 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20

to 0.60 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Available water storage in profile: High (about 11.6 inches)

Interpretive groups

Land capability classification (irrigated): 3e Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: B Hydric soil rating: No

Minor Components

Byler

Percent of map unit: 4 percent Landform: Stream terraces

Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave, convex Across-slope shape: Linear, convex

Hydric soil rating: No

Dellrose

Percent of map unit: 4 percent

Landform: Hillsides

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

Mimosa

Percent of map unit: 2 percent Landform: Escarpments

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave, convex Across-slope shape: Linear, convex

Hydric soil rating: No

ByB2—Byler silt loam, 2 to 5 percent slopes, eroded

Map Unit Setting

National map unit symbol: kpd6 Elevation: 400 to 700 feet

Mean annual precipitation: 48 to 55 inches Mean annual air temperature: 57 to 61 degrees F

Frost-free period: 190 to 205 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Byler and similar soils: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Byler

Setting

Landform: Stream terraces

Landform position (three-dimensional): Tread

Parent material: Loamy alluvium over clayey residuum weathered from limestone

Typical profile

H1 - 0 to 9 inches: silt loam
H2 - 9 to 24 inches: silt loam
H3 - 24 to 44 inches: silty clay loam
H4 - 44 to 60 inches: silty clay loam

Properties and qualities

Slope: 2 to 5 percent

Depth to restrictive feature: About 24 inches to fragipan

Natural drainage class: Moderately well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.06 to 0.20 in/hr)

Depth to water table: About 24 to 36 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Low (about 4.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C Hydric soil rating: No

En—Ennis gravelly silt loam, occasionally flooded

Map Unit Setting

National map unit symbol: kpd9 Elevation: 900 to 1,300 feet

Mean annual precipitation: 45 to 54 inches Mean annual air temperature: 57 to 61 degrees F

Frost-free period: 180 to 205 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Ennis and similar soils: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Ennis

Setting

Landform: Flood plains

Landform position (three-dimensional): Tread

Parent material: Loamy alluvium derived from limestone, sandstone, and shale

Typical profile

H1 - 0 to 7 inches: gravelly silt loam H2 - 7 to 60 inches: gravelly silt loam

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: Occasional Frequency of ponding: None

Available water storage in profile: Moderate (about 7.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2w

Hydrologic Soil Group: A Hydric soil rating: No

HaC—Hawthorne gravelly silt loam, 5 to 12 percent slopes

Map Unit Setting

National map unit symbol: kpdf Elevation: 900 to 1,300 feet

Mean annual precipitation: 48 to 55 inches
Mean annual air temperature: 57 to 61 degrees F

Frost-free period: 185 to 205 days

Farmland classification: Not prime farmland

Map Unit Composition

Hawthorne and similar soils: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hawthorne

Setting

Landform: Hillslopes

Landform position (three-dimensional): Crest

Parent material: Gravelly residuum weathered from limestone and siltstone

Typical profile

H1 - 0 to 6 inches: gravelly silt loam

H2 - 6 to 33 inches: very channery silt loam

Cr - 33 to 43 inches: bedrock

Properties and qualities

Slope: 5 to 12 percent

Depth to restrictive feature: 20 to 39 inches to paralithic bedrock

Natural drainage class: Somewhat excessively drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

high (0.00 to 0.20 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Low (about 3.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4s

Hydrologic Soil Group: B Hydric soil rating: No

HaD—Hawthorne gravelly silt loam, 12 to 20 percent slopes

Map Unit Setting

National map unit symbol: 2v59f Elevation: 350 to 1,070 feet

Mean annual precipitation: 48 to 58 inches
Mean annual air temperature: 57 to 69 degrees F

Frost-free period: 190 to 230 days

Farmland classification: Not prime farmland

Map Unit Composition

Hawthorne and similar soils: 88 percent

Minor components: 12 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hawthorne

Setting

Landform: Hillslopes

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Gravelly residuum weathered from limestone and siltstone

Typical profile

Oi - 0 to 1 inches: slightly decomposed plant material

A - 1 to 5 inches: gravelly silt loam
AE - 5 to 12 inches: gravelly silt loam
Bw - 12 to 18 inches: very gravelly silt loam
C - 18 to 26 inches: very gravelly silt loam

Cr - 26 to 36 inches: bedrock

Properties and qualities

Slope: 12 to 20 percent

Depth to restrictive feature: 20 to 30 inches to paralithic bedrock

Natural drainage class: Somewhat excessively drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.10 to 0.20 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Available water storage in profile: Very low (about 2.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B Hydric soil rating: No

Minor Components

Sugargrove

Percent of map unit: 6 percent

Landform: Hillsides

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

Dellrose

Percent of map unit: 4 percent

Landform: Hillsides

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Concave Across-slope shape: Linear

Hydric soil rating: No

Sengtown

Percent of map unit: 2 percent

Landform: Hills

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Hydric soil rating: No

HsF—Hawthorne-Sulphura association, steep

Map Unit Setting

National map unit symbol: kpdh Elevation: 600 to 1,300 feet

Mean annual precipitation: 48 to 55 inches Mean annual air temperature: 57 to 61 degrees F

Frost-free period: 185 to 205 days

Farmland classification: Not prime farmland

Map Unit Composition

Hawthorne and similar soils: 60 percent Sulphura and similar soils: 20 percent Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hawthorne

Setting

Landform: Hillslopes

Landform position (three-dimensional): Side slope

Parent material: Gravelly residuum weathered from limestone and siltstone

Typical profile

H1 - 0 to 6 inches: gravelly silt loam

H2 - 6 to 33 inches: very channery silt loam

Cr - 33 to 43 inches: bedrock

Properties and qualities

Slope: 20 to 60 percent

Depth to restrictive feature: 20 to 39 inches to paralithic bedrock

Natural drainage class: Somewhat excessively drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

high (0.00 to 0.20 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Low (about 3.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: B Hydric soil rating: No

Description of Sulphura

Setting

Landform: Hillslopes

Landform position (three-dimensional): Side slope

Parent material: Channery residuum weathered from limestone and shale

Typical profile

H1 - 0 to 10 inches: gravelly silt loam
H2 - 10 to 22 inches: very channery silt loam

R - 22 to 32 inches: bedrock

Properties and qualities

Slope: 20 to 60 percent

Depth to restrictive feature: 20 to 40 inches to lithic bedrock Natural drainage class: Somewhat excessively drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Very low (about 2.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: C Hydric soil rating: No

Minor Components

Minor components

Percent of map unit: 20 percent

Hydric soil rating: No

HuB—Humphreys gravelly silt loam, 2 to 5 percent slopes

Map Unit Setting

National map unit symbol: kpdj Elevation: 600 to 1,200 feet

Mean annual precipitation: 46 to 60 inches
Mean annual air temperature: 57 to 61 degrees F

Frost-free period: 180 to 205 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Humphreys and similar soils: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Humphreys

Setting

Landform: Stream terraces

Landform position (three-dimensional): Tread

Parent material: Loamy alluvium and/or colluvium derived from limestone

Typical profile

H1 - 0 to 8 inches: gravelly silt loam
H2 - 8 to 51 inches: gravelly silty clay loam
H3 - 51 to 60 inches: gravelly silty clay loam

Properties and qualities

Slope: 2 to 5 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00

in/hr)

Depth to water table: About 60 to 72 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Moderate (about 7.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: A Hydric soil rating: No

MnD2—Minvale gravelly silt loam, 12 to 20 percent slopes, eroded

Map Unit Setting

National map unit symbol: kpdp Elevation: 500 to 1,200 feet

Mean annual precipitation: 45 to 55 inches Mean annual air temperature: 57 to 61 degrees F

Frost-free period: 180 to 205 days

Farmland classification: Not prime farmland

Map Unit Composition

Minvale and similar soils: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Minvale

Setting

Landform: Hillslopes

Landform position (three-dimensional): Base slope

Parent material: Loamy colluvium derived from cherty limestone

Typical profile

H1 - 0 to 8 inches: gravelly silt loam H2 - 8 to 18 inches: gravelly silt loam

H3 - 18 to 60 inches: gravelly silty clay loam

Properties and qualities

Slope: 12 to 20 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to

high (0.60 to 2.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Moderate (about 8.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: B Hydric soil rating: No

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